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Resented by the National Observatory,

Washington:

ZONES OF STARS

OBSERVED AT

THE NATIONAL OBSERVATORY, WASHINGTON.

APPROVED BY

CAPT. G. A. MAGRUDER,

CHIEF OF THE BUREAU OF ORDNANCE AND HYDROGRAPHY;

AND PUBLISHED UNDER AUTHORITY OF

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VOL. I.—PART I.

CONTAINING THE ZONES OBSERVED WITH THE MERIDIAN CIRCLE IN 1846.

WASHINGTON:
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INDEX.

Introduction.	
Register of Zones	x
Zones	
Notes	10
Errata.	10

INTRODUCTION.

Commander M. F. MAURY, U. S. N.,

Superintendent of the Observatory.

Sir.: In compliance with your instructions, I herewith present observations of zones, made with the Meridian Circle in the year 1846, arranged for convenient reference, and accompanied with the reductions and results. The zones of stars contained in the present volume—even when completed by the addition of those observed during the same year by the Transit and Mural—will make but a small portion of the series of observations commenced at the National Observatory, in pursuance of an order from the Secretary of the Navy, dated March 6, 1846, and which, in consequence of many other pressing duties, and the limited computing force allowed, it has been found impossible to reduce and prepare for publication at an earlier day. The series was originally designed to include all stars within the compass of our instruments, and crossing the meridian at an elevation of above eight degrees. The observations were continued without interruption until the year 1853, or until it had become apparent that the labors of the observers were only accumulating an amount of material which they had no means, within a reasonable time, of putting into a shape convenient for use. Previous to this time, however, the observations made in the years 1846 and 1847, had been copied from the observing books, the forms of reduction arranged, and some progress made in the reduction itself. This commencement was soon after interrupted, not again to be resumed till the autumn of 1859. The present volume contains all of the work which there has, as yet, been time to prepare for publication, and must be taken merely as the first fruit of a very comprehensive plan, the execution of which has only been impeded by lack of adequate force.

The observations with the Meridian Circle (the results of which make the first part of this volume) were made by Professor J. S. Hubbard and Lieutenant L. Maynard. It will be a necessary preliminary to describe the instrument with which they were made, the methods of observation, adjustment, and reduction, and to explain the tabular forms in which the data, the reductions, and results are now presented.

THE INSTRUMENT.

The Meridian Circle of the Observatory is now much changed from its original construction. The following description of it as it was in 1846, when these observations were made, is taken, with little variation, from the second volume of the Washington Astronomical Observations published in that year: "The foundation upon which it rests is of masonry, and similar to those of the Transit Instrument and Mural Circle. The piers are of granite. At each end of the axis and outside of each pier is a circle thirty inches in diameter, of which, one, the western, during the year 1846, is graduated only to fifteen minutes, and subdivided by a vernier to single minutes. This is the finding circle. To it is attached the clamp, the binding screw of which passes through the pier; the tangent screw for slow motion in declination, acting on the clamp, carries with it the circle and the telescope. This circle may be moved about its axis, and is adjusted so that the zero of graduation corresponds to the zenith. The reading for the equator is, when the finding circle is West, 321° 6'; when East, 38° 54'. The second circle is graduated to three minutes and subdived by four microscopes, lettered A, B, C, D, which read to single seconds, and, by estimation, to tenths of a second. This circle is left entirely free from clamps, and is never touched by the observer. The microscopes are held by four bearers, resting on the circumference of a smaller circle, which is supported by a prolongation of the axis of the instrument, but prevented from turning with it by means of a small bar proceeding downwards from the center:



this bar being confined between the two screws which, when the telescope is reversed, give the slow motion to the instrument. A spirit level attached to the bar and small circle, and called the Alidade level, is intended to detect any movement of the microscope system about the common center. This level, however, cannot be reversed, and experience has shown that its indications could not be trusted, as the presence of the observer's person, while reading the microscopes, affected it sensibly. And whenever a current of air passed through the room, it caused such changes of position in the bubble as to render unsafe any inference of change in the instrument, and the readings have been therefore entirely disregarded. One division of this level is equal to 2".78. A similar level is attached to the other extremity of the axis near the finding circle, but no use has been made of it. From the top of each pier rises a small brass pillar to the height of 21.5 inches, through which passes a steel lever 15.5 inches long, parallel with the horizontal axis, and intended to remove by a counterpoise the additional weight of the alidade circle and microscopes from the axis of the instrument. From the side of one of these pillars also projects a small hook which serves to support the striding level when in position. The pillars fit in sockets at their base, instead of being permanent, as it is necessary to remove them before reversing the instrument. The main counterpoises bearing up the axis are applied through friction rollers and by means of short horizontal levers at points immediately adjoining and within the termination of the steel pivots. The telescope tube is 56 inches in length, being composed of the central cube and two brass cones, each 24 inches long, 7.2 inches diameter at the cube, and 3.8 inches diameter at the end. The broad rings containing the object-glass and eye-piece, fit accurately the extremities of the main tube, surface to surface, and are convertible; the change from object-end to eye-end being very easily effected, and the simplest means thus afforded for eliminating the effect of flexure. The object-glass has 4.5 inches of clear aperture, and 58.2 inches focal length. The optical performance of the telescope is most excellent, enabling the observer to use the highest magnifying power with advantage in the ordinary state of the atmosphere. The lower powers have generally been used only for observations of the sun and of faint stars, which would bear but feeble illumination. The eye-piece is arranged to have a vertical, as well as horizontal motion, and commands the whole field of view. The illumination of the field is effected by means of a small lamp attached to a bent arm, which enters the pier immediately below the finding circle, and the light is conveniently modified by a small piece of red glass fitted to the open end of the axis. The reversing apparatus, was attached to the piers by two cross pieces, which supported and steadied the screw. A slight experience, in 1845, was sufficient to show that this mode of reversing was too prejudicial to the permanence of adjustment to be continued with safety, and there being no other means at hand of effecting the reversal, the instrument was suffered to remain in one position during the year 1846. The value of one division of the striding level, as determined by means of the mural circle, was found to be 1".681, or 0s.1121 in time." This value has been used in determining the inclination of the axis to the horizon, and also in the discussion of a series of observations, made in this and the preceding years, to determine the figure of the pivots, for the details of which the reader is referred to Washington Astronomical Observations for 1846, pp. xxxviii to xl. The circle is read by four microscopes, held by the bearers already mentioned. "In the focus of the eye-piece of each microscope are two parallel wires, about 10' apart, which, when the circle is read, are placed so as to include between them the broad division marks of the limb a mode of reading inferior in accuracy to that with cross wires, as in the Troughton microscopes." In the second volume of Washington Observations, already quoted, (pp. xli to liii,) will be found an investigation of the inequality of the micrometer screw, and errors of graduation, which it is not deemed necessary to insert in this place. As in these zone observations the circle was uniformly set near a division of the circle, the correction for runs of the microscope is inappreciable, and has been neglected. The diaphragm contained, in 1846, eleven transit wires and seven micrometer or declination wires; the transit wires being designated as follows: 1, 2, I, II, III, IV, V, VI, VII, 10 11; and the micrometer wires by the numbers, 1, 2, 3, 4, 5, 6, 7. The first of the transit wires is that over which. when the circle is east, the star first passes at its upper culmination. And the first of the micrometer wires is that which is uppermost in the field, with the circle east, and the observer looking southward.

The equatorial intervals of the transit wires (their distances from the mean wire,) for the whole of these observations is as follows:

$$M-1=+60.49$$
 $M-11=-60.49$ $M-10=-49.31$ $M-10=-49.31$ $M-11=+32.903$ $M-11=+21.791$ $M-11=+10.964$ $M-1V=-0.026$ $M-V=-10.877$

These values, with the exception of the two first and two last, (those at the extremities of the field,) have been deduced from transits of Polaris and δ Ursæ Minoris, and obtain for the middle or fixed wire. No transits were observed on the wires 1, 2, and there is no recorded determination of the value of the intervals between them and the mean wire. These intervals M - 1, M - 2, being only used as arguments for the reduction to the meridian, they have been set down at the same distances from the mean wire as 10 and 11.

"For the zone observations where the stars have been observed at various distances from the middle of the field, it becomes important to determine the errors of the transit wires throughout their whole length. For this purpose the following table has been deduced from the zones themselves."

	M—I.	M—II.	M—III.	M—IV.	MV.	M—VI.	M—VII.	M—10.	M—11.
Rev.	*. +32.99	*. +21.96	s. +11.03	s. 0.03	s. —10.94	s. 22.00	s. -32.94	s. 49.05	s. 60.42
10	.99	.93	.02	.03	.93	.01	.94	.13	.44
20	.99	.90	.02	.03	.92	.03	.95	.20	.46
30	.98	.87	.01	.03	.92	.05	.96	.26	.48
40	.98	.84	.00	.03	.91	.06	.97	.30	.48
50	.98	.81	.00	.03	.90	.04	.96	.30	.45
60	.97	.78	.01	.03	.90	.01	.94	.29	.40
70	.97	.75	.01	.03	.89	21.98	.91	.27	.33
80	+32.97	+21.72	+11.01	-0.03	-10.89	21.95	-32.88	-49.25	-60.25

"The distances between the micrometer wires and the middle one have been determined by means of the collimating eye-piece and circle-readings, each wire being made to coincide with its own image, or that of wire 4. The mean of all the determinations gives:

$$4-1 = -20 \ 30^{\circ}.25 = 35.677$$
 $4-2 = -14 \ 38.54 = 25.477$
 $4-3 = -5 \ 55.42 = 10.307$
 $4-5 = +5 \ 46.13 = 10.038$
 $4-6 = +14 \ 28.94 = 25.199$
 $4-7 = +20 \ 19.03 = 35.351$

"The value of a revolution of the micrometer screw has been obtained from the intervals of 4 — 3 and 4 — 5, by comparing the coincidences of wires 3, 4, and 5 with the fixed wire." The mean of all the determinations gives 34.483 for this value. There seems to have been no determination of the inclination, or of any irregularity in the intervals of the declination wires, during the year. The intervals have, therefore, been assumed as constant, and the wires as parallel and perpendicular to the meridian.

The revolutions of the micrometer screw are counted on a notched scale, placed in the focus of the telescope and in the edge of the field. The intervals between the notches of this scale are equal to one revolution of the screw, and every fifth notch is further marked by a hole opposite to it in the scale. A pointer moved by the micrometer screw and



so adjusted that when it is in the interval between two notches, the index of the screw-head shall mark zero, serves to count the number of revolutions. The notch nearest the middle of the field, being one of the holed notches, is numbered 40. The scale counting in the same direction as the declination wires, that is, beginning at the upper edge of the field when the circle is east, and the observer looking southward, and counting from 0 to 80. The head of the micrometer screw is graduated to hundredths.

A fixed horizontal wire marks the middle of the field at or near the fortieth division of the scale. To this are referred all the angular measures of the telescope, and its relation to the micrometer scale is determined by noting the readings of the scale and screw-head, when the fourth declination wire is brought to coincide with it. This reading is recorded as the micrometric coincidence. In these observations it has always been a fraction greater than 40.

The collimating eye-piece heretofore mentioned, was constructed out of one of the eye-pieces of the instrument by inserting between its lenses a plane mirror perforated at the center and movable about an axis perpendicular to the optical axis of the telescope—the cell of the eye-piece being left open opposite the mirror to receive the light of a lamp held before it.

METHODS OF OBSERVATION AND ADJUSTMENT.

The Nadir Point upon which the observed altitudes depend has been determined by the collimating eye-piece—the fixed wire being brought to coincide with its image as seen through the telescope reflected in a basin of quicksilver, and the reading of the circle in this portion taken as the Nadir Point at the instant of observation. These coincidences were repeated five times at each determination, and the mean, corrected for runs, taken as final. The details of these observations will be found in the second volume of the Washington Astronomical Observations, already quoted. The result (N+180°) under the head of Zenith Point, with the corresponding value of the micrometer coincidence, comprehend all that it has been thought necessary to insert here.

The corrections for errors of level, azimuth, and collimation have been made according to the formula of Bessel, by which, supposing the telescope to be directed to any point where declination is δ , and that the axis of the meridian circle prolonged westward mark a point in the heavens whose declination is n, and its hour angle from the meridian counted westward (90°—m); the angle which the optical axis of the telescope makes with the axis of the instrument, counted also westward, being (90°+c,) we will have for the sum of these errors—

$$I = m + n$$
. tang. $\delta + c$ sec. δ .

And if now we make b the inclination of the axis of the circle with the horizon and $(90^{\circ}-k_{\circ})$ its azimuth counted from the south westward; φ being the latitude of the observer, we have—

$$m = b \cos \varphi + k \sin \varphi$$
.
 $n = b \sin \varphi - k \cos \varphi$.

The quantity b is determined directly by the striding level, having regard to the error arising from inequality of the pivots, and the quantity $(b\pm c)$ by the collimating eye-piece. By this process, without reversal of the instrument, (which during the year 1846 could not be safely effected,) we obtain the value of c, which is further corrected for the reduction to the mean wire and for diurnal aberration.

The value of (n+c) is obtained by either of the following formulas:

$$n+c = \frac{(\alpha-\tau)-(\alpha+12-\tau)}{2 \text{ tang. } \delta}$$

$$n+c = \frac{(\alpha-\tau)-(\alpha'-\tau')+c \text{ (sec. } \delta'-\tan. \ \delta')}{\tan. \ \delta-\tan. \ \delta'}$$



In which α , δ , τ represent the right ascension, declination, and time of transit of a circumpolar star, and α' δ' τ' the right ascension, declination, and time of transit of an equatorial star. In determining the value of (n+c) the transit of a circumpolar star was compared with all the others observed on the same night, these transits having been first corrected by the quantity c. (sec. δ —tang. δ .)

The value of m was then computed from the formula—

$$m = b \sec \varphi - n \tan \varphi$$
.

The stand and rate of the clock, at the hour most convenient for the observations, were determined by comparing the corrected transits of fundamental stars with their tabulated places.

METHODS OF REDUCTION.

These include the determination for each zone, of the following quantities:

- (1.) The correction for the error and rate of the clock.
- (2.) The declination of the middle of the zone, or of the 40th division of the micrometer scale, corrected for the refraction dependent upon the state of the atmosphere at the commencement of the observations.
- (3.) The difference of refraction between the middle of the zone and each 10th division of the micrometer scale at the commencement of the observations.
 - (4.) The corrections for changes in atmospheric conditions occurring during the observations.
 - (5.) The corrections for changes in the reading of the Circle during the observations.
- (6.) The intervals of the transit wires, or their distances from the mean wire, answering to the declination of the middle of the zone, and to each 10th division of the micrometer scale. These intervals being computed from the equatorial intervals given at page VII.
- (7.) The reductions to the mean places for 1850.0, for the declination of the middle of the zone, and for each 20th minute of right ascension contained in it; also the change in these reductions for each 10th division of the micrometer scale.
- (8.) The sum of the corrections, for error of level, azimuth, and collimation, for the declination of the middle of the zone, computed by the formula—

$$I = m + n \text{ tang. } \delta + c \text{ sec. } \delta.$$

And the changes in this correction for each 10th division of the micrometer scale.

(9.) The reduction of the observed declination to the meridian = $-\frac{\sin^2 \frac{1}{2} h \cdot \sin^2 \frac{1}{2} h}{\sin^2 \frac{1}{2} h}$ where h is the hour angle and δ the declination of the star observed.

These different quantities having been computed, those dependent only upon the time were combined and the values of their sums interpolated for every 10th minute. Those dependent upon the declination of the observed body or its place in the zone being applied separately to each observation.

In reducing the observed right ascensions, the observed transits were first referred to the mean wire by means of the intervals described in (6.) Then using the following notation:

 $\alpha =$ the right ascension of the observed star,

T = its time of transit over the mean wire.

 $\Delta \delta =$ the difference of declination from the middle of the zone,

K =correction to the clock,

I = correction for level, azimuth, and collimation at the middle of the zone,

 $\Delta I =$ change in the value of I answering to $\Delta \delta$,

 $M\alpha =$ reduction to mean place of 1850.0 for the middle of the zone,

A



 $\Delta M\alpha =$ change in the value of $M\alpha$ answering to $\Delta \delta$.

We shall have, for the mean right ascension for 1850.0,

$$a = T + K + I + \Delta I + M\alpha + \Delta M\alpha$$
.

The quantity I being constant for the whole zone; K and M depending upon the time, and ΔI , $\Delta M\alpha$, upon the position of the observed star, or its difference of declination from the declination of the middle of the zone.

In reducing the observed declinations, the following method was adopted: The micrometer intervals were counted, not from the middle of the zone, but from 30' north of it, so that their values have all the same sign as the declination. The corrections for differential refraction in the zone, and also the reductions to the mean place for 1850.0, being applied by differences, two arbitrary constants were introduced, n', n'', the first greater than the whole of $M\partial$, and the other greater than the whole change of ρ , each with a negative sign. These constants avoid the liability to error arising from a change of sign in the quantities $M\partial$, ρ , in the same zone; using the following notation:

 δ = mean declination of an observed star for 1850.0.

D = mean declination of the middle of the zone for 1850.0, supposing the refraction at the commencement of the zone to remain constant.

D - D + 30' - n' - n''.

i =the micrometer interval, or $\delta = (D + 30'.)$

 δ = difference between the declinations of the star and of the middle of the zone.

 ρ differential refraction for $\Delta \delta$.

 $M\delta$ = reduction to the mean place for 1850.0.

 $\Delta M \delta$ = change in the value of $M \delta$; answering to $\Delta \delta$.

 $\Delta \rho =$ correction for change of refraction during the observations.

 ΔR . Correction for change of reading in the circle.

r. Reduction to the meridian.

We shall have—

$$\delta = -(D + i + (\rho + \mathbf{n}') + (M\delta + \mathbf{n}'') + \Delta M\delta + \Delta \rho + \Delta R + r.)$$

Of these quantities, D, i, r, are determined from the observations; $M\delta$, $\Delta\rho$, and ΔR , depend upon the time; and ρ and ΔM d upon $\Delta\delta$.

The process of reduction will be better understood from the following example of Zone III:

(A.)

		FROM REFRACTION TABLES.	
Circ. R'g	$ \begin{array}{r} 359 59 58.79 \\ 40^{7}.070 = -2.41 \\ 83 38 55.60 \\ 51 6 20.75 \\ - 32.15 \end{array} $	At. ther. 51°.3 " t. 0.00189 " " t. — 4.8 — Ex. ther. 41°.8 " T. 0.04748 " " T. — 5.0 — " R. 2.62369 " " \$\frac{1}{2} \frac{1}{2} \frac{1}	- 0.22 - 4.93
D.	-44 23 30.0	R == 491".99	

(B.) VALUE OF INTERVALS OF THE TRANSIT WIRES IN ZONE III.

	I.	II.	III.	IV.	v.	VI.	VII.	10.	11.
Rev.	s. 46.91	s. 31.24	s. 15.73	s. -0.04	s. 44.67	s. 29.10	s. 13.70	s. 51.02	s. 35.03
10	.83	.15	.69	.04	.71	.14	.77	.03	.12
20	.75	.06	.66	.04	.74	.16	.84	.04	.25
30	.67	30.97	.62	.04	.77	.18	.90	.06	.36
40	.60	.88	.59	.04	.80	.22	.96	.12	.49
50	.52	.78	.56	.04	.84	.29	.05	.23	.67
60	.44	.69	.54	.04	.87	.38	.15	.35	.88
70	.36	.60	.52	.04	.91	.48	.27	.49	36.12
80	46.29	30.57	15.50	-0.04	44.94	29.57	13.39	51.64	36.36

These values are derived from those given at page vII, by multiplying these last into the secant of 44° 53′ 28″.3, the declination of the middle of the zone.

Reductions to the mean place for 1850.0, for the declination — 44° 53′ 28″.3, and the right ascensions following:

(C.)

α.	Ma.	$M\delta$.	Δ
h. m. 9 20	+6.706	-32.15	4.76
10 0	6.869 7.059 7.279	36.91 41.33 45.43	9.18 13.28
40	7.526 7.797	49.11	16.96 20.22
20	8.092	55.24	23.09 25.47
12 0	8.407 +8.741	57.62 59.53	-27.38

(D.) CORRECTIONS DEPENDENT ON TIME.

	IN	RIGHT ASCE	NSION.			IN DECL	INATION.	
α.	K.	I.	Mα.	$\Sigma \Delta \alpha$.	ΔR .	Δho .	$M\delta$.	$\Sigma \Delta \delta + n'$.
h. m. 9 20 40 10 0	+67.838 .840 .851 .862	+1.209 .209 .209 .209	+6.714 6.878 7.069 7.291	+75.761 75.927 76.129 76.362	.00 0.78 1.56 2.34		- 0.28 5.03 9.43 13.52	n—4.49 — 4.77 11.07 17.01 22.65
40 11 0 20 40	.872 .883 .894 .904	.209 .209 .209 .209	7.540 7.812 8.108 8.424	76.621 76.904 77.211 77.537	2.74 2.75 2.77 2.79	3.06 3.83 4.60 5.37	17.17 20.41 23.26 25.62	27.46 31.48 35.12 38.27
12 0	+67.915	+1.209	+8.759	+77.883	-2.81	-6.13	-27.50	-40.93

 ${\it Ma}$ and ${\it M\delta},$ in the above table, are corrected for the error of the clock K.



(E.) corrections dependent on $\Delta \delta.$

	3 TO A TO	Δ Μα.	•		Construction of the Constr	ΔΝ	1 δ.				
	9h.	10h.	11h.	12h.	9h.	10h.	11h.	12.0.	ΔΙ.	ρ.	$(\rho + n''.)$
Rev.	s. -0.044	s. -0.038	s. -0.030	s. -0.019	+0.040	+6.027	+0.008	.000	s. +0.007	-26.81	-52.81
10 20	.033 .022	.028	.022	.015	.030 .020	.020			.005	19.84	45.84
30	011	009	008		+.010	+.007			+.004 + .002	13.08 6.44	39.08 32.44
40	.000	.000	.000	.000	.000	.000	.000	.000			26.00
50 60	+ .011 $.022$	+ .009 $.019$	+ .008 $.015$	+0.010	-0.010 0.020	-0.007 0.012			002 .004	+6.32 12.44	19.69 13.56
70	.033	.028	.022	.015	.030	.020			.005	18.43	7.57
80	+0.044	+0.038	+0.030	+0.019	0.040	0.027	-0.008	.000	-0.007	+24.34	- 1.66

The tables containing the corrections $\Sigma \Delta a$, $\Sigma \Delta \delta$, were interpolated as follows:

(F.)

α.	$\Sigma \Delta a$.	Diff. for 10m.	$\Sigma \Delta \delta + n''$.	Diff. for $10m$.
h. m. 9 20 30 40 50 10 0	+75.761 .841 .927 76.023 .129 .242	-0.080 .086 .096 .106	- 4.77 7.97 11.07 14.08 17.01 19.86	-3.20 3.11 3.07 2.93 2.85
20 30 40	.362 .487 .621	.120 .125 .134	22.65 25.15 27.46	2.79 2.50 2.31 2.11
50 11 0 10 20	.760 .904 77.055 .211	.144 .151 .156	29.57 31.48 33.25 35.12	1.91 1.87 1.77
30 40 50 12 0	.371 .537 .708 +77.883	.160 .166 .171 +0.175	36.77 38.27 39.68 -40.93	1.65 1.50 1.41 —1.25

The manner of determining the quantities i and r, the micrometric interval, and the reduction to the meridian depending merely upon the readings of the micrometer, require no explanation. These being obtained, the mean right ascension of any observed star for 1850.0 will be $= T + \Sigma \Delta \alpha + \Delta M \alpha + \Delta I$; the quantity $\Sigma \Delta \alpha$ being taken from Table F, and $\Delta M \alpha$ and ΔI from Table E.

In like manner, the mean declination for 1850.0 of an observed star, will be

$$= - (D + i + r (+ \rho + n' + \Delta M \delta) + (\Sigma \Delta \delta + n'')$$

 $(\rho + n')$ and $\Delta M \delta$ being taken from table E, and $(\Sigma \Delta \delta + n'')$ from table F.

In the tabulated results, the sum of all the corrections to the observed right ascension is designated by a; and in the corrections to the observed declination,

$$i + r + (\rho + n' + \Delta M \delta) = D$$
: and $(\Sigma \Delta \delta + n') = d$.

EXPLANATION OF THE PRINTED OBSERVATIONS.

At the head of each zone is placed, the number of the zone; the date of the observations; the initial of the observer's name; (H for Professor Hubbard, M for Lieutenant Maynard;) the value of D, and of the constants n' n'', above described.

In the body of the page, the first column from the left hand contains the number of the star in the zone, and the second column its magnitude.

The next nine columns, headed "seconds of transits," exhibit the seconds by the clock, at which the star passed the wires as numbered.

The twelfth column, headed T, shows the clock time of the transits reduced to the mean wire.

The thirteenth column, headed a, contains the sum of the corrections for reducing T to the mean right ascension for 1850.0.

In the fourteenth column, headed Micrometer, the roman numeral indicates the transit wire at which the declination of the star was observed. It is the argument for obtaining the reduction to the meridian. The second number is that of the micrometer wire used in observing the declination, and the following numbers show in revolutions and parts the position of that wire on the scale.

The fifteenth and sixteenth columns contain the reductions, which being added to D, give the mean declination of the observed star for 1850.0. In these reductions using the previous notation—

$$D = i + r + (\rho + \ln' + \Delta M \delta.)$$

d = $(\Sigma \Delta \delta) + \ln''$.

The two last columns show the resulting mean right ascensions and declinations for 1850.0.

The letters B, M, Z, on the right hand of the page, indicate that the stars against which they are placed may be found either in the catalogue of the British Association, the Madrass catalogue of Taylor, or in the catalogue of Argelander's Southern Zones. The asterisks on the left hand margin refer to notes at the end of the volume. And in regard to them, it is proper to state that the hand-books of the observers contain many notes relative to the state of the weather; to errors of reading which have been corrected by reference to the context; to groups and colors of stars; and other incidents which have been omitted, as not affecting the results.

At the bottom of every page, in which a zone is commenced, are given the readings of all the instruments, the circle, barometer, and thermometers, with the times at which they were taken; also, under the head of "corrections," the corrections for error of the clock, and their rates; the quantities m, n, c, used in determining the corrections for errors of azimuth, level, and collimation; also the zenith point and micrometer coincidence.

The reduction of these observations was commenced in the year in which they were made, and, under the direction of Professors Hubbard and Major, the observations had been copied from the observing-books, and the intervals of the transit wires, as also the reductions to the mean places for 1850 had been computed for each zone. The time of transit over the mean wire, designated by T, had also, for the greater part of the work, been determined.

On resuming the work in 1859, the reductions for all the zones, as before described, were computed and tabulated by myself. I also applied these reductions to the first twenty-six zones—completing the work thus far. While thus engaged, Professor Pendleton had revised and corrected the values of T found previously. He also computed this quantity for the zones where it had been omitted; and, from the twenty-sixth zone to the end, he applied



the corrections, thus finishing the whole work. To insure as great accuracy as our means permitted, we both revised these parts of the first computation.

It will be perceived that a very considerable portion of the zones now published are in high south declination. The reason for observing them first has been that they require a more favorable atmosphere, will probably present the greatest difference of results, and demand more frequent observation to arrive at the necessary accuracy of determination. And here it is proper to state that, in these more southern zones, the estimates of magnitude, which are those of the observer at the time, will always depend upon the kind of weather in which they were made, and be on this account uncertain. In other respects, the present publication gives all the data from which the results have been derived, so that each observation may be computed separately—thus affording a check upon the more general methods described in the first part of this letter. The discrepancies between the results of observations of the same star made here, as well as those which have been discovered in comparisons with other catalogues, will be the subject of future examination. Such of them as have probably been occasioned by misreadings of the micrometer are mentioned in the notes at the end of the volume.

Very respectfully,

JAS. FERGUSON,

Assistant Astronomer.

NATIONAL OBSERVATORY, October 1, 1860.

						$oldsymbol{D}$ is the	declination of t	ne middle	e o:	f the	Zon	es.				
	***				$D = -2\mathring{4} 56$.									$D = -28 ext{ } 56.$		
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ZONES OF STARS

OBSERVED WITH

THE MERIDIAN CIRCLE

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THE NATIONAL OBSERVATORY.

1846.

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$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	pril 13, at	10h.	+67	.851	+ 0.00	32 +	s. -0.521	s. -0.	342	s. -0.246	359° 59′ 58″.79	r. 40.070	Zone		1	1 1	1		29.996		41.8
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:	ude.	- Constitution	SEC	CON	DS OF	TRAI	NSI'	rs.	A	man of the estate in construction are signed and						Mean	Right	Mea	ın So	uth
Number.	Magnitude	ı.	11.	III.	ıv. v	. VI.	vII.	10.	11.	т.	a.		MICROMETER.	D.	d.	H	ension,	1	clinati 50.0.	ion,
				Z	Zone III	. A ₁	pril]	13.	н.	D = -44	23′30.′).	n'. == -449.	n'. = -26.0	0. (Co	ntinued	.)			
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	L		1		!!	Zone I	v.	A_1	oril 13	. н. <i>1</i>). = -4	3° 38	8 20.0. n.=	-8.26. n.				<u> </u>		***************************************
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 †17	7 9 7 9 8.9 8.9 8 8 9 7.8 9 9.8.9		17.43 21.83 18.03 31.34 2.51 38.55	86.4 66.2 13.2 32.3 36.8 33.5 16.3 18.0 	12.0 27 52.0 7 11.5 27 59.0 14 48.0 3 52.0 7 48.5 4 2.0 17 33.3 48 9.0 24	.0	57.3			14 9 49.05 11 11.88 13 51.88 15 11.64 17 58.81 20 47.83 33 52.01 34 48.62 41 1.85 44 33.24 45 9.11 45 6.01 47 19.26 54 36.50 57 20.40 15 0 37.73 1 27.58	80 80 80 80 80 80 80 80 81 81 81 81 81	.00 .02 .08 .20 .26	V. 1 40.195 IV. 5 48.313 " 2 38.292 " 1 35.200 " 1 39.973 " 4 41.000 " 5 42.315 " 3 41.702 " 2 49.332 " 4 46.570 " 4 45.610 VI. 2 49.410 " 1 39.580 IV. 2 37.750 " 6 40.546 " 1 45.290 " 2 40.270	51 6.22 19 39.22 46 16.31 54 1.49 51 13.96 29 46.98 23 9.16 35 23.59 39 49.39 26 31.67 27 5.34 39 46.46 45 36.31 46 35.00 15 21.36 48 7.70 45 6.97	7.49 7.39 7.14 7.04 6.80 6.55 5.23 5.13 4.43 4.01 3.93 3.94 3.66 2.73 2.35 1.93 1.81	1: 1. 1: 2: 3: 3: 4: 4: 4: 4: 4: 5: 5: 5:	1 9.40 2 32.23 5 12.31 6 32.10 9 19.32 2 8.37 5 12.81 6 9.45 2 22.79 5 54.23 6 30.11 6 27.03 8 40.34 5 57.70 8 41.66 1 59.05 2 48.91	43 58 44 24 44 33 44 29 44 6 44 1 44 13 44 18 44 4 44 5 44 24 43 53 44 26	33.7 3 6.6 4 43.4 2 28.5 5 40.7 3 13.5 6 5 6 5 29.2 3 10.4 3 59.9 4 57.7 3 43.7 6 29.6 5 28.7	11 m. 55 3 B. 6 3 M. 9 2 M. 92 8 7 0 7 3 1
2 3 *4 5 6 7 8 9	8 8 10 4	37.7	53.0 36.25 40.05 45.5 41.05 6.52 8.82	8.0 52.0 55.0 1.0 56.0 22.3 23.6 	27.8 43 23.5 38 7.1 22 10.5 26 29.5 44 16.2 31 11.1 26 38.0 53 39.0 54 27.0 .	5 54.0 1 38.0 0 41.0 5 0.0 3 46.5 1 41.5 3 8.5 0 9.5 	9.0 56.5 15.0 57.0 24.0		[M. D 9 15 27.85 40 23.44 48 7.12 54 10.53 10 5 29.47 25 16.11 53 11.16 11 3 37.77 23 39.00 36 26.96 43 21.70 11 52 13.74	16. 16. 16. 16. 17. 17. 17.	.18 .41 .44 .52 .65 .84 .19 .32 .62 .81	00.0. n. == IV. 3 35.16 7 38.63 2 46.73 5 46.07 7 46.14 5 40.00 6 45.90 1 37.62 6 41.56 1 40.31 5 46.62 7 43.46	-9.44. ". = 39 14.36 10 33.32 41 20.19 20 58.32 6 11.23 24 30.86 12 14.63 52 38.07 14 46.91 51 4.60 20 42.03 7.44.18	= -23″.00. 13.81 20.55 22.50 24.11 26.79 31.30 37.03 38.95 42.31 44.24 45.18 46.32	40 44 50 10 22 51 11 22 30	5 44.03 0 39.85 8 23.56 4 27.05 5 46.12 5 32.95 3 28.35 3 55.09 3 56.62 6 44.77 8 39.62 2 31.80	44 34 44 44 44 14 44 14 14	2 28.1 3 53.8 4 42.6 4 22.4 3 38.0 3 2.1 5 51.6 5 17.0 3 29.2 4 48.8 4 27.2 30.5	7 в. 9 в. 3 2 6 6 2 2 4
			1		CO	RRECTI	ons			1				INSTRU	MENT RE	ADINGS		1		
			COR.		HOURLY COR.	m,	1	n.	c.	ZENITH POINT.	coinc.			Α.	B. C	1	Mean.	BAR.	THER	Ex.
	13, at 1 15, at 1	2h	s. +67.8 + 8.2 Zone IV	214	s. + 0.032 + 0.004	+0.521	0.	342	s. +0.246 +0.246	359°59′59″.08 0 0 0.94	r. 40.070 40.075		he IV.—April 13, 14. 15. 15. 16 V.—April 15, 9.3 11. 12. 14. 15. 16. 16. 16. 16. 16. 16. 16. 16. 16. 16	2 276 50 54.0 0	4.0 7.5 58 9. 54.5 58	5 7.2 2 52.4 	5.07 6.62 54.77 	1. 30.082 30.084 30.235 30.282 30.320 30.350	45°.5 44.5 56.0 52.0 51.0 47.5 46.0	35.8 34.0 50.0 43.0 40.5 38.5 38,5



ن ا	ıde.	<u> </u>	SE	CON	DS C	F T	RAN	ISIT	'S.	BC-2.230000								ı	Mean	Right	 Mea	n So	uth
Number.	Magnitude.	ı.	п.	III.	IV.	v.	VI.	vII.	10.	11.	Т.	a.		MICROMETER	•	D.	d.		Asce 1850	ension,	Dec 185	linati 0.0.	on,
					Zone	v.	Ap	ril 15	5.	м.	D. =:—43	53 00.0).	n.=-9.44.		n. == -23 ["] .09.	. (Conti	nued.))	1		
13 14 15	7.8 6 7.8	$11.5 \\ 32.0$	$27.0 \\ 48.0$	$\frac{42.5}{3.5}$	31.0 58.0 19.0	13.5	50.0	44.5	• •		h. m. s. 11 59 30.97 12 2 58.05 24 18.86	+18 18 18	.18 .24 .60	r. IV. 1 40.6 " 2 46.5 " 2 42.57		-50 54".08 41 30.10 43 50.83	-47." 47.	61 65	12 3 24	49.15 16.29 37.46	37	$17.7 \\ 40.4$	1 м. 8
16 17 18 19 *20	$\begin{vmatrix} 6 \\ 8.9 \\ 9 \\ 6.7 \\ 6.7 \end{vmatrix}$	7.8	$\begin{vmatrix} 3.0 \\ 23.2 \\ \end{vmatrix}$	18.5 38.7	54.0 34.0 54.0 	49.0 9.1	4.5 24.5	20.5 40.0	12.0	26.5	13 4 54.03 14 33.92 18 53.93 21 2.33 32 12.52	19 19 19 19	.52 .60 .64	" 4 42.16 III. 1 36.25 IV. 5 41.86 10. 1 39.30 IV. 1 42.53		29 7.42 53 26.43 23 26.63 51 38.20 49 46.32	51. 52. 52. 52. 52.	22 30 33	14 19 21	13.36 53.44 13.53 21.97 32.35	47 17 45	59.4 18.6 18.9 30.5 38.6	5 3 3
21 22 23 24	6.7 3.4 6.7 4.5	2.5	35.5 18.0 18.5	50.6 33.0 34.0	26.2 6.3 49.0 49.0	$\frac{21.4}{3.3}$	$37.0 \\ 19.0 \\ 19.5$	$51.8 \\ 34.0 \\ 35.0$		• •	34 26.19 49 6.20 14 5 48.44 10 49.09	19 20 20 20	.15 .46 .56	VI. 2 37.51 VI. 7 39.20 " 5 41.49 " 3 41.34		46 44.59 10 13.59 23 38.93 35 37.81	52. 52. 51.	12 51 29	49 14 6 11	9.65	4 17 29	36.9 5.7 30.4 29.1	1 4 0 в.
25 26 27 28 29	$\begin{vmatrix} 3.4 \\ 3.4 \\ 4.5 \\ 7 \\ 7 \end{vmatrix}$	2.3	38.0	58.0 53.5 33.2	49.0	28.0 24.0 2.5 3.5	 40.0 18.0 19.0	33.3			16 11.46 16 13.14 20 9.06 21 47.46 35 48.52	20 20 20 21	.75 .74 .01	VII. 3 36.31 11. 2 35.22 IV. 2 40.55 V. 6 42.20 VI. 5 47.92		38 27.88 48 3.62 44 58.88 14 24.20 19 53.17	51. 51. 50. 50. 49.	00 77 66	16 20 22	32.12 33.81 29.81 8.20 9.53	38 8	18.8 54.6 49.6 14.8 42.7	2 5 6 м.
30 31 32 33 34	9 8 6 3 7		18.0 53.5	33.5		 23.8 40.0	39.2 55.4	$54.5 \\ 10.5$			42 1.59 45 48.63 46 8.64 58 24.51 15 1 6.95	21 21 21	.13 .19 .19 .46	IV. 5 40.36 III. 7 37.52 V. 6 36.58 IV. 2 35.20 " 2 34.34		24 17.34 11 12.00 17 41.18 48 6.28 48 36.54	49. 48. 48. 47.	74 71 46	46 46 58	9.82 9.83 45.97 28.45	5 11 41	6.4 0.7 29.8 53.7 23.7	4 9 4
35 36 37 38	7.8 3 8.9 6	53.7	31.5 9.0 4.0	47.0 24.5 19.3	2.2	17.5 55.0 50.0	32.8 11.2 5.3	48.1			11 2.19 12 9.48 17 40.01 21 34.61 25 12.83	21 21 21 21	.66 .66 .80 .86	" 4 41.17 10. 6 41.17 IV. 2 34.55 " 3 35.13 " 4 34.0		29 42.10 14 59.02 48 29.30 39 15.45	47. 46. 45. 45.	36 69 20 68	11 12 18 21	23.85 31.14 01.81 56.47	23 8 42 33	28.4 44.7 14.5 0.1	6 1 0 3
39 40	8.9	20.6			25.7	41.5		12.0	 A	.pril 3	15 29 25.93	i	.99	" 3 37.64		33 53.34 37 47.13	44. 43. —12.0	61		34.75 47.92	44 31	37.6 30.7	
	10 10 8.9 9 10 8 10		37.2	54.0 22.5	16.0: 48.3 8.4: 538.0	2.8 23.3	37.5	52.2	7.8	22.5 22.0	11 4 16.05 8 6.00 9 48.39 10 2.50 18 2.64 23 8.55 29 37.52 35 42.31	17 17 17 17 17 17	.58	IV. 4 41.02 II. 5 47.08 IV. 6 44.37 10. 2 39.06 10. 6 44.18 IV. 1 40.65 10. 5 49.53 V. 5 45.24	30 70 30 31 50 38	29 36.44 20 16.38 13 5.28 45 30.82 13 10.48 50 30.93 18 50.01 21 20.22	10. 10. 11. 11. 12. 13.	86 12 15 33 03 89	10 10 18 23 29	33.57 323.58 5.96 20.08 320.35 26.28 55.37 6 0.24	40 50 40 41 40 34 41 6 40 34 41 11 40 40 40 42	27.2 16.4 41.9 22.8 43.9 3.9	4 0 7 1 6 0
9 10	8.9					21.2	11.4 36.0	51.0			44 42.62 11 45 7.04	i		VII. 7 50.36 VI. 3 41.08		3 43.55 35 32.70	15. 15.	70	11 45	0.69 25.09	40 24 40 56		
			cor	TO	Hour				T		ZENITH						CIRC					THER	MOM.
			CLC		COR	- 1	<i>m</i> .	n		с.	POINT.	COINC.				Λ.	в.	с.	D.	Mean.	BAR.	At.	Ex.
April 1	6, at 1	2h	+ 8	.190	+ 0.0	006 +	s. -0.521	s. 0.:	342	s. ⊢0.246	359 59 59".96	r. 40.062	Zon		h. 11.0 12.3 14.4 15.2	280° 21′ 5″.3 5.3 0.1 5.1	6.8 • • • 0.4 5.1	11.2 5.5 10.1	8.4 2.5 7.2	7 ["] .92 • 2.12 6.87	1. 30,338 30,320 30,308 30,300	51.0 50.1 48.8 48.0	46.4 45.0 43.1 42.1
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tude.		s	ECOI	NDS	OF	TRA	NSIT	s.									Right	1	ın Sc	
Magnitude.	ı.	11.	III.	IV.	v.	VI.	vII.	10. 11.	T.	a.		MICROMETER.	D.	d.		Asc 1850	ension,	1	clinat 50.0.	ion,
				Zone	e VI	. A	A pril 1	6. H	D. —40° 5	21 0.0.	n.	=-9″.61.	″. ≕—1≝́.00.	((Contir	nued.)				
11 9					52.9	2 7.0			h. m. s. 11 46 37.80	+18.	06	vI. 2 39.045	-45 32 ["] .73	-15	87		m. s. 3 55.86	41 (5 48 ["] .6	30
2 8.9				1	1	459.8			47 30.84	1	9	V. 2 43.473	42 58.79	15	P		7 48.91	41 4	4 14.7	
$\begin{vmatrix} 13 & 8.9 \\ 4 & 10 \end{vmatrix}$	9 3.	318.	32.8			516.0 34.2			53 47.14 56 5.00	1	8	V. 3 36.165 V. 4 38.248	38 24.45 31 12.91	16. 16.			4 5.30 5 23.20	1	941.0 229.7	
5 10		. 38.	452.5		1	36.5	,		12 5 7.22	1	- 8	V. 3 38.862	36 55.15	17.			5 25.55	1	3 12.7	
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$egin{array}{c c} 7 & 8 \\ 8 & 9. \end{array}$						$\begin{array}{c} 315.5 \\ 40.0 \end{array}$			11 46.56	i		V. 7 39.051	10 16.91	18.		19		1	1 35.1	
$\begin{vmatrix} 3 & 3 & 3 \\ 9 & 7 & 3 \end{vmatrix}$						59.6			15 11.27 16 30.56			III. 3 34.310 V. 7 36.765	39 28.61 11 36.46	18. 18.	1		5 29.76 5 49.06	1) 47.0 2 55.0	
8.8		1	1	1	ì	7.2			21 38.39	1	H	V. 4 35.398	32 52.08	18.			1 56.97	1	1 10.9	
ı 8	35.	5 50.	4.8	18.8	33.	547.8	2.5		14 3 19.02	20.	20 I	V. 3 42.511	34 43.58	18.	70	14 :	39.22	40 56	3 2.2	28
2 7.8	8	. 38.	3 53.2	7.8	22.	5 37.0			5 7.80	1		V. 2 37.390	46 30.30	18.			5 28.04	1	7 48.8	
3 10	- 1		0 48.4			31.5			7 2.76	ì		V. 7 38.460	10 37.52	18.			23.01	i	55.9	
$\begin{bmatrix} 10 \\ 5 \end{bmatrix}$	8 58	- 1	1			55.0 11.8		• • • •	14 26.11 25 42.56	20.		VI. 7 36.414 IV. 4 40.312	11 48.59	17.		$\frac{1}{2}$	46.48	1	6.5	
$\begin{bmatrix} 1 \\ 5 \end{bmatrix} \begin{bmatrix} 1 \\ 9 \end{bmatrix}$	1					030.0			38 0.39	20.		" 3 35.871	$\begin{bmatrix} 30 & 1.24 \\ 38 & 34.27 \end{bmatrix}$	16. 15.			$\frac{3}{8}$ $\frac{3.13}{21.17}$	1	1 18.2 9 50.0	
7 10		$\cdot \cdot $			١	1	52.5		40 9.00	1		" 1 38.500	51 45.71	15.			29.83	1	3 1.2	
3 9			41.7	1	į.			$ \cdot $	44 56.17	20.		I. 5 41.590	23 26.71	14.			5 17.04	1	441.6	
$\begin{array}{c c} 9 & 9.1 \\ 0 & 10 \end{array}$	10	- 1	::		58 ($\begin{vmatrix} 37.0 \\ \cdot \end{vmatrix}$	1		45 8.46 51 44.23		E .	VII. 7 41.100 IV. 1 37.620	$\begin{array}{ccc} 9 & 5.41 \\ 52 & 16.08 \end{array}$	14.			5 29.33 2 5.25	1	20.3	
						1				1	ı		1	14.					30.2	
1 10 2 9			27.8			11.8	- 1	1.3 36.0	51 42.57 52 16.02	21. 21.		" 1 38.082 VI. 2 41.190	$52 0.12 \ 44 17.91$	$\frac{14}{14}$.		55	$2 3.59 \\ 2 37.04$		3 14.3 5 32.0	
3 9		1	::					0.835.2	53 15.74	21.		" 5 48.682	19 20.57	13.	R		36.74	1) 32.0) 34.5	
1 7.	8	$\cdot \mid \cdot \cdot$		1	28.8	342.2			55 14.04	21.	02	IV. 7 43.858	7 30.19	13.	2		35.06	1	3 43.9	
5 10	• •	1	19.8	1			00.0	• • •	58 34.51	21.	- 8	III. 1 41.772	49 51.61	13.	8		3 55.64	1	4.9	
$\begin{bmatrix} 6 & 10 \\ 7 & 10 \end{bmatrix}$	44	3 59.		52.5 $ 28.4 $			- 1		59 52.49 15 3 28.13	21.	8	IV. 6 41.195 " 3 43.095	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	13. 12.) 13.59 3 49.31	1	8.6	
8 7.	1	1				320.8			5 51.57	21.	ä	IV. 3 42.680	34 37.48	12. 12.	8		3 49.31 3 12.80	1	5 35.8 5 49.8	
9 10	22.	2 37.					.		8 5.91	21.	9	II. 4 40.643	49 29.95	12.			3 27.16	1	41.9	
$0 \mid 8$	_ •	$\cdot \mid \cdot \cdot$	1			226.2		$ \cdot \cdot\cdot $	7 57.07	21.		IV. 7 40.945	9 11.03	12.			3 18.29	1	23.0	
1 6.	7 5.	0	34.0		2.4	1 17.0	• • •		15 19 48.32	21.	41	" 6 35.072	18 28.27	10.	35	15 20	9.73	40 39	38.6	2
		****			7	Zone V	711.	April 17	. M. D.	=-39°	20 1	0.0. n.=-	-375. n	=—12	.00.					
1 7.8	8 34.	5 48.	3.3	17.5	31.	5	0.0		9 20 17.36	17.	07	IV. 4 38.45	31 5.91	3.	86	9.20	34.43	39 51	19.7	7
2 4				31.5	45.	59.8	14.0	$\cdot \cdot \cdot \cdot $	24 31.14	17.	10	" 4 42.97	28 28.92		89		48.24	39 48		
3 7	54		100 5			34.5 6.5		$\cdot \cdot $	26 5.73	1		VI. 3 35.02	39 2.87		30		22.82		18.1	
$\begin{array}{c c} 1 & 6 \\ 5 & 6. \end{array}$		-	23.0	1	1	35.0	40.0		$oxed{49\ 37.91} 10\ 7\ 6.28$	17.5		IV. 2 37.27 10. 6 39.40	$\begin{array}{c c} 46 & 33.04 \\ 15 & 56.57 \end{array}$	10. 14.	- 1		55.13	8	553.9 521.3	
6.		1			l				7 15.96	1		10. 6 43.30	13 38.12	14.	- 1		33.55	ā	21.3	
				-	COR	RECT	ions.						INSTRU	MENT	REA	DINGS	•			_
		1	. TO	HOUR		m.	n.	С.	ZENITH	COINC.				CIR	CLE.			BAR.	тнег	eм
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il 17, a	t 12h.,	+	s. 3.564	+0.	008	$^{s.}_{+0.521}$	s. _0.34	$2 \begin{vmatrix} s \\ +0.246 \end{vmatrix}$	o° 0′ 1″.89	r. 40.078	Zone `	NII.—April 17, 9.	281° 21′ 5″.2	6.8	10.8	9.2	8.00	1. 30.200	61°.0	6
			† Zon	e VI,	41	Cloudy	•													
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ber.	Magnitude.		SECO	NDS (OF TRA	NSI	TS.		T.	a	nydddiadau arufu di		D.	d.	Н	Right	1	an Sc	
Number.	Magı	1.	п. ш	. Iv.	v. vi.	vii.	10.	11.	ч. о	a	•	MICROMETER.	υ.	α,	1850	ension,	1	clinat 50.0.	10n,
		1	· · · · · ·		Zone	7111.	A	pril	17. M.	D.=-	-28°	58′ 50″.0. n′.=	1.10. n	= <u>-2</u> 80					
1 2 3 4	7.8 7.8 7.8 5		15.	$\begin{bmatrix} 3.5 \\ 0.14.5 \\ 0.27.7 \end{bmatrix}$	27.240.0 $40.153.0$	52.5 52.5		• •	h. m. s. 11 11 48.94 26 3.62 32 14.64 39 27.71	+18 18 18	s. 1.46 1.55 1.57	r. IV. 6 37.92 10. 4 38.88 III. 1 33.08 I. 4 44.16	-16 44".78 30 40.70 54 35.60 27 38.72	- 1".41 4.94 5.72 6.61	11 19 26 32	n. s. 2 7.40 6 22.17 2 33.21 0 46.36	29 53	5 36".1 9 35.0 3 31.3 5 35.3	54 32
5 *6 7 8 9	8 5 7.8 7.8 8	47.5	15.027.	7 25.2 	$egin{array}{ccccc} & 50.3 \\ & 52.6 \\ 27.0 & 39.7 \\ 52.5 & 5.5 \end{array}$	$ \begin{array}{c} 3.0 \\ 5.0 \\ 52.5 \\ 18.0 \end{array} $			46 12.22 51 25.27 52 27.08 54 14.51 12 12 40.20	18 18 18	.72 .76 .75 .76	IV. 7 39.79 I. 6 41.00 IV. 6 38.22 VI. 2 35.48 11. 2 38.27	9 49.03 14 57.97 16 34.41 47 20.89 45 43.49	7.33 7.89 7.98 8.16 9.74	46 51 52 54	30.94 44.03 45.83 33.27 59.12	1; 1; 4;	3 46.3 3 55.8 5 32.3 6 19.0 4 43.5	36 z. 86 z. 39
*10 11 12 13 14	7 8 8 6.7 3		4.8 18. 16.5 29. 11.0 23. 21.5 34.	$131.8 \\ 542.0 \\ 536.0$	54.5 7.6 48.5 1.5	14.5		• • •	15 38.15 19 30.67 22 41.98 24 36.10 12 30 46.57	19 19 19	.95 .00 .00 .04 .09	I. 4 37.60 11. 6 38.71 IV. 1 37.82 " 6 42.77 " 3 38.63	31 25.42 16 16.27 51 51.86 13 57.11 36 46.80	9.94 10.22 10.42 10.52 10.88	19 23 24	5 57.10 9 49.67 8 0.98 55.14 5.66	30 13 50 15	0 25.3 5 16.4 0 52.3 2 57.6 5 47.6	36 z. 19 28 z. 33 z.
					Zone I	X.	Apr	il 17	. M. D.	=-2	8° 57	' 20.0. n.'=-	–27.19. n.	=-3.00.	l		<u>l</u>		,
1 2 3 4 *5 6 7 8 9 10 11 12 *13 14 15 16 17 18 19 20 21 22 23	8 7.8 8 7.8 8 4 7.8 5.6 8 7	41.0 59.0 21.5 31.0 12.5 16.0 19.0 29.0 19.2 58.5 49.5	41.0 53.6 43.5 56.3 25.3 37.7 28.5 41.6 31.5 44.5 41.5 54.6 31.5 44.5 	8 19.0: 4 11.0; 5 36.0; 1 36.5; 0 38.5; 0 59.5; 0 20.5; 6 6.2: 3 9.1; 7 50.2; 0 53.5; 5 56.4; 0 12.5; 0 36.5; 0 12.5; 0 36.5; 0 28.0; 0 34.4; 0 58.5;	31.5 44.6 23.4 36.6 49.0	57.00 14.5 37.00 46.5 28.00 31.5 34.00 58.5 			15 30 6.43 32 19.09 36 10.88 39 36.25 42 36.78 47 38.60 49 59.45 53 20.72 16 4 6.38 7 8.97 10 50.38 14 53.72 21 56.66 29 27.26 34 6.59 50 57.00 51 20.59 55 12.64 58 36.59 17 8 27.81 10 34.61 13 58.66 17 25.06	21 21 21 21 21 21 21 21 21 21 21 21 21 2	.95 .01 .03 .09 .10 .16 .19 .24 .35 .34 .36 .41 .47 .55 .76 .83 .86 .93 .90	V. 6 43.88 II. 2 45.15 VII. 3 39.71 VI. 2 36.18 IV. 4 43.00 VII. 3 40.84 " 2 46.04 " 1 36.26 " 1 38.12 10. 5 40.01 VII. 7 37.19 10. 5 41.65 VII. 7 37.08 " 3 33.54 V. 5 46.60 I. 4 41.87 10. 4 40.22 VII. 1 38.71 VI. 1 41.88 VII. 2 39.67 VI. 6.41.21 II. 2 43.14 I. 2 37.98	13 18.95 41 46.98 36 9.39 46 56.96 28 19.34 35 30.27 41 16.09 52 45.80 51 41.51 24 13.87 11 18.66 23 7.25 11 22.44 39 42.79 20 27.63 29 32.51 29 54.62 51 21.11 49 31.67 44 56.58 14 51.02 42 56.45 45 54.65	26.18 25.92 25.49 25.11 24.74 24.15 23.84 21.99 21.55 21.03 20.45 19.42 18.29 17.54 14.72 14.65 13.97 13.35 11.59 11.22 10.58 9.93	32 36 39 42 47 50 53 16 4 7 11 15 22 29 34 51 55 58 17 8 10 14	27.38 240.10 31.91 57.34 257.88 59.76 20.64 41.96 27.73 30.31 11.74 15.13 48.81 28.18 18.75 42.35 34.47 58.45 49.74 56.51 20.63 47.07	39 33 44 20 33 38 50 49 20 50 27 18 27 48 40 42 40	1 5.1 32.5 32.5 4.4 42.6 3.1 4.4 4.6 3.1 4.4 4.6 3.1 4.7 4.7 4.7 4.7 4.7 4.7 4.7 4.7	00 z. 09 z. 09 z. 07 08 02 03 02 05 06 0 z. 09 07 08 07 08 07 07 08 07 07 08 08 07 07 08 08 08 08 08 08 08 08 08 08 08 08 08
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				c	CORRECT	ions		~~~					INSTRU	MENT REA	·			1	
			COR. TO	HOURI COR.		,	ı.	c.	ZENITH POINT.	COINC.			Δ.	B. C.	D.	Mean.	BAR.	THER	Ex.
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49 50	8				1.015 25.840	$5.4 \\ 5.0 54.7$		1 1	50 0.88 12 50 25.63	1	.80 .81	" 6 38.12 VII. 4 37.49	16 40.60 31 36.71	57.5 57.5	R	50 20.68 50 45.44	į.	27.8 5 23.9	
			7	-	CC	RRECTIO	ons.		1				INSTRU	MENT	READIN	ss.			
			COR.	- 1	HOURLY	m.	n.	c.	ZENITH POINT.	COINC.				CIR	CLE.		BAR.	THEF	RMOM.
			0,000											в.	C. D	Mean.		At.	Ex.
April	19, at 1		s. +8.9 At 17.		+0.010	$\begin{pmatrix} s, \\ +0.521 \end{pmatrix}$ ent disturb	s. -0.345	<u> </u>		r. 40,080	Zon	h. ne XI.—April 19, 9.6 10.9 11.5 13.7 16.6 16.5 16.8	21.0	52.0 25.6 24.6 25.7	55.0 50.0 28.0 23 27.0 22 26.5 24	1 24.42 1 23.42 	1. 30.302 30.332 30.343 30.362 30.384	65.0 63.5 62.0 60.0 58.5	65.1 57 0 54.0 49.5 48.5 46.5

er.	tude.		$_{ m SE}$	CON	DŞ (OF '	TRA	NSI	rs.							Mean Right	Mean South
Number.	Magnitude.	I.	11.	111.	ıv.	v.	vi.	vII.	10.	11.	Т.	а.	MICROMETER.	D.	d.	Ascension. 1850.0.	Declination.
				2	Zone	XI.	A	.pril :	19.	М.	$D = 39^{\circ} 52^{\circ}$	50.0.	n'.== -10".00.	n'.== -0'.22	. (Con	tinued.)	
51	8						52.0	7.0			h. m. s. 12 51 23.29	+19.82	VII.2 31.51	-49 ['] 51 ["] .30	—57 .30	h. m. s. 12 51 43.11	40° 43′ 38″.60
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56	7.8	41.5	د. د		25.0		1	8.3			13 0 31.09 2 24.89	19.96 19.99	I. 5 33.68 VI. 2 42.57	27 59.90 43 27.36	57.67 57.73	13 0 51.05 2 44.88	21 47.57 37 15.09
57	8	40.5			24.0						5 23.81	20.04	I. 4 38.36	31 6.56	57.83	5 43.85	24 54.39
5 8	8				43.6						$6\ 43.56$	20.06	III. 5 35.33	27 3.18	57.87	7 3.62	20 51.05
59	7	• •					21.0				751.54	20.08	VI. 3 41.07	35 31.07	57.90	8 11.62	29 18.97
60	7	22.0	36.5	50.8	5.6	19.1	34.0	48.6	• •		$9 ext{ } 5.26$	20.09	I. 4 39.86	30 14.34	57.95	9 25.35	24 2.29
61	9	57.5									17 41.06	20.23	I. 2 41.28	44 15.25	58.06	18 1.29	38 3.31
62	4	$ \cdot\cdot $					22.5				17 53.35	20.23	IV. 1 42.97	49 7.06	58.07	18 13.58	42 55.13 r
63	7	$ \cdot\cdot $	٠.				52.4		• •		22 23.41	20.30	" 1 33.17	54 47.92	58.24	22 43.71	48 36.16 M
64 65	$\frac{7}{7.8}$	$ \cdot\cdot $	• •				$\frac{3.0}{38.5}$		• •		24 33.80	20.34	" 3 35.19	38 55.57	58.28	24 54.14	32 43.85 M 7 45.43
66		58.2					11.0				28 9.13 33 41.72	20.38 20.50	VII. 6 42.82 IV. 2 40.58	13 57.11 44 36.74	$58.32 \\ 58.30$	28 29.51 34 3.22	38 25.04 n
67	8		10.0	~			13.0	1 1			34 43.92	20.50	VII. 2 46.05	41 26.08	58.29	35 4.43	35 14.37
63	8							50.8			36 7.54	20.53	" 2 50.18	39 3.61	58.28	36 28.07	32 51.89
69	8	$ \cdot\cdot $					26.5				49 57.40	20.72	" 6 40.46	15 19.42	57.95	50 18.12	9 7.37
70	8.9	21.0	35.7	50.0	4.5	18.3	33.1	• •	• •		53 4.25	20.77	" 7 36.93	11 29.24	57.83	53 25.02	5 17.07
71	9								4.8	19.3	53 59.81	20.83	V. 1 34.52	54 0.53	57.79	54 20.64	47 48.32
72	4			19.0	33.5	48.0	2.5	17.0			56 33.52	20.84	IV. 4 33.93	33 40.84	57.70	56 54.36	27 28.54
73	8	• •	54.0	8.3	22.0					[14 3 22.51	20.93	I. 6 43.16	13 45.39	57.42	14 3 43.44	7 32.81 1
74	9	• •	• •	• •			24.4		• •		3 55.60	20.95	VII.3 42.70	34 34.10	57.40	4 16.55	28 21.50
75 76	7.8 8	$ \cdot\cdot $	94 0	• • 40 0			$\frac{36.0}{32.3}$		• •	• •	5 6.93 8 3.45	20.98 21.01	" 5 35.69 IV. 6 39.44	26 50.08	57.34	5 27.91 8 24.46	20 37.42
77	8		34.0				$\frac{32.3}{24.0}$			• •	9 55.07	21.01 21.02	VII.5 44.41	15 55.34 21 47.45	$57.20 \\ 57.11$	10 16.09	9 42.54 r 15 34.56
78	9	l i	33.0		2.0						13 2.02	21.14	IV. 1 43.35	48 53.99	56.93	13 23.16	42 40.92
79	9						54.0	1 1			14 25.06	21.13	VI. 2 49.68	39 21.15	56.86	14 46.19	33 3.01
80	6	$ \cdot\cdot $					$ \cdot\cdot $	47.0			15 4.04	21.11	VII.6 48.93	$10\ 25.25$	56.81	15 25.15	4 12.06 1
81	5.6		44.0	58.3	12.4	27.0					21 12.53	21.21	1. 6 38.10	16 41.28	56.44	21 33.74	10 27.72
82	8.9				21.3						27 21.21	21.31	VII.6 42.49	14 8.94	55.98	$27\ 42.52$	7 54.92
83	7						56.8				30 27.82	21.36	III. 6 36.29	$17\ 44.56$	55.73	30 49.18	11 30.29
84	8							12.0		• •	33 28.74	21.42	II. 4 41.78	29 7.94	55.47	33 50.16	22 53.41
85 86		$\frac{31.0}{17.8}$							- 1	• •	$38 \ 14.33$ $42 \ 1.15$	21.50 21.54	I. 4 41.67 " 6 37.10	29 11.68 17 15.99	55.04	38 35.83 42 22.69	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
1		12.5						44.3		::	42 1.13	21.63	" 1 39.69	51 1.53	54.40	42 22.09	44 45.93
[8			- 1	! 1			1			45 8.81	21.62	11. 3 39.245	36 32.60	54.38	45 30.43	30 16.98
89	8						44.8		1]	14 53 15.55	21.76	V. 2 36.535	46 57.16	53.54	14 53 37.31	40 40.70
90		• •	• •	• •	• •		$ \cdot\cdot $	• •	• •			• • • •	VI. 5 43.50	22 17.29			16
91							$ \cdot \cdot $		18.6	3.0	14 55 13.70	21.77	10. 3 42.15	34 52.54	53.33	14 55 35.47	40 28 35.87 1
92		• •				18.5					58 3.85	21.81			53.02	58 25.66	
1	3.4	• •	• •	• •	• •	• •	• •	- 1	11.8	H	58 7.53	21.79	10. 7 45.94	6 15.83	53.02	58 29.32	39 59 58.85 1
94	8	• •	• •	• •	- 1	• •	• •	٠. ا		2.0	59 52.42	21.85	11. 2 44.42	42 21.45	52.82	15 0 14.27	40 36 4.27
1	8 6	!	28.0	· · · 42.5	56.8	11.0		25.0	i	• •	$\begin{array}{cccc} 15 & 1 & 41.96 \\ & 7 & 56.74 \end{array}$	$21.84 \\ 21.97$	11. 6 41.26 I. 3 39.11	14 50.20 36 40.20	$52.60 \\ 51.85$	$egin{array}{cccccccccccccccccccccccccccccccccccc$	40 8 32.80 40 30 22.05 m
	4			- 1				28.6	- 1		8 45.20	21.97 21.95	VI. 6 41.72	14 35.76	51.75	9 7.15	40 50 22.05 M
	2		42.0					53.5			11 10.59	21.98	IV. 7 35.39	12 23.09	51.45	11 32.57	40 6 4.54 1
99	6							- 1	4	9	11 22.94	21.99	11. 6 35.96	17 57.26	51.43	11 44.93	40 11 38.69 m
00	7		8.5	22.3	36.5				• •	• • •	17 36.75	22.08	III. 7 32.17	14 14.77	50.58	17 58.83	40 7 55.35
c1	9								18.0	2.5	18 13.46	22.10	10. 6 34.50	18 45.59	50.50	18 35.56	40 12 26.09
1	6	1	1	- 1		- 1	35.0	- 1	- 1		23 6.52		IV. 7 48.50	4 48.46	49.83	23 28.66	39 58 28.29
.03	2									Į.	15 24 47.57	22.23	VI. 1 48.65	45 49.74	49.59	15 25 9.80	40 39 29.33 в

	m. s. 26 45.21 27 11.44 36 58.24 37 18.37 44 15.13 44 17.22 45 59.92 49 51.02 50 46.68 54 6.28 54 41.22 56 22.18 59 37.50 1 5.21 9 43.61 13 22.01 19 20.22	Declination, 1850.0. 40° 33′ 22″.76 м. 40° 30′ 57.78 м. 40° 44° 31.83 40° 33° 16.42 40° 40° 27.80 40° 43° 22.86 40° 15° 27.93 40° 13° 10.72 40° 0° 25.54 40° 25° 21.64 40° 19° 9.12 40° 16° 49.08 40° 39° 32.21 40° 43° 0.52 в. 40° 26° 37.01
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	m. s. 26 45.21 27 11.44 36 58.24 37 18.37 44 15.13 44 17.22 45 59.92 49 51.02 50 46.68 54 6.28 54 41.22 56 22.18 59 37.50 1 5.21 9 43.61 13 22.01	40 30 57.78 м. 40 44 31.83 40 33 16.42 40 40 27.80 40 43 22.86 40 15 27.93 40 13 10.72 40 0 25.54 40 25 21.64 40 19 9.12 40 16 49.08 40 39 32.21 40 43 0.52 в. 40 26 37.01
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	26 45.21 27 11.44 36 58.24 37 18.37 44 15.13 44 17.22 45 59.92 49 51.02 50 46.68 54 6.28 54 41.22 56 22.18 59 37.50 1 5.21 9 43.61 13 22.01	40 30 57.78 м. 40 44 31.83 40 33 16.42 40 40 27.80 40 43 22.86 40 15 27.93 40 13 10.72 40 0 25.54 40 25 21.64 40 19 9.12 40 16 49.08 40 39 32.21 40 43 0.52 в. 40 26 37.01
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	36 58.24 37 18.37 44 15.13 44 17.22 45 59.92 49 51.02 50 46.68 54 6.28 54 41.22 56 22.18 59 37.50 1 5.21 9 43.61 13 22.01	40 44 31.83 40 33 16.42 40 40 27.80 40 43 22.86 40 15 27.93 40 13 10.72 40 0 25.54 40 25 21.64 40 19 9.12 40 16 49.08 40 39 32.21 40 43 0.52 B. 40 26 37.01
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	37 18.37 44 15.13 44 17.22 45 59.92 49 51.02 50 46.68 54 6.28 54 41.22 56 22.18 59 37.50 1 5.21 9 43.61 13 22.01	40 33 16.42 40 40 27.80 40 43 22.86 40 15 27.93 40 13 10.72 40 0 25.54 40 25 21.64 40 19 9.12 40 16 49.08 40 39 32.21 40 43 0.52 B. 40 26 37.01
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	44 15.13 44 17.22 45 59.92 49 51.02 50 46.68 54 6.28 54 41.22 56 22.18 59 37.50 1 5.21 9 43.61 13 22.01	40 40 27.80 40 43 22.86 40 15 27.93 40 13 10.72 40 0 25.54 40 25 21.64 40 19 9.12 40 16 49.08 40 39 32.21 40 43 0.52 B. 40 26 37.01
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	44 17.22 45 59.92 49 51.02 50 46.68 54 6.28 54 41.22 56 22.18 59 37.50 1 5.21 9 43.61 13 22.01	40 43 22.86 40 15 27.93 40 13 10.72 40 0 25.54 40 25 21.64 40 19 9.12 40 16 49.08 40 39 32.21 40 43 0.52 в. 40 26 37.01
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	49 51.02 50 46.68 54 6.28 54 41.22 56 22.18 59 37.50 1 5.21 9 43.61 13 22.01	40 13 10.72 40 0 25.54 40 25 21.64 40 19 9.12 40 16 49.08 40 39 32.21 40 43 0.52 в. 40 26 37.01
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	50 46.68 54 6.28 54 41.22 56 22.18 59 37.50 1 5.21 9 43.61 13 22.01	40 0 25.54 40 25 21.64 40 19 9.12 40 16 49.08 40 39 32.21 40 43 0.52 в. 40 26 37.01
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	50 46.68 54 6.28 54 41.22 56 22.18 59 37.50 1 5.21 9 43.61 13 22.01	40 0 25.54 40 25 21.64 40 19 9.12 40 16 49.08 40 39 32.21 40 43 0.52 в. 40 26 37.01
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	54 6.28 54 41.22 56 22.18 59 37.50 1 5.21 9 43.61 13 22.01	40 25 21.64 40 19 9.12 40 16 49.08 40 39 32.21 40 43 0.52 в. 40 26 37.01
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	54 41.22 56 22.18 59 37.50 1 5.21 9 43.61 13 22.01	40 19 9.12 40 16 49.08 40 39 32.21 40 43 0.52 B. 40 26 37.01
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	59 37.50 1 5.21 9 43.61 13 22.01	40 39 32.21 40 43 0.52 в. 40 26 37.01
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1 5.21 9 43.61 13 22.01	40 43 0.52 в. 40 26 37.01
118 8 6.5 21.0 35.0 49.5 4.2 9 20.76 22.85 " 4 34.97 33 4.72 42.29 119 8	9 43.61 13 22.01	40 26 37.01
119 8	13 22.01	i
120 7		
121 9 28.5 57.0 12.0 20 42.84 22.99 VI. 5 38.22 25 22.60 40.14	19 20.22	40 42 58.82
10.11		40 46 20.52 м.
$oxed{122} oxed{8} oxed{ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \$	21 5.83	40 18 52.74
	22 21.64	40 42 23.10
	23 17.01	40 26 44.57
	26 11.00	39 59 11.02
	32 32.07	40 19 39.00
	34 20.05	40 33 2.43 в.
	37 28.42	40 41 30.61
128 8 · · 29.5 · · · · 12.5 · · 41.0 · · · · 16 38 57.99 23.19 II. 6 48.28 16 33.01 36.39 16	39 21.18	40 9 59.40
Zone XII. April 20. H. D. = -43 22 30.0. n. = -3.15. n. = -20.00		
1 7.8 36.451.8 6.5 22.2 37.2 52.8 8.0 9 40 22.18 17.66 III. 2 46.750 41 16.98 3.27 9	40 39.84	44 3 50.25 в.
12 20.00	44 3.73	43 32 59.12
	47 20.63	43 52 52.21
	53 26.90	44 14 18.24 м.
$oxed{5 \mid 9 \mid \dots \mid \dots \mid 42.8 \mid 58.0 \mid 13.8 \mid \dots \mid 10 \mid 5 \mid 27.75 \mid 17.88 \mid " 3 \mid 39.070 \mid 36 \mid 53.42 \mid 9.71 \mid 10}$	5 45.63	1
$\left[\begin{array}{cccccccccccccccccccccccccccccccccccc$	8 48.46	43 43 27.99
	15 14.48	43 47 10.69
	17 27.61	43 29 4.25
	21 18.64	43 34 45.79
11 10	24 32.49	43 35 29.41
	25 18.75	43 48 46.75
1 10 10	26 8.09 34 43.93	43 50 47.06 44 15 55.68
10.11 100.010 55 5.20 10.40 10	34 40.30	44 15 55.00
INSTRUMENT READIN	G.	
CIRCLE.		THERMOM.
A. B. C. D.	Mean.	At. Ex.
† Zone XII.—Clouds. Zone XII.—April 20, 9.5 277° 21′ 2′4 6.8 13′.0 7′.	0 7″30	ı. 30.338 66.0 60.0
10.5 0.9	1 6	30.332 64.4 58.5

Number	Magnitude.	SECOI	NDS OF	1 1		11.	т.	a.		MICROMETER.	D.	d.	Mean Right Ascension, 1850.0.	Dec	n South
Z	E	.	.	. ,,,											
	1		Z	one XII	II. A	April 20). H. <i>I</i>	0.=-	40°5	0 50.0. n.=	—30.23. n		0.	1	
1 2 3 3 4 4 5 6 6 7 8 8 9 10 11 12 13 14 15 16 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 29 30 31 32 33 34	10 7.8 10 8 5 10 10 10 9 7.8 9.10 8 10 10 10 8 5.6 5 10 10 7.8 4 10 7.8 4 10 7.8 9 10 7.8 10 10 10 10 10 10 10 10 10 10 10 10 10	18.5 7.0 21.8 36 16.0 32	6			28.4 	h. m. s. 10 41 24.51 47 37.58 47 52.62 47 55.03 49 32.67 50 49.64 52 58.33 55 0.40 58 37.08 11 0 47.91 9 50.89 22 45.91 23 22.21 28 51.66 34 48.36 37 47.21 45 36.54 46 56.03 46 7.96 50 55.67 53 45.93 55 34.79 12 0 6.00 5 6.21 7 25.58 11 49.52 12 52.34 15 9.78 16 52.94 21 50.84 25 17.65 25 24.61 27 40.92 30 21.27	+18 18 18 18 18 18 18 18 18 18 18 18 19 19 19 19 19 19 19 19 19 19 19 19 19	.52 .53 .53 .54 .56 .58 .59 .66 .66 .79 .92 .93 .03 .03 .23 .24 .32 .36 .36 .36 .44 .51 .54 .66 .66 .66 .38 .38 .38 .38 .39 .39 .30 .30 .30 .30 .30 .30 .30 .30 .30 .30	VII. 2 43.012 I. 5 43.335 IV. 5 43.420 11. 3 40.590 VI. 4 42.213 V. 5 42.652 IV. 3 43.848 " 1 41.278 " 6 41.993 II. 2 42.710 I. 6 40.150 II. 4 43.860 IV. 6 41.900 II. 6 40.932 III. 5 39.200 " 5 41.775 " 5 45.580 IV. 2 44.960 VII. 2 54.995 VI. 6 38.128 II. 7 42.950 IV. 2 41.582 II. 7 42.950 IV. 2 41.582 II. 7 45.078 IV. 7 45.560 I. 6 45.013 " 6 40.693 V. 1 37.910 II. 7 40.728 " 1 42.720 I. 6 42.575 " 6 40.702 V. 3 42.270 III. 3 37.800 I. 2 38.598	- 43 18.00 22 29.06 22 26.61 35 51.85 28 57.87 22 53.04 34 0.12 50 13.10 14 30.26 43 28.68 15 33.89 28 0.48 14 33.47 15 6.92 24 53.24 23 23.57 21 11.48 42 10.66 36 20.92 16 44.67 8 3.57 44 8.46 6 49.66 6 33.25 12 45.06 15 15.15 52 10.17 9 20.72 49 22.59 14 9.68 15 14.53 34 55.11 37 30.52 45 51.54	-30".55 31.86 31.91 31.92 32.25 32.50 32.92 33.32 34.04 34.44 36.12 38.34 40.68 41.79 41.89 42.52 42.87 43.11 43.70 44.29 44.58 45.17 45.28 44.80 44.90 45.18 45.36 45.49 45.62	h. m. s. 10 41 42.95 47 56.10 48 11.15 48 13.56 49 51.21 51 8.20 53 16.91 55 18.99 58 55.74 11 1 6.57 10 9.68 23 4.83 23 41.17 29 10.69 35 7.45 38 6.35 45 55.77 47 15.27 46 27.20 51 14.99 54 5.29 55 54.15 12 0 25.44 5 25.72 7 45.12 12 9.12 13 11.95 15 29.44 17 12.61 22 10.59 25 37.45 26 44.41 28 0.75 30 41.14	41 13 41 27 41 20 41 14 41 25 41 41 41 5 41 16 41 16 41 14 41 13 41 27 41 8 40 59 41 35 40 58 40 58 41 4 41 6 41 43 41 0 41 40 41 5 41 6 41 26 41 29	38.55 50.92 48.52 13.77 20.12 15.54 M. 23.04 B. 36.42 54.30 M. 53.12 0.01 28.82 1.90 M. 36.25 23.48 54.25 43.27 42.64 52.81 17.19 36.44 41.57 B. 23.36 7.54 19.64 M. 55.52 43.27 42.64 52.81 53.12 44.86 44.87 85.81 86.45 86.45 87.40 86.45 86.45 86.45 86.45 86.45 86.45 86.45 86.45 86.46 86.47 86.47 86.48 86.49 86.40 8
1	$\begin{bmatrix} 8 & 3 \\ 9 & 9.10 \\ 4 & 10 & 1 \\ 7.8 & 4 \\ 9 & & \end{bmatrix}$	$egin{array}{cccccccccccccccccccccccccccccccccccc$	3 21.2 36 0 49.0 3 5 30.0 44 4 54.0 8 8 26.0 41 0 10.0 24 6 34.0 48	.0 51.0 .2 18.0 3 .2 1 .5 23.1 3 .0 55.3 1 .2 39.0 5	5.0			19 . 19 . 20 . 20 .	.87 .96 .01 .05 .12		45 51.54 23 21.24 23 57.47 13 40.94 37 0.14 14 30.75 49 53.01	45.62 45.84 46.00 46.08 46.25 46.33 46.32	30 41.14 36 8.66 39 49.97 42 14.10 46 46.33 48 30.06 12 51 53.78	41 37 41 14 41 15 41 5 41 28 41 6	
		COR. TO	HOURLY	RRECTIO	ons.		WENTER		-		INSTRU	MENT RE.			THERMOM.
		CLOCK.	COR.	<i>m</i> .	n.	c.	ZENITH POINT.	coinc.			Α.	В. С.	D. Mean.	BAR.	At. Ex.
April April	20, at 12 <i>h</i> 20, at 15 <i>h</i>	+9.353 	+0.008	+0.521	s. _0.342	+0.246	0° 0′ 0′.46 0.95	7. 40.083	Zone	e XIII.—April20, 10, 11, 12, 12, 12, 13, 14, 14, 15, 16, 17	.7	59.5 64. 57.5 63. 59.2 64.	56.60	1. 30.304 30.286 30.284 30.276 30.244 30.240 30.228	62.0 55.1 60.6 54.4 60.5 53.5 59.0 51.3 58.4 50.1 58.0 49.8 57.7 48.5

er.	itude.	SEC	ONDS	OF TRA	ANSIT	rs.						Mean Right	Mean South
Number.	Magnitude.	I. II. I	ıı. ıv.	v. vi	. vii.	10. 11.	Т.	a.	MICROMETER.	D.	d.	Ascension, 1850.0.	Declination, 1850.0.
				·								U .	I
	ı	, 	Zone X	CIII.	April 9	20. H	$D = -40^{\circ}$	50″50.0.	n'. == -30'.23.	n".=-15		Continued.)	
41 42	10 8.9	$\begin{bmatrix} . & . & . \\ 2.0 & 16.8 & 3 \end{bmatrix}$		37.052.			h. m. s. 12 56 22.82	s. + 20.27	V. 7 45.567	-6'32'.66	-46.39	h. m. s. 12 56 43.09	40° 58′ 9″.05
43	i	24.539.053	1		1 1		$\begin{array}{c} 14 \ 30 \ 46.24 \\ 36 \ 8.47 \end{array}$	21.80 21.88	III. 2 43.830 IV. 2 50.060	42 50.21 39 13.21	42.20 41.61	14 31 8.04 36 30.35	41 34 22.41 41 30 44.82
44	8	31.0 43	5.0 59.2	14.0 28.	5		37 59.56	21.90	II. 7 43.280	7 52.16	41.40	38 21.46	40 59 23.56
45		24.4 39.3 53					40 8.32	21.94	IV. 5 44.872	$21 \ 35.94$	41.17	40 30.26	41 13 7.11
$\frac{46}{47}$		52.2 7.02			4 20.2	• • • •	44 36.21	22.01	" 3 43.484	34 13.01	40.64	44 58.22	41 25 43.65
48	5.6	$\begin{vmatrix} 24.0 & 38.6 & 53 \\ & 34.0 & 48 \end{vmatrix}$		$\begin{vmatrix} 22.2 & 37. \\ 17.4 & 32. \end{vmatrix}$			$\begin{array}{cccc} 47 & 7.96 \\ 49 & 3.12 \end{array}$	22.05 22.09	" 2 48.461 " 3 36 198	40 8.99	40.34	47 30.01	41 31 39.33
49	9		.8 59.2		1 1		50 59.24	22.09	" 3 36.198 " 1 41.971	38 26.44 49 48.94	40.10 39.86	49 25.21 51 21.37	41 29 56.54 в. 41 41 18.80
50	10	1 1 1		43.5 58.			51 29.05	22.14	V. 5 44.223	21 58.83	39.80	51 51.19	41 13 28.63
	10			1.	0		51 31.62	22.11	VI725		39.80	51 53.73	
52	9	1 1			_	20.4 35.0	52 15.07	22.20	10. 6 42.600	14 7.77	39.70	52 37.27	41 5 37.47
53 54	10 10		0.825.5	40.055.	3 1	• • • •	56 25.48	22.24	IV. 3 40.343	36 2.25	39.15	56 47.72	41 27 31.40
55	7.8			$\begin{bmatrix} 7.5 \\ 5.0 \end{bmatrix}$.			57 53.10 15 5 50.68	22.31 22.37	" 2 39.995 " 7 49.340	$egin{array}{cccc} 45 & 3.54 \ 4 & 21.78 \end{array}$	38.94	58 15.41 15 6 13.05	41 36 32.48
56	8.9			16.0	1		7 1.42	22.57	" 4 39.202	30 42.82	$\frac{37.85}{37.67}$	7 23.99	40 55 49.63 в. 41 22 10.49
57	7.8	14.6 29.2 44	.0 58.4	13.028.			19 58.53	22.56	" 4 36.310	32 23.49	35.63	20 21.09	41 23 49.12 м.
58	9.10	1 1 1		• • • •		28.0 42.4	20 22.48	22.59	10. 6 38.178	16 41.66	35.59	20 45.07	41 8 7.25
59 60	$\begin{array}{c} 10 \\ 8.9 \end{array}$	$\begin{vmatrix} . & . & . & . \\ . & . & 35.0 \end{vmatrix}$				12.5 28.0	22 7.12	22.62	VII. 6 37.198	17 16.51	35.29	22 29.74	41 8 41.80
00	0.3	33.0 43	.5 5.0	10.033.	0 40.0		$25 \ 4.28$	22.66	IV. 7 42.442	8 21.27	34.82	25 26.94	40 59 46.09
61	8.9			59.3			27 45.42	22.68	III. 6 45.755	12 19.32	34.40	28 8.10	41 3 43.72
62		29.8 44.5 59					29 13.44	22.71	IV. 6 42.082	14 27.15	34.13	29 36.16	41 5 51.28
$\frac{63}{64}$	9		_1	21.035.	1 1		30 6.10	22.72	VII. 3 40.932	35 41.12	33.99	30 28.82	41 27 5.11
65	7.8	43.0 57.2 12	- 1	8.022.	1 1		33 27.05 33 53.60	22.76 22.77	IV. 2 48.118 " 4 42.380	40 20.73 28 52.32	33.42	33 49.81	41 31 44.15
66		56.011.025	i				36 40.31	22.11	II. 1 37.810	52 14.15	$\frac{33.32}{32.87}$	$34\ 16.37$ $37\ 3.14$	41 20 15. ² 64 м. 41 43 37.02
67		59.4 14.5 28	.5 43.5	58.013.	0 27.0		38 43.44	22.85	IV. 4 43.722	28 5.45	32.51	39 6.29	41 19 27.96
68	9	1.6 16.0 30					47 45.15	22.97	II. 5 44.270	$21\ 56.79$	30.90	48 8.12	41 13 17.69
69 70	$\frac{6}{8.9}$	$\begin{bmatrix} . & . & 26.0 & 40 \\ 48.4 & 3.8 & 18 \end{bmatrix}$		10.024.			48 55.04	22.99	IV. 4 43.239	27 12.84	30.68	49 19.03	41 18 33.52 в.
						• • • •	56 32.90	23.13	I. 1 44.750	48 12.02	29.23	56 56.03	41 39 31.25
71	9.10						16 11 0.24	23.33	IV. 1 46.680	47 5.65	26.33	16 11 23.57	41 38 21.98 м.
72 73	7.8 8.9	$9.3 24.2 39 \\ 59.0 13.5 28$					$20 53.56 \\ 35 42.76$	$23.45 \\ 23.63$	" 3 37.040	37 57.10	24.25	21 17.01	41 29 11.35
74	9	15.5 45					35 42.76 35 59.72	23.63	I. 4 42.854 VII.5 46.123	28 35.19 20 52.05	$21.00 \\ 20.91$	36 6.39 $36 23.34$	41 19 46.19 м. 41 12 2.96
	10	1 1		1 1	1)	36.451.2	36 30.63	23.66	10. 2 47.492	40 41.49	20.81	36 54.29	41 12 2.96 41 31 52.29 м.
76	9		. 53.0	8.022.	4		38 53.14	23.72	IV. 1 37.810	52 14.07	20.26	39 16.86	41 43 24.33
77	9			29.5			40 0.03	23.70	" 2 44.102	42 40.51	20.02	40 23.73	41 33 50.53
78 79	8	$\begin{array}{c c} . & 10.025 \\ . & 24.038 \end{array}$.039.0	54.0	0 37 0	• • • •	41 39.38	23.73	VI. 2 41.020	44 27.35	19.65	42 3.11	41 35 37.00
80	7.8	1 1		22.036.			41 52.99 43 07.37	$23.73 \\ 23.74$	" 3 32.742 IV. 3 30.180	40 26.39 41 58.36	$19.61 \\ 19.29$	$\begin{array}{c} 42 \ 16.72 \\ 43 \ 31.11 \end{array}$	41 31 36.00 м. 41 33 7.65
81	9					38.5	43 17.98	23.73	11. 4 36.800	32 4.44	19.25	43 41.71	41 23 13.69
82		13.5 28.5 43	.0				47 57.52	23.76	III. 5 48.360	19 34.73	18.17	48 21.28	41 10 42.90
83		24.8 40.0 54					57 8.94	23.89	IV. 3 45.088	33 17.05	15.99	57 32.83	41 24 23.04
84 85	$\frac{9.10}{9}$	24.5 39.0 53 25.5 40					17 0 8.29	23.94	" 3 34.970	39 9.13	15.27	17 0 32.23	41 30 14.40
86	8	. 25.5 40					2 54.71	23.97	" 3 35.287 " 7 45.111	38 58.22	14.59	3 18.68	41 30 2.81
87	9	7.822.536	.5	5.520.	5 35.0		$\begin{array}{c c} 11 & 16.90 \\ 13 & 51.38 \end{array}$	$24.00 \\ 24.08$	" 7 45.111 " 4 39.939	6 48.63 30 17.11	$12.54 \\ 11.88$	$\begin{array}{c} 11 \ 40.90 \\ 14 \ 15.46 \end{array}$	40 57 51.17 41 21 18.99
	10	53.0 23	.0 37.2	51.8 6.0	0 21.0		16 37.21	24.08	" 5 48.128	19 42.80	11.19	14 15.46 17 1.29	41 21 18.99
89	7.8	25.2 40.0 54	.2 9.0	23.5 38.6	052.5		22 8.96	24.13	I. 6 45.556	12 26.03	9.79	22 33.09	41 3 25.82 м.
90	9	12.0 26	.0 41.0	55.3 9.8	8		17 23 40.83	24.16	IV. 5 44.532	21 47.96	9.47	17 24 4.99	41 12 47.43

er.	itude.		SE	CON	DS OF	TRA	NSIT	s.	FD			# Control of the Cont			H	Iean R	_		n So	
Number.	Magnitude.	I.	ıı.	ш.	ıv. v	. уі.	vII.	10. 11.	Т.	a.	•	MICROMETER.	D.	d.		Ascens 1850.0.	' 1		elinati 0.0.	on,
	,	,	,		Z	one X	IV.	May 3.	M. D.	=-49	2° 51′	′ 10.″0. n.′=-	-41. ["] 94. n."	=-4	0.00.	,				
1	8			59.0	14.329	2 44.5			$ \begin{array}{cccccccccccccccccccccccccccccccccccc$.27	I. 1 44.6	-48 ['] 46 ^{''} .17	-41".	54 1	h. m. 16 2 4	s. 3.48	43 40	37″.7	1
2	6.7		56.8		26.541				11 26.41	1	.39	2. 2 47.35	41 13.73	39.		11 5	5.80	43 33		
3	9				16.031			• • • •	13 16.13	1	.41	10 4 39.94	30 40.80	39.	9	13 4		43 22		
4	9 8.9		• •		$43.059 \\ 30.045$			$\cdot \cdot \cdot \cdot $	16 43.68	1	.43	2. 1 43.29	49 31.13	38.	8	17 1		43 41		
5 6	5				57.012				21 30.44 22 56.98	1	.53	I. 4 36.75 IV. 1 39.74	32 33.27 51 36.44	$37. \\ 36.$	8	$21 ext{ } 5$ $23 ext{ } 2$		43 24 43 43		
7	6	: :			20.836				27 21.00	•	.58	I. 6 44.12	13 36.55	36.	į.	23 Z 27 5	1	43 43		
8	9				1 1	1	1 1		31 20.96		.67	" 3 42.11	35 26.07	35.		31 5	1	43 27		
9	9			47.4	2.9 17	.7 33.0			32 - 2.73	29	.67	VII. 4 41.44	30 23.45	35.	i i	32 3	1	43 22		
10	9				50	7 5.8	20.9		36 35.49	29	.76	2. 2 35.76	47 58.48	34.	13	37	5.25	43 39	42.6	1
11	8.5	١			.	. 48.8	4.0		38 18.46	29	.79	III. 1 44.79	48 5.66	33.	75	38 4	8.25	43 39	49.4	1
12	9		1	}	3.518	1	1 1		41 3.23	1	.78	I. 5 39.29	25 13.16	33.	2	41 3		43 16		
13	8		1	15.3	30.7 45	0.6			43 30.44	1	.82	2. 5 36.57	18 5.95	32.	a a	44	1		48.2	
14	8			3	25.5 40	1	1 1		44 25.57	1	.81	VII. 7 36.26	12 16.27	32.		44 5		43 3	58.5	7 в.
15	9				46.5 1			• • • •	48 46.28	1	.85	" 7 44.45	6 55.92	31.		49 1	(42 58		
16	8				16.732			• •] • • •	53 16.98	1	.92	2. 6 44.36	13 27.81	30.		53 4		43 5		
17 18	8.9		20.0		50.0 5 55.5 10			• • • • •	59 50.01 17 0 55.64		.03	2. 5 36.66 VII. 7 39.35	26 44.28	28.	2	17 0 2	,	43 18		
19	9				ll				6 44.51	1	.10	I. 4 36.31	10 28.28 32 48.21	28. 26.			5.65 4.61	43 2 43 24		
20	9	5.8			51.5 6		30.0		12 51.63		.24	VI. 2 36.15	47 45.90	$\frac{20.}{25.}$	1	13 2		43 39		
01	0	1	1	1	1 1										1		1			
21 22	8	1		1	14.629 9.0	1	1	• • • • •	16 14.82	1	.23	1. 4 36.78	32 30.53	24.	2	16 4	The state of the s	43 24		
23	8	::		34.0	$\begin{vmatrix} 9.0 \\ \end{vmatrix}$ 31				19 9.12 19 16.78	1	.31 .23	1. 2 38.98 VII. 6 42.68	$\begin{array}{c cccc} 46 & 5.99 \\ 14 & 26.93 \end{array}$	23. 23.	1	19 3: 19 4	- 1	43 37 43 6		
24	7.8		::	1	45.0 0				27 45.42	1	.31	2. 7 38.32	11 3.59	23. 21.		28 1	- 1	43 2		
25	8.9					. 33.4			28 3.42	1	.32	VII. 7 35.60	12 39.24	21.	8	28 3		43 4		
26	8			48.0	1 1				31 3.22	1	.42	I. 3 37.94	37 51.67	20.	8	31 3	1	43 29		
27	8.9				6.321				34 6.28	1	.46	" 3 33.09	40 41.18	20.	R	34 3	- 1	43 32		
28	8.9			22.3	37.552				35 37.55	30	.46	VI. 4 34.11	33 5.58	19.	57	36		43 24	35.1	5
29	8.9			• •	3	1] [40 48.90	30	.46	I. 6 36.69	17 55.87	18.	20	41 1	9.36	43 9	24.0	7
30	8				17.2 32	0 47.1	2.7	• • • •	17.01	• •		10. 1 44.15	49 1.02	17.	00 .		• •	43 40		
31	8.9				41.556			[51 41.66	30	.62	1. 3 41.34	35 51.84	15.	29	52 13	2.28	43 27	17.1	3
32	4.5	44.0	59.0	14.0	29.344	1]]	$55\ 29.14$	30	.66	2. 3 44.30	34 9.07	14.	26	55 59	9.80	43 25	33.3	3 в.
33	8.9	• •			1 1	. 50.0		• •] • • [56 19.68	1	.67	VII. 4 36.65	32 36.34	14.	03	56 5	0.35	43 24	0.3	7
34	8.9				28.5 43			• • • •	18 1 28.35	1	.65	2. 6 41.89	14 54.00	12.	a	.8 1 5	1	43 6		
35 36	8.7				$28.544 \\ 31.546$			• • • •	2 29.18	3	.68	1. 5 43.60	22 42.47	12.	. fi		9.86	43 14		
37	9				11.025		10.0		4 31.29 12 10.79	ì	.69 .70	I. 5 46.36 V. 7 44.67	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\frac{11}{9}$.	D D	5 12 4	1.98	43 12 42 58		
38	5.6				35.651				20 35.84	1	.70	I. 2 40.96	44 57.41	7.	1	21	1	42 38 43 36		
39	8.9		1		23.038				26 23.09	ł	.84	2. 6 45.01	13 4.97	5.	9	26 5		43 4		
40	6		48.0	2.8	18.033	247.4			28 17.89		.91	I. 4 45.82	27 16.10	5.	3	28 48	1	43 18		
41	8				29.5 45				36 29.81	l	.05	" 1 41.20	50 44.73	2.	Si .	37	1	43 41		
42	8		٠.						36 48.55	1	.06	VII. 1 38.28	52 26.84	2.	7	37 19	1	43 43		
43	5.6		• •	• •	17.0 32	0 47.1	2.2	• • • •	18 38 16.85	31	.06	" 2 41.91	44 24.19	2.	44 1	.8 38 4	7.91	43 35	36.7	3
					CO.	RRECT.	ions.						INSTRU	MENT	READI	NGS.				
			}				1							CIR	CLE.				THER	MOM.
			COR.	- 5	HOURLY COR.	m.	n.	c.	ZENITH POINT.	coinc.			A.	В.	c.	р. М	lean.	BAR.	At.	Ex.
					s.	s.	8.	8.		r.		<i>ħ</i> .						Ţ.		
May 3	3, at 13h		+16	149	+ 0.034	+0.590	+0.4	58 +0.207	0 0 0.31	r. 40,130	Zon	h. ne XIV.—May 3, 16.0 17.1	1	9.7	- 1	ł	b b	30.000 30.000	60.8 59.5	53.0 54.5
						***						18.0	ł	11.0	ı		H	30.000 30.000		53.0
I														1 1		1				

ber:	Magnitude.		SECO	NI	os o	FΊ	'RAN	SIT	s.		т.	a.		MICROMETER.	D.	d.			Right	I	n Sou	
Number:	Magr	1.	11. 11	n.	ıv.	v.	vı.	vII.	10.	11.	-							1850		185		,
-						Z	one X	V.	M	ay 4.	н. Д.	=-28	26	20″.0. n′.=-	-40.00. n.	=-3	563.					
1	9						10.2				h. m. s. 12 2 45.12	+26.		IV. 1 37.078	-52 50 ["] .33	-40.	17	12 3	s. 11.60	29 19		
2	9 9.10		25.037 16.2		$50.0 \\ 41.5$		1 1	27.5 19.0			7 49.95 9 41.30	26. 26.		" 5 47.751 " 5 47.054	$20 \ 20.56$ $20 \ 44.66$	40. 40.	6		$16.41 \\ 7.81$	28 47 28 47		
4	9					45.4	58.4	10.8			10 33.12	26.	53	V. 2 47.223	41 8.09	40.	65	10	59.65	29 8	8.7	4
5 6	$8.9 \\ 9.10$	1	$43.055 \\ 12.024$	- 1			1 1				13 7.76 15 36.97	26. 26.		IV. 4 47.248 " 1 37.290	26 25.15 52 43.03	40.			34.30 3.54	28 53 29 19		
7	8		52.5 5	5.0	17.5	30.2	42.8				17 17.63	1	57	R i	44 3.96	40.			44.20	29 11		
8	9.10		!	- 1			59.0			• •	17 33.94	26.		VII.5 42.991	23 7.48	40.	9		0.52	28 50		
9 10	8 9.10		45.057	- 1			$\frac{35.0}{56.0}$				19 10.04 20 30.55	26. 26.	. 60	IV. 1 45.127 VI. 6 39.748	48 12.22 16 14.33	40.	4		36.63 57.15	29 15 28 43		
*11	8		40.0 .	ł			29.4				21 4.57	26.		" 6 40.710	15 41.34	41.	06		31.17	28 42		
12	7	50.8		5.0	28.2	41.0					24 28.50	26.		IV. 2 38.871	$45\ 56.70$	41.		24	55.13	29 12	57.8	7 z.
13	9.10	1	1 1	- 1			07 0	ı		44.5	24 35.69	26.		10. 5 40.900	24 16.58	41.			2.32	28 51		
14 15	$ 8.9 \\ 9.10$	i .	36.5 49	- 1	- 1	14.4		39.0 30.0			$\begin{array}{ccc} 27 & 1.79 \\ 27 & 53.69 \end{array}$	26. 26.		IV. 1 44.770 VI. 6 35.331	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	41.41.			28.44 20.34	29 15 28 45		
16	7.8	1	35.047	. 1							30 58.83	26.		I. 6 40.740	15 39.92	41.			25.50	28 42		
17	7.8	46.0	1 1		23.5		1 1	$\frac{1.0}{20.0}$			31 23.53	26.		IV. 5 43.508	22 47.51	41.			50.21	28 49		
18 19	$\begin{vmatrix} 8.9 \\ 9 \end{vmatrix}$		1 1	1.0	$\frac{\cdot}{6.2}$		19.5	32.0			31 53.75 34 5.89	26. 26.		VII. 5 47.810 IV. 5 51.132	20 18.21 18 23.81	41.			20.43	28 47 28 45		
20	8.9						44.0				34 18.79	26.		VII. 1 48.602	46 11.81	41.			45.49	29 13		
21	8.9				52.2		17.0				35 52.67	26.	71	IV. 6 44.498	13 30.46	41.	47	36	19.38	28 40	31.9	3
22	8		1 1	- 1	53.0		17.5	1		• •	36 52.76	26.		VI. 4 40.060	30 33.38	41.			19.48	28 57		
$\frac{23}{24}$	$\begin{vmatrix} 9 \\ 7.8 \end{vmatrix}$	1	$\begin{vmatrix} 29.5 \\ 48.0 \end{vmatrix}$. 5	• •		38.0	32.0		$\frac{.}{22.5}$	38 54.45 39 13.15	26. 26.		IV. 6 34.605 10. 4 38.545	$\begin{array}{c} 19 \ 12.17 \\ 31 \ 25.24 \end{array}$	41. 41.			21.19 39.89	28 46 28 58		
25	9	27.5		- 4			30.5			22.5	44 5.25	1		III. 6 44.302	13 37.11	41.			32.02	28 40		
26	7.8					58.0	10.5	23.0			44 45.39	26.		V. 2 40.680	44 54.24	41.			12.17	29 11		
*27 28	8.9		$\begin{vmatrix} \cdot & \cdot \\ 34.446 \end{vmatrix}$				6.0			• •	45 41.07 46 59.22	26. 26.		IV. 7 43.364 " 1 45.038	8 18.87 48 15.32	41.41.			$\begin{array}{c} 7.86 \\ 26.02 \end{array}$	29 35 29 15		
29	9	: :		- 1			28.5				48 3.34	26.		" 2 41.620	46 13.32	41.			30.15	29 11		
30	7.8	• •	57.5 10	0.1	23.0		47.5	٠.		• •	50 22.68	26.	.83	" 2 41.930	44 11.06	41.	61	50	49.51	29 11	12.6	7 z.
31	8.9		.				16.5	29.0			50 51.54	26.	.83	VII. 6 45.478	12 56.27	41.	62	51	18.37	28 39	57.8	9 z.
32	7		22.0 .								54 46.98			IV. 5 40.906	24 17.13	41.			13.84	1		
$\frac{33}{34}$	9 9	$ ^{13.0}$	26.0 38				$\begin{array}{c} 16.0 \\ 2.0 \end{array}$			• •	54 50.81 56 36.76	26. 26.		" 3 40.906 V. 1 40.490	36 0.99 50 52.50	41. 41.			3.64	29 3 29 17		
35	9	: :	:: :				25.4				58 0.33	1		IV. 7 37.702	11 34.10	41.			3.04	28 38		
36	8.9		• • •		10.4	22.6	35.2	48.0			59 10.37	26.		" 7 34.854	13 12.50	41.		59	37.27	28 40		
37 38	9.10	• •	9.221	. 0	34.0		27.5	40.0		• • •	13 0 2.34 4 34.01	26. 26.		VI. 2 36.283 III. 1 39.592	$47 \ 26.00$ $51 \ 23.47$	41. 41.			29.25	29 14 28 18		
39	8.9		58.511	- 1			1 1	1			5 23.66	26.		" 3 38.200	37 34.49	41.			50.61	29 4		
40	8	• •	41.554	1.0	6.5	19.0	32.0	44.2		• •	13 7 6.63	26.	.96	IV. 6 41.178	15 25.15	41.	50	13 7	33.59	28 42	26.6	5 z.
	1	1				cor	RECT	IONS	 -						INSTRU	MENT	REA	DINGS,				
				T				1					-			CIR	CLE.				THER	MOM.
			COR. T		HOUR		m.	1	n.	c.	ZENITH POINT.	COINC.			Α.	В.	c.	D.	Mean.	BAR.	At.	Ex.
				- -				-						7.						, , , , , , , , , , , , , , , , , , ,		
May 4	l, at 12.	.0h	+16.49	95	+ 0.		+0.590) -0°.	458	$^{s.}_{+0.207}$	359° 59′ 59″.41	r. 40.114	Z_0	one XV.—May 4, 12.	0 292 11 54.9		73″.7	1 1	6492		68.0	62.0
		-												13. 14.	1	58.1	71,4	71.2	63.67	30.086 30.086	66.2 65.2	60.2 59.1
														15.	0 51.2	55.2	68.3	67.4	60.52	30.088	64.5	57.5
														17.	51.5	55.1	67.5	69.1	60.80	30.084	63.3	56,5
													l			i	1	1 1	l	l		1

Number.	Magnitude.	SECONDS OF TRANSITS. 1. II. III. IV. V. VI. VII. 10. 11.	т.	a.	MICROMETER.	D.	d.	Mean Right Ascension, 1850.0.	Mean South Declination, 1850.0.
<u> </u>									2000101
		Zone XV. May 4. H.	$D. = -28^{\circ} 26^{'} 20^{''}_{.0}$.		n.'=40.'00.	n" = -35"63. (Continued.		ntinued.)	
41	8.9	15.027.2	h. m. s. 13 8 2.28	+26.97	v. 1 41.518	_50 16.96	4146	h. m. s. 13 8 29.25	29 17 18."42
42	8	$ 17.0 30.0 42.0 55.0 \dots 21.0 \dots \dots $	11 55.02	27.01	IV. 6 34.085	19 30.21	41.38	12 22.03	28 46 31.59
43		$ 51.0 3.8 \dots 29.0 \dots 53.5 6.0 \dots \dots $	$12\ 28.67$	27.01	VI. 7 36.950	11 59.91	41.40	12 55.68	28 39 1.31 z.
44	9	34.0	19 11.87	27.07	IV. 4 34.640	33 49.85	41.21	19 38.94	29 0 42.06
45 46	9 7	7 5 90 9 22 5 45 9 57 4 10 0 22 5	21 1.27	27.08	" 1 41.056	50 32.95	41.15	21 28.35	29 17 34.10
*47	9	$ \begin{vmatrix} 7.5 & 20.2 & 32.5 & 45.2 & 57.4 & 10.0 & 22.5 & \dots \\ 36.0 & \dots & 1.0 & 14.0 & 26.4 & \dots & \dots \\ \end{vmatrix} $	23 45.07	27.10 27.12	" 5 47.580 " 4 48 470	20 26.61	41.04	24 12.17	28 47 27.65 z.
48	7	36.0 . 1.0 14.0 26.4 	25 13.83 $26 6.41$	27.12	" 4 48.470 " 2 45.532	25 43.01 42 6.66	40.99 40.98	25 40.95 26 33.54	28 52 44.00
49	7.8	15.227.5	26 50.17	27.14	VI. 7 41.272	9 30.70	40.93	20 33.34 27 17.31	29 9 7.64 28 36 31.63
50		18.0 30.2 43.0 55.0	28 42.90	27.15	II. 1 38.470	52 2.15	40.88	29 10.05	29 19 3.03 z.
51	7		29 29.94	27.16		<u> </u>			
52	6	17.0 30.2 43.0 33.3	29 50.44	27.16	IV. 3 38.482 VI. 6 42.240	37 24.82 $14 48.28$	40.83 40.81	$\begin{array}{c} 29 \ 57.11 \\ 30 \ 17.60 \end{array}$	29 4 25.65 z. 28 41 49.09
53	8.9	29.8 42.2 55.0	32 7.46	27.18	II. 4 39.140	31 5.23	40.70	32 34.64	28 41 49.09 28 58 5.93 z.
54	8.9		32 20.63	27.18	IV. 2 45.828	41 56.38	40.69	32 47.81	29 8 57.07 z.
55	9		32 44.67	27.18	VI. 1 39.103	51 40.25	40.68	33 11.85	29 18 40.93
56	9	• • • • • • • • 46.0 59.0 18.0 • •	33 21.33	27.19	" 3 45.250	33 30.73	40.64	$33\ 48.52$	29 0 31.37
57	9		33 23.23	27.19	IV. 4 40.114	30 31.80	40.64	33 50.42	28 57 32.44 z.
58	9	$ \cdot\cdot \cdot\cdot $ $ 12.0 24.2 $	34 15.85	27.18	VI. 6 45.620	12 51.53	40.58	34 43.03	28 39 52.11
59 60	9	39.2 51.8 17.0 .	36 51.82	27.21	IV. 5 40.303	24 38.02	40.27	37 19.03	28 51 38.29 z.
			39 24.91	27.24	I. 1 42.712	49 35.37	40.29	39 52.15	29 16 35.66
*61	7	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	39 55.03	27.25	IV. 4 44.238	28 9.29	40.26	40 22.28	$28 \ 55 \ 9.55$
*62	7.8	7.0 20.0 32.5 45.0 57.4 10.0 22.5	41 44.94	27.26	" 2 48.126	40 37.00	40.17	42 12.20	29 7 37.17 z.
63 64	9 8		42 13.38	27.26	VII.1 38.032	52 17.11	40.12	42 40.64	29 19 17.23
65	7.8	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$43 \ 40.68$ $44 \ 52.69$	27.28 27.28	VI. 1 43.088 IV. 1 43.565	49 22.88 49 6.30	40.03	$\begin{array}{c} 44 & 7.96 \\ 45 & 19.97 \end{array}$	29 16 22.91
*66		23.5 36.2 49.0 1.2 13.8 26.2 38.5	47 1.25	27.20	II. 2 45.092	49 0.30	$39.95 \\ 39.80$	47 28.55	29 16 6.25 29 9 21.44
67	9	58.0 23.0	47 10.63	27.30	IV. 6 48.261	11 20.49	39.79	47 37.93	28 38 20.28
68	7	$ \dots \dots \dots $	49 8.32	27.32	" 3 45.318	33 28.60	39.66	49 35.64	29 0 28.26 z.
69	8.9	9.6 22.8 35.0 47.2 $ 12.5 25.0 $ $ $	$51\ 47.44$	27.33	" 6 40.775	15 39.17	39.47	52 14.77	28 42 38.64 z.
70	8.9	23.0 . 47.0	52 35.13	27.33	" 6 44.712	13 23.05	39.41	53 2.46	28 40 22.46
71	9		53 43.96	27.35	V. 6 44.750	13 21.70	39.33	54 11.31	28 40 21.03
72	9		$54\ 27.26$	27.36	VI. 6 40.250	15 57.09	39.27	$54\ 54.62$	28 42 56.36
73	9	52.0 5.0	$54\ 27.26$	27.36	" 6 41.040	15 29.79	39.27	$54\ 54.62$	28 42 29.06
74	8		55 18.82	27.37	10. 2 43.070	43 30.99	39.21	$55\ 46.19$	29 10 30.20 z.
75 76		$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	57 18.11	27.40	IV. 7 39.485	10 32.55	39.06	57 45.51	28 37 31.61 z.
77	9		59 55.39	27.42	I. 5 43.020 IV. 6 39.128	23 3.78	38.87	14 0 22.81 14 1 12.85	28 50 2.65
78		$\begin{bmatrix} & 21.0 & . & . & . & 57.510.223.0 & . & . & . \\ & . & . & . & . & . &$	14 0 45.43 2 11.42	$27.42 \\ 27.44$	" 3 38.433	16 36.05 37 26.56	$\frac{38.81}{38.68}$	14 1 12.85 14 2 38.86	28 43 34.86 29 4 25.24 z.
*79	9		15 0 20.52	27.96	V. 2 44.211	42 52.36	34.54	15 0 48.48	29 4 25.24 z. 29 9 46.90
80	8.9	29.5 42.4 55.0 7.4 20.0 32.8 44.8	4 7.47	27.99	IV. 2 41.190	44 36.78	33.82	4 36.46	29 11 30.60
*81		46.659.211.324.136.349.0	9 24.03	28.04	" 7 44.870			9 52.07	
82		14.0 27.0 40.2 51.8 17.0	$\frac{9}{11} \frac{24.03}{52.00}$	28.06	" 4 37.528	$7 26.56 \\ 32 1.25$	$\frac{33.04}{32.62}$	12 20.06	28 34 19.60 28 58 53.87
83	6.7	33.0 46.0 58.8 11.0 24.0 36.0 48.0	13 11.00	28.08	111. 5 46.538	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\frac{32.02}{32.42}$	13 39.08	28 47 55.09
84	9.10	0 17.5 29.8	13 52.47	28.08	VI. 6 48.890	10 58.63	32.30	14 20.55	28 37 50.93
85	9	$ 51.2 \dots 16.5 \dots 41.5 \dots 6.7 \dots $	16 29.07	28.10	IV. 4 46.344	26 56.65	31.87	16 57.17	28 53 48.52 z.
	10	45.0 23.0	17 57.75	28.12	" 3 45.945	33 7.03	31.62	18 25.87	28 59 58.65 z.
87	8.9	0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0	19 4.91	28.13	" 3 41.522	35 39.89	31.43	19 33.04	29 2 31.32 z.
88 en		33.8 46.2 58.4 11.5	23 11.34	28.16	I. 3 39.280	36 56.98	30.72	23 39.50	29 3 47.70 z.
89 90	$\frac{8.9}{9}$	17.0 42.0 54.8 7.0 36.1 48.6 1.2 13.6 26.2 39.0 51.2	23 29.56	28.17	IV. 2 45.795	41 57.67	30.67	23 57.73	29 8 48.34 z.
			26 13.72	28.19	" 3 38.773	37 14.82	30.19	26 41.91	29 4 5.01 z.
91	9	$ \cdot \cdot \cdot \cdot \cdot \cdot 22.0 35.0 47.3 $	27 9.85	28.19	V. 6 42.573	14 37.00	30.02	27 38.04	28 41 27.02 z.
1	8.9	7 9 7 9 9 0	27 46.47	28.20	VII. 5 45.295	21 45.24	29.93	28 14.67	28 48 35.17 z.
93	9	$ \cdot \cdot \cdot \cdot \cdot \cdot 54.8 7.2 20.0 \cdot \cdot \cdot \cdot $	15 29 42.26	28.21	VI. 2 51.053	38 55.79	29.56	15 30 10.47	29 5 45.35
		3 🛘							



er.	itude.		SE	CON	DS	OF '	TRA	.NSI	rs.		m					Mean Right	Mean South
Number.	Magnitude.	1.	п.	ш.	1V.	v.	vi.	vii.	10.	11.	Т.	a.	MICROMETER.	D.	d.	Ascension, 1850.0.	Declination, 1850.0.
				Z	one I	XV.	Ŋ	Ма у 4	Į.	н.	D.=-28° 2	6 20.0.	n'=-40″.00.	n".==-35".6	3. (Co	ntinued.)	
94	5						24.0				h. m. s. 15 29 58.84	*. +28.21	r. 11. 1 42.150	-49 ['] 54 ^{''} .12	29 ["] .51	$^{h.\ m.\ s.}_{15\ 30\ 27.05}$	29° 16′ 43″.63
95 96	$8.9 \\ 8.9$				44.0			52.0		$ \cdot\cdot $	30 14.19 $31 43.81$	28.21 28.22	VI. 1 44.890 11. 1 41.240	48 20.38 50 25.53	29.48 29.20	$31 \ 42.40$ $32 \ 12.03$	29 15 9.86 29 17 14.73
97	7.8				• •	i	1	31.2			31 53.49	28.22	VI. 5 45.252	21 46.91	29.16	32 21.71	28 48 36.07 z.
98	7.8							36.2			31 58.65	28.22	VII.5 41.870	23 43.63	29.14	32 26.87	28 50 32.77
99	8			- 1		i	6.0	i i			33 41.03	28.25	IV. 6 40.552	15 46.96	28.81	34 09.28	28 42 35.77
100	8.9	1 1	3.0		• •	10.0	$ \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot $	1 1	50.8	3.8	34 54.61 35 57.49	28.26 28.27	10. 2 42.230 IV. 6 37.132	$\begin{array}{ c c c c c c }\hline & 44 & 0.18 \\ & 17 & 45.07 \\ \hline \end{array}$	$28.59 \\ 28.39$	35 22.87 $36 25.76$	29 10 50.77 28 44 33.46
102	8.9	41.05				1	1	57.0			36 19.01	28.28	" 6 41.110	15 27.66	28.33	36 47.29	28 42 15.99
103	9	35.24	7.8	0.8	12.8						38 12.96	28.30	" 5 42.150	23 34.27	27.96	38 41.26	28 50 22.23
104	7.8	42.0 5	5.0	$7.2^{ }_{ }$	20.0	1	44.5	i I			39 19.75	28.31	" 3 44.210	34 7.00	27.75	39 48.06	29 0 54.75
105	9 9	1 1	• •	• •		ı	$\frac{22.5}{6.0}$	34.5		• •	39 57.13	28.32	VI. 4 39.495	30 53.06	27.63	40 25.45	28 57 40.69
106	9		-					48.4			40 40.81 41 10.78	28.32 28.32	IV. 4 40.630 " 3 41.265	30 14.11 35 48.77	$27.49 \\ 27.39$	41 9.13 41 39.10	28 57 1.60 29 2 36.16
108	9	1 1		26.0		ì					42 38.46	28.33	I. 3 38.055	37 39.33	27.08	43 6.79	29 4 26.41
109	9	: 1				7.5	20.0	32.8		$ \cdot\cdot $	$42\ 55.08$	28.34	V. 4 38.548	31 26.03	27.03	43 23.42	28 58 13.06 z.
110	$\frac{9}{7.8}$	$\begin{vmatrix} 13.02 \\ 10.82 \end{vmatrix}$				• •		•	• •		44 50.84 45 48.50	28.36 28.36	I. 6 41.402 IV. 6 47.022	15 17.18 10 54.38	26.64	45 19.20 46 16.86	28 42 3.82 z. 28 37 40.84
1112	5	$\frac{10.02}{32.04}$			•••		34.0	$\frac{\cdot \cdot}{46.8}$			47 9.34	28.37	" 6 44.140	13 42.93	$26.46 \\ 26.16$	47 37.71	28 40 29.09
*113	9	1					1	59.8			47 24.19	28.37	" 6 40.175	15 59.95	26.11	47 52.56	28 42 46.06
114	8	15.42	8.0	10.4	53. 0	5.8	18.2	30.4			49 53.03	28.38	" 2 40.370	45 5.16	25.59	50 21.41	29 11 50.75
115	9	39.05									$52\ 16.57$	28.40	" 1 41.140	50 30.23	25.10	52 44.97	29 17 15.33
116	6.7	1 1						31.5			52 54.07	28.43	" 6 40.278	15 56.42	24.98	53 22.50	28 42 41.40 z.
117	8.9	$\begin{vmatrix} 11.52 \\ 49.0 \end{vmatrix}$		- 1		1	1	$\frac{26.4}{4.2}$			57 49.00 59 26.66	28.46 28.48	" 3 39.242 " 4 45.890	36 58.68 27 12.39	$23.97 \\ 23.54$	58 17.46 59 55.14	29 3 42.65 28 53 55.93 z.
119	8 -	1		23.8			ł	14.0			16 0 36.43	28.49	" 4 47.642	26 11.79	23.34	16 1 4.92	28 52 55.16 z.
120	5.6	8.22	1					22.5			245.59	28.50	VII.3 44.222	34 6.29	22.93	3 14.09	29 0 49.22
*121 122	$\frac{9}{7.8}$	42.0 5				l .	t	$58.0 \\ 29.2$			3 20.12	28.51	IV. 1 43.333 VI. 6 44.950	49 14.48	22.80	3 48.63	29 15 57.28
123	9	3	- 1	17.4	$\frac{\cdot}{0.3}$	13.0	1				$egin{array}{cccccccccccccccccccccccccccccccccccc$	28.52 28.55	IV. 7 38.770	13 14.81 10 57.35	$22.69 \\ 22.23$	$\begin{array}{c} 4 \ 20.16 \\ 6 \ 28.71 \end{array}$	28 39 57.50 z. 28 37 39.58 z.
124	8.9			14.4	27.0	39.2		4.0			6 26.82	28.55	VII.5 39.825	24 54.28	22.04	6 55.37	28 51 36.32 z.
125	9	15.0						31.0			9 53.04	28.56	II. 3 38.300	37 31.07	21.40	10 21.60	29 4 12.47
126	7	2 1	8.0	31.0	43.2	55.6	8.2	20.8		٠.	10 43.14	28.57	IV. 2 45.422	42 10.66	21.23	11 11.71	29 8 51.89 z.
127 128	$\frac{6}{7.8}$	$\begin{bmatrix} 8.02\\10.02\end{bmatrix}$							• •	• • [14 45.83	28.59	" 1 33.770 " 2 40 200	54 45.45	20.37	15 14.42	28 21 25.82
129	9	49.0									$\begin{array}{c} 15 \ 47.83 \\ 17 \ 26.70 \end{array}$	28.59 28.62	" 3 40.398 " 3 33.275	36 18.76 40 24.91	$20.14 \\ 19.77$	$\begin{array}{c} 16 \ 16.42 \\ 17 \ 55.32 \end{array}$	29 2 58.90 z. 29 7 4.68 z.
130	9	54.8		19.4		44.4					17 32.54	28.62	" 4 32.630	★ 34 50.49	19.75	18 1.16	29 1 30.24 z.
131	7	1.0								• •	17 38.63	28.63	10. 4 41.182	29 54.35	19.74	18 7.26	28 56 34.09 z.
132 133	7.8	$\begin{array}{c} 12.02 \\ 56.0 \end{array}$									20 49.56 22 33.48	28.64 28.65	IV. 2 45.270 I. 6 39.800	42 15.91 16 12.59	$19.07 \\ 18.68$	21 18.20 $23 2.13$	29 8 54.98 z. 28 42 51.27 z.
	9	5	1	1													
134	8							8.8			24 20.94 25 31.22	28.69 28.67	IV. 4 41.786 V. 2 38.470	29 34.16 46 10.84	$18.26 \\ 18.00$	24 49.63 25 59.89	28 56 12.42 29 12 48.84 z.
136	8.9		:	34.5	47.0	59.3	12.5	24.5			26 47.04	28.69	IV. 2 36.318	47 25.22	17.70	27 15.73	29 14 2.92
137	9	1				1	1				28 39.11	28.75	II. 7 39.520	10 31.24	17.29	29 7.86	28 37 8.53
138 139	8 7	$\begin{vmatrix} 37.5 \\ \cdot \cdot \end{vmatrix}$ 5		$\frac{2.5}{6.0}$			43.5		• •		29 15.05 30 18.60	28.76 28.76	IV. 7 41.767 " 7 37.640	9 13.80 11 36.40	17.15	29 43.81 30 47 36	28 35 50.95 z.
140	8	35.84									32 13.44	28.77	" 5 43.490	22 48.07	$16.91 \\ 16.45$	$30 \ 47.36$ $32 \ 42.21$	28 38 13.31 z. 28 49 24.52 z.
141	8	22.03	4.84	17.2							33 59.92	28.75	" 1 39.630	51 22.46	16.02	34 28.67	29 17 58.48 z.
142	9		` 1	- 1		i .		1 1			34 1.52	28.78	" 6 40.500	15 48.81	16.00	34 30.30	28 42 24.81
143	9	1			-				• •		35 36.07	28.79	" 5 46.142	21 16.38	15.65	36 4.86	28 47 52.03
144	8	3.	- 1				l	38.2		0.5	36 0.57	28.79	" 4 43.250	28 43.82	15.54	36 29.36	28 55 19.36 z.
145 146	8 8			19.5	$\frac{.}{2.0}$	14.5	$\frac{.}{27.4}$	1 1		9.5	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$28.79 \\ 28.84$	11. 4 43.230 IV. 6 43.112	28 43.33 14 18.46	$15.54 \\ 14.81$	36 29.31 16 39 30.99	28 55 18.87 z. 28 40 53.27
														10.10		10 00 00.00	20 00.21

Number.	Magnitude.	I.	SECO.	NDS C	1		SITS.	11.	т.	a.		MICROMETER.	D.	d.	As	Right cension,	!	n So clinati	
4				Zone X	cv.	Ma	ıy 4.	н.	D.=-28° 5	26 20.0	•	n.'==-40.00.	n".=-35".63	. (0	Continued	l.)			
*147 148 149 *150 151 152 153 154 155 156 157 158 159 160 161	$\frac{9}{7.8}$	59.8 12.0 35.0 52.7 5.8 54.0		0 37.2 5 50.0 13.5 6.5 0 36.0 5 30.0 0 43.7 0	49.7 	2.21 	3.5 7.6 1.0 		h. m. s. 16 40 21.66 41 37.39 43 49.88 44 13.10 45 6.52 45 36.15 48 30.37 48 59.98 50 43.40 52 31.52 52 39.14 56 0.78 56 32.32 58 21.96 16 58 23.46	+28 28 28 28 28 28 28 28 28 28 28 28 28 2		TV. 5 40.552 " 2 45.493 " 2 48.378 " 2 46.730 " 3 39.732 VII. 3 42.618 I. 2 43.161 V. 4 43.180 IV. 2 42.690 " 6 45.500 VII. 3 36.340 IV. 7 35.070 " 6 32.450 " 2 43.780 " 2 44.402	-24 29".64 42 8.23 40 28.52 41 25.43 36 41.75 35 1.66 43 28.44 28 46.01 43 45.06 12 56.00 38 39.01 13 5.21 20 26.91 43 7.41 42 45.95	14".5 14.5 13.6 13.5 13.5 13.5 12.5 11.5 10.6 10.6	50 16 4 20 4 57 4 55 4 55 4 56 4 58 4 69 5 63 5 61 5 67 5 68 5 60 5 60 5 61 5 63 5 63 5 64 5 65 5 66 5 67 5 68 5 68 5 69 5 60	m. s. 0 50.51 2 6.21 4 18.72 4 41.94 45. 35.37 6.6 5.01 8.8 59.23 9.28.85 61 12.29 63 0.45 63 7.06 66 29.72 67 1.26 68 50.92 68 52.42	29 7 29 7 29 3 29 1 29 10 28 55 29 10 28 39 29 5 28 39 28 46 29 9	42.4 2.1 58.9 15.1 34.8 0.9 18.4 17.0 27.5 10.5 35.8 56.9 37.4	3 z. 9 18 0 19 7 3 15 3 16 2 2. 19 z.
					Zone	×V	I. N	1ay 19	. н. р	.=-4	.0° 5:	í 20.0. n. =	—12 ["] .29. n.	=-20	ő.00 .				
1 2 3 4 5 6 7 8 9 10	7.8 9 9.10 9 8 8 9 8.9 7	37.5 40.0 55.2 	28.2 42. 6. 	2 21.0 	5 38.2 5 53.0 22.2 3 22.0 3 15.5 3 4	50.0 50.5 53.0 2 66.0 56.5 60.0 41.5 53.0 30.0	4.2 5.2 8.0 2.2 2.0 		13 1 57.00 4 20.88 6 21.36 11 23.78 13 38.76 16 7.89 17 7.57 19 0.96 20 12.89 21 53.57 13 39 55.28	40 40 40 40 40 40 40 40 40	.16 .20 .22 .28 .31 .35 .35 .38 .39 .43	IV. 4 43.260 " 3 46.012 VII. 5 40.712 II. 4 42.174 IV. 6 40.180 " 6 42.340 " 6 45.403 II. 5 47.430 VI. 6 41.720 IV. 1 42.059 " 1 38.255	28 26.70 32 49.82 24 4.84 29 4.20 15 38.36 14 23.32 12 36.86 20 11.97 14 44.45 49 50.39 52 2.81	11.9 11.6 10.9 10.5 9.9 9.7 9.8 8.8 1.6	00	2 37.16 5 1.08 7 1.58 2 4.06 4 19.07 6 48.24 7 47.92 9 41.34 20 53.28 22 34.00 10 35.95	41 24 41 15 41 20 41 7 41 5 41 4 41 11 41 6 41 41	6.8 53.3 6.6 41.2 13.4 18.9	72 52 37 30 53 28 42
					Z one	XVI	I. I	May 19	. н. и).=- ⁵	28° 2	27 00.0. n'.	—20.00. n.	=-1	1.72.				
1 2 3 4 5 6		1	27. 52.0 4. 4.2 16.	5 41.0 0 16.4	52.0 4 28.8 4	5.2 5.2 1 19.0 11.2 5	7.8		14 1 58.24 3 34.52 5 40.28 6 23.85 8 16.56 14 13 29.18	40 40 40 40	.60 .61 .69 .63 .62	VII. 3 38.330 VI. 1 40.430 IV. 7 44.330 " 3 46.264 I. 7 38.010 " 4 36.620	37 5.70 50 30.35 7 21.24 32 31.91 10 59.21 32 8.12	19.7 19.6 19.4 19.3 19.1	30 41 35 18	2 38.84 4 15.13 6 20.88 7 4.48 8 57.18 4 9.86	29 17 28 34 28 59 28 38	49.9 40.6 51.2 18.3	05 z. 65 z. 26
				(CORRE	ECTIC	ons.						INSTRUM	IENT F	READINGS	•			
			COR. TO	HOUR COR		m.	n.	c.	ZENITH POINT.	coinc.			Α.	CIR.	C. D.	Mean.	BAR.	THER	Ex.
May 1	9, at 1	2h	s. +29.708	+0.0)26 +0	s. 0.505	s. +0,353	+0.207	0° 0′ 2″.57	r. 40.137		one XVI.—May 19,	h. 13.0 279° 50′ 39″.9 13.6 46.2	52.0 59.2	60″.4 64″.5 67.6 71.2 81.0 83.2	54.20 61.05	1. 30.066 30.066	50°.5	53.1
													56.7	1 1	80.5 83.0	1	8 8	58.5	50.7



Number.	Magnitude.	I.			DS	ог т		NSI'.	гs. 10.	11.	Т.	a.	MICROMETER.	D.	d.	As	Right cension,	Do	an Sc eclinat 50.0.	
				Zor	ne X	VII.	ľ	May	19.	Н.	D. =-28°	27 00.0.	n'.=-20″.00.	n".==-11		(Continu	ied.)	1		
7 8 9 10 11 12 13 14 *15 16 17 18 19 20 21 22 23 *24 25 26 *27	7 9 9 9 8 9 8	6.0 43.0 20.2 17.0 35.2 51.2 20.0 55.5	55.5 33.0 4 47.8 16.0 2 4.2 1 32.8 4 8.3 2 36.0 4	1.0 9.0 9.0 11.5 	43.2 2.0 34.0 21.0 21.0 38.0 38.0 24.0 41.0 118.0 118.0 119.0 11	55.5 14.0 43.3 46.2 43.0 43.0 33.0 7.0 25.2 35.0 550.8 41.3 53.0 441.3 541.0 445.2 445.2	8.2 .556.2 .559.0 3.2 49.0 	21.0 9.0 46.2 11.5 8.0 50.0 2.0 18.4 55.2 6.3 35.9 10.8 35.9	5.0	117.4	h. m. s. 14 15 10.90 18 43.30 20 1.81 20 31.24 21 8.84 23 33.98 24 30.44 26 20.69 27 58.16 30 54.71 32 12.77 32 22.65 33 38.13 35 24.17 45 40.88 47 17.85 51 28.93 53 57.52 57 33.17 59 0.79 15 0 7.58	\$.\\ \phi 40.69\\ 40.71\\ 40.73\\ 40.73\\ 40.73\\ 40.73\\ 40.77\\ 40.77\\ 40.78\\ 40.82\\ 40.80\\ 40.82\\ 40.91\\ 40.95\\ 40.99\\ 40.90\\ 40.9	" 5 45.023 II. 3 42.395 VII. 4 39.740 " 7 37.853 IV. 6 36.400 " 4 34.970 " 5 40.630 I. 3 43.280 III. 7 36.600 IV. 3 40.580 " 6 40.702 " 2 45.150 VI. 6 42.190 IV. 4 43.950 " 6 42.788 " 3 42.788 " 3 42.788 " 1 44.582 " 4 43.000 " 5 47.998	-28 46.65 21 30.58 34 45.39 30 20.35 11 4.63 17 46.30 33 5.50 24 2.74 34 15.02 11 48.20 35 48.31 15 17.62 41 55.15 14 26.04 27 55.26 14 5.57 34 31.98 48 7.09 28 28.08 19 48.14 48 57.72	-18.53 18.19 18.00 18.01 17.94 17.77 17.58 17.32 16.90 16.63 16.64 15.19 14.44 14.22 13.64 13.42 13.33	100 11	m. s. 55 51.59 9 24.01 00 42.54 11.1.97 11.21 7 1.46 8 38.95 1 35.49 2 53.58 3 3.47 4 18.93 6 4.99 6 21.79 7 58.76 2 9.88 4 38.48 8 14.17 9 41.78 0 48.57	28 4 29 28 5 28 3 28 4 29 28 5 29 28 3 29 4 29 4 28 5 28 4 29 1 28 5 28 4	6 5 7 38.: 8 48.: 2 3 7 38.: 5 4.: 0 23.: 1 20.: 1 32.: 5 4.: 0 23.: 1 20.: 1 32.: 5 4.: 2 34	777 z. 2. 445 z. 686 z. 577 z. 2. 201 z. 208 z. 13 23 z. 110 z. 206 z. 206 z. 206 z. 444 z. 445 z. 656 444 z. 2. 656 z. 772 z. 2. 2566 z. 2. 6566 z. 2. 65672 z. 6566 z. 2. 65672 z. 65
1 2 3 4 5 6 *7 8 9 10 11 12 13 14 15 16	7.8 9 8 9 5 7.8 9 8.9 7	25.0 46.3 45.0 52.5 41.8 4.5	57.8 	0.0 2 9.0 3 3.3 3 5.0 4 4 4 9.2 5	28.2 	34.5 4 388.0 5 227.0 3 40.3 5 56.0 36.0 4 34.5 4 36.2 4 36.2 4 36.2 4	 				9. H. D 15 21 58.02 22 22.16 25 1.78 25 25.81 25 55.20 27 14.62 28 28.16 29 43.75 33 23.78 35 22.36 36 24.14 39 30.46 40 18.92 44 41.78 45 51.90 15 47 12.79	$\begin{array}{c} -2\mathring{7} \\ \hline \\ 41.12 \\ 41.11 \\ 41.15 \\ 41.15 \\ 41.13 \\ 41.14 \\ 41.15 \\ 41.18 \\ 41.17 \\ 41.22 \\ 41.18 \\ 41.28 \\ 41.28 \\ 41.28 \\ 41.32 \\ \end{array}$	IV. 7 36.570 I. 7 39.533 IV. 4 39.248 VI. 6 41.630 V. 7 38.350 IV. 6 40.792 '' 3 44.521 I. 6 45.128 IV. 3 40.198 '' 7 43.220 I. 1 37.828 '' 2 45.738 IV. 7 35.192 V. 5 34.249	26 2.01 11 45.76 10 2.99 30 33.98 14 41.82 10 44.22 15 10.92 33 26.40 12 40.82 35 57.70 7 56.03 51 56.18 41 36.29 12 33.33 27 39.44 47 4.22	". = -8 19.58 19.57 18.83 18.71 18.60 18.27 17.95 16.18 15.92 15.11 14.89 13.73 13.42 13.06	3 15 2 2 2 2 2 2 2 3 3 3 3 3 4 4 4 4 4 4 4 4	2 39.14 3 3.27 5 42.90 6 6.96 6 36.33 7 55.76 9 9.31 0 24.93 4 4.95 6 3.58 7 5.32 0 11.74 1 0.20 5 23.02 6 33.18 7 54.11	27 33 27 5 27 4 27 33 27 4 27 33 28 3 28 3 28 1 28 1 28 8 27 36 27 5	3 21.5 3 21.5 7 21.8 7 52.6 0.4 4.0 0.4 0.0 0.0 0.0 0.0 0.0	33 z. 39 z. 42 y. 49 z. 37 z. 38 z. 52 z. 52 z. 58 z. 66 z. 66 z.
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	ay 2	27, at 16	3h	+35	.269	+0.03	8 +0.5	05 +	353	+0.247	0° 0′ 03′.79	40.110	XX				1	ĺ			73.5 69.5

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at 16/	r	$^{s.}_{+42.761}$	+ 0.00	$08 \begin{vmatrix} s \\ +0.1 \end{vmatrix}$	198	$^{s.}_{+0.39}$	$\begin{array}{c c} s. \\ +0.2 \end{array}$	17 0° 0′ 1″.27	r. 40.110	Zon XX		293° 42′ 0′.0	0,0	6.5 4	.7 2.80			1
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er	tude.		SECO	ONI	os o	OF _. T	raa:	NSIT	s.							Mean Right	Mean South
Number	Magnitude.	ı.	11.	111.	ıv.	v.	VI.	vII.	10.	11.	Т.	a.	MICROMETER.	D.	d.	Ascension, 1850.0.	Declination, 1850.0.
						\mathbf{Z}_0	ne X	XV.	J	ine S	8. M. D.	=-26°50	6 40.0. n.=	-42.23. n".	.=-4.5 ⁸		
30	8						34.0	0.46.0			h. m. s. 14 41 9.03	*. +53.50	IV. 2 40.00	44 46.41	-34.29	$\begin{array}{cccc} h. & m. & s. \\ 14 & 42 & 2.53 \end{array}$	27 42 0.70 z.
31	8		35.54'								44 0.28	53.52	2. 1 40.83	50 8.74	33.86	44 53.80	47 22.60 z.
32	7						59.5				44 34.46	53.52	II. 2 36.40	46 50.68	33.79	45 27.98	44 4.47 z.
33	8 7.8		- 1	- 1		1		49.5		• •	59 12.34	53.60	I. 1 41.28	49 53.43	$31.55 \\ 30.66$	$\begin{array}{cccc} 15 & 0 & 5.94 \\ & 6 & 16.73 \end{array}$	47 4.98 z. 17 36.96 z.
34 35	6		- 1	. !	23.0		1	25.4			15 5 23.14 5 48.44	53.59 53.58	" 5 46.68 IV. 7 48.375	20 26.30 4 54.68	30.60	6 42.02	2 5.28 z.
36	7	1 1	12.0_{24}	1			1	1			10 36.75	53.65	II. 2 35.91	47 7.58	29.80	11 30.40	44 17.38 z.
37	9			5.0							12 47.42	53.61	VI. 7 42.73	8 9.54	29.47	13 41.03	5 19.01
38	9		.					1	1		13 48.94	53.64	VII.4 44.40	27 32.29	29.30	14 42.58	24 41.59
39	8		$ \cdot $.		45.0		9.5	5			$16\ 44.83$	53.67	" 3 39.44	36 20.10	28.69	17 38.50	33 28.79 z.
*40	8					5.5	18.0	30.0			16 53.14	53.66	" 4 40.17	29 58.38	28.76	17 46.80	27 7.14
41	8.9						40.0	52.5			18 15.50	53.64	" 7 41.27	8 59.75	28.53	19 9.14.	6 8.28
42	8.9			- 1			1	46.3			22 9.21	53.71	II. 2 45.10	41 50.13	27.85	23 2.92	38 57.98 z.
43	6		14.026			ł					24 38.87	53.71	1. 3 41.53	35 7.40	27.42	25 32.58	32 14.82 z.
44	9		20.039				07 (• •	• •	25 44.80	53.71	IV. 2 39.87	44 50.88	27.24	26 38.51 $27 55.79$	41 58.14 z. 38 15.68 z.
45 46	$\frac{4.5}{7}$						27.0 52.5			• •	27 2.07 $28 27.83$	$53.72 \\ 53.73$	VI. 2 46.30 VII. 2 38.78	$\begin{array}{c c} 41 & 8.70 \\ 45 & 28.18 \end{array}$	26.98 26.72	29 21.56	30 13.00 z. 42 34.90
47	8		į				1	14.0			29 37.07	53.70	" 7 36.29	11 51.76	26.54	30 30.77	8 58.30 z.
48	9		i					1	1		31 24.47	53.72	" 5 42.20	23 1.09	26.20	32 18.19	20 7.29
49	9		$ \cdot $.				28.3	3]	$33 \ 3.51$	53.75	" 3 46.27	32 24.19	25.89	$33\ 57.26$	29 30.08 z.
50	7		.		12.0	24.0	36.5	5			36 11.82	53.77	I. 3 36.32	38 7.86	25.30	37 5.59	35 13.16 z.
51	8.9		1			54.5		1			38 42.20	53.74	" 7 39.91	9 46.71	24.73	39 35.94	6 51.44 z.
52	8.9						14.0			[40 49.25	53.78	VI. 4 44.70	27 22.13	24.44	41 43.03	24 26.57
53	8		13	3.4	26.0						$43\ 25.90$	53.77	2. 6 37.11	$17\ 14.25$	23.93	$44\ 19.67$	14 18.18
54	8	• •	• • •			36.0	48.7				44 23.96	53.76	II. 7 40.25	9 35.23	23.74	45 17.72	6 38.97 z.
55 5 c	8.9	• •	1	•	• •	٠.	• •			• •	44 58.42	53.80	VII. 4 39.74	30 13.21	23.63	45 52.22	27 16.84 z.
$\frac{56}{57}$	8		1	•	• •	٠.			39.5	N N	$\begin{array}{c} 45 \ 43.96 \\ 47 \ 10.69 \end{array}$	$53.81 \\ 53.79$	11. 4 34.51 " 6 41.20	$53 \ 13.34$ $14 \ 52.70$	$23.48 \\ 23.21$	$\begin{array}{ccc} 46 & 37.77 \\ 48 & 4.48 \end{array}$	50 16.82 11 55.91 z.
58	8.9				$\frac{.}{2.7}$	15.0	27.0	1			56 2.56	53.15	I. 4 44.21	27 38.85	21.44	56 56.41	24 40.29
*59	8			i				29.0			56 51.98	53.84	IV. 5 44.10	21 55.86	21.28	57 45.82	18 57.14
60	7						25. 7	38.0			58 0.97	53.85	VII. 5 43.26	22 24.49	21.03	58 54.82	19 25.52 z.
61	8		i	- 1			1	11.0			16 0 33.89	53.87	" 3 46.30	32 23.13	20.51	16 1 27.76	29 23.64
62	8		1								1 44.45	53.85	I. 6 45.58	12 21.94	20.27	2 38.30	9 22.21 z.
63	5									[$2\ 10.39$	53.88	VII.3 47.78	31 32.00	20.18	3 4.27	28 32.18
64	8					}	1		37.0 5	50.2	241.79	53.91	11. 1 45.50	47 27.15	20.08	3 35.70	44 27.23 z.
65 cc	8			- 1			1	43.5	- 1	• •	8 6.54	53.93	VI. 2 43.11	42 58.86	18.94	9 0.47	39 57.80 z.
66 67	8	• •					44 5		- 1		15 2.30	53.93	I. 5 44.20	21 52.01	17.44	15 56.23	18 49.45 z. 20 27.30 z.
68	8 7		39.251	. ½	4 0	52.0 16.2	44.7			• •	$\begin{array}{ccc} 16 & 19.91 \\ 20 & 3.97 \end{array}$	$53.93 \\ 53.97$	I. 5 41.36 1. 3 36.57	$\begin{array}{c c} 23 & 30.13 \\ 37 & 58.71 \end{array}$	17.17 16.35	17 13.84 20 37.94	34 55.06 z.
69	8						25.0				23 0.30	53.99	2. 1 49.30	45 16.15	15.69	23 54.29	42 11.84
*70	8																40 2.93
71	8.9		39				í			• •	28 51.30 $29 58.70$	$54.02 \\ 54.02$	VI. 2 42.83 VI. 2 40.23	43 8.53 44 38.35	$14.40 \\ 14.14$	$\begin{array}{c} 29 \ 45.32 \\ 30 \ 52.72 \end{array}$	40 2.93 41 32.49 z.
72	7							1.0			32 23.96	$54.02 \\ 54.02$	VII. 2 40.23 VII. 3 43.90	33 46.01	13.60	33 17.98	30 39.61
*73		28.0	40.5 52				1	1			34 5.02	53.99	1. 6 43.10	13 47.07	13.21	34 59.01	10 40.28
74	8		$\cdot \cdot $.					14.7			35 37.71	53.99	IV. 6 42.98	13 52.05	12.86	36 31.70	$10\ 44.91$
75	8		$\cdot \cdot \cdot$	- 1	٠.			0.5		٠ .	37 23.44	54.01	III. 6 40.62	15 13.51	12.45	38 17.45	12 5.96
76	9		30.0 42	- 1	- 1					$\cdot \cdot $	54.78	54.03	VII. 5 45.40	21 10.58		48.81	18
77	8	• •	- 1		• •		1	8.4			40 31.24	54.07	V. 2 46.12	41 14.95	11.74	41 25.31	38 6.69 z.
78 79	8 8	• •	.					1 3	4.5	- 1	$ \begin{array}{c cccc} 41 & 8.93 \\ 44 & 12.87 \end{array} $	$\begin{array}{c} 54.08 \\ 54.05 \end{array}$	11. 1 43.36 VI. 5 43.74	$\begin{array}{c cccc} 48 & 41.06 \\ 22 & 8.12 \end{array}$	$11.62 \\ 10.89$	$\begin{array}{ccc} 42 & 3.01 \\ 45 & 6.92 \end{array}$	45 32.68 z. 18 59.01 z.
			.		.5.0	• •			1	• •							
80 *01	8	• •					1	11.3		• •	44 33.21	54.07	VII. 3 45.28	32 58.37	10.82	45 27.28	29 49.19
*81 82	8 8	• •	l	1	- 1		29.0			• •	47 38.90	$54.07 \\ 54.09$	I. 4 48.27 I. 2 50.76	25 18.63	$10.09 \\ 9.75$	48 32.97 16 49 58.33	22 8.72 z. 27 35 24.15
00	0	• •	• • •	•		10.9	23.0	$ \cdot\cdot $		• •	16 49 4.24	94.09	1. 2 30.10	38 34.40	J. (3	10 42 90.99	~1 00 AT.10

oer.	Magnitude.		SEC	ONE	os o)F T	ΓRA	NSIT	rs		т.	a.		Wan awaran	D.	d.	8	Right		n So	
Number.	Magn	ı.	11.	ı. ı	ıv.	v.	vi.	vII.	10.	11.	1.	а.		MICROMETER.	D.	u.	1850		ł	0.0.	оп,
				Zon	e Χ Σ	XV.	-	June	3.	м.	D.=-26	56 40.0	00.	n. = -42.23	. n'.=-4	, 58. (Continue	d.)			
83 84 85 86 87 88 89 90 91	8 7.8 7 8 8 8 8 7.8 7	54.5	7.0 . 26 	.0 .0 .19	5.0 9.53 7.51	9.8	3.0	7.5 28.5			h. m. s. 16 50 52.09 51 4.97 51 39.36 53 31.61 55 38.39 56 19.62 59 30.52 59 51.55 17 1 7.50 3 44.07	s. +54. 54. 54. 54. 54. 54. 54. 54. 54.	12 05 12 09 08 12 13 14 14	r. IV. 1 45.69	-47 21"37 4 22.12 45 52.28 19 53.17 13 5.34 34 33.64 29 30.73 37 39.16 37 31.58 40 0.53	- 9.31 9.28 9.13 8.20 8.18 8.01 7.25 7.17 6.85 6.23	16 55 55 56 56 57 6 6 6 6 6 6 6 6 6 6 6 6	3. s. 46.21 59.02 2.33.48 3.25.70 3.32.47 1.13.74 0.24.65 0.45.69 2.1.64 4.38.22	1 42 16 9 31 26 34 34	10.66 11.44 41.4 41.3 53.5 21.6 17.9 26.3 18.4 46.7	0 z. 1 7 2 5 8 3 z. 3
93 94 95 96 97 98 99	8 8 8 8 7.8 8				2	 21.5 50.0	34.2	$\frac{.}{26.0}$	 30.8	43.5	5 3.26 6 13.44 7 9.32 7 35.35 9 48.89 11 37.73 17 15 47.59	54. 54. 54. 54. 54. 54.	14 18 18 19 14	V. 1 39.66 III. 5 36.385 VII.3 34.57 11. 3 34.53 VII.3 33.27 IV. 6 42.29 2. 4 38.97	50 49.62 26 22.29 39 8.25 39 9.16 33 53.21 14 15.91 30 39.60	5.90 5.61 5.38 5.28 4.74 4.30 3.26		5 57.44 7 7.58 8 3.50 8 29.53 0 43.08 2 31.87 5 41.78	23 35 35 30 11	35.5 7.9 53.6 54.4 37.9 0.2 22.8	0 3 z. 4 z. 5
		1			?	Zon	e XX	VI.	J	une 1	5. H.	D.=-	40°4	19 50.0. n.=	=-70.00.	n.=-1	4.57.				
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	7.8 7 8.9 5.6 8.9 9 8.9 8.9 7 7.8 9	15.6 47.2 42.2 28.5 5.0 40.2 44.6 	39.0 54 30.5 45 2.0 16 57.2 11 43.0 7 37.5 55 519.5 34 58 20.3 34 55.2 10 55.2 10 59.3 14 27.0 42 53.0 7	0 55 6 3 4 4 6 2 6 2 6 5 2 6 6 6 6 6 6 6 6 6	8.0 9.4 11.5 4.0 5.6 6.0 4.2 5.5 7.2 9.2 9.0 6.0 7.2 9.0 7.0 15.0 38.4 4.0 5.0 38.4 4.0 5.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6		29.0 1.0 55.4 18.2 36.3 18.2 26.0 54.0 4.2 51.2	52.3 43.3 10.3 32.2 51.0 33.4 40.6 8.5 12.3 5.8 50.3			14 39 31.20 42 8.38 43 59.58 46 31.43 46 43.80 48 26.28 50 22.35 51 6.87 51 19.20 55 48.78 57 15.96 58 7.22 15 0 49.30 3 56.76 6 24.63 16 28.54 16 34.90 17 56.64 19 22.04	58. 58. 58. 58. 58. 58. 58. 58. 58. 58.	70 72 76 76 77 78 76 77 83 85 83 88 92 91 00 03 02	IV. 5 43.830 " 3 39.842 " 3 42.490 II. 2 47.402 IV. 1 43.375 " 3 35.190 II. 1 0.972 III. 5 43.230 VI. 5 43.730 IV. 3 39.522 " 2 38.925 V. 5 37.450 IV. 2 38.150 " 1 34.022 " 4 48.250 " 4 44.280 " 1 36.080 " 4 33.770 V. 4 35.320 VII. 6 37.260	22 11.97 36 18.82 34 46.93 40 44.74 48 58.86 39 0.69 22 32.92 22 15.29 36 27.85 45 39.52 25 53.90 46 6.55 54 23.75 31 15.50 27 45.86 53 12.09 33 51.11 32 56.92 17 14.50	69.96 69.62 69.36 69.02 68.99 68.76 68.48 68.36 67.72 67.51 67.38 66.52 66.52 64.55 64.55	2 4: 4: 4: 4: 4: 4: 4: 4: 4: 4: 4: 4: 4:	29.86 3 7.08 4 58.30 7 30.19 7 42.56 9 25.05 1 21.13 2 5.63 2 17.97 3 47.61 8 14.81 1 48.18 1 48.18 1 48.18 1 48.18 1 48.18 1 48.18 1 48.18 1 48.18 1 55.68 1 23.54 1 33.93 8 55.66 9 21.06 1 5.65	41 27 41 25 41 31 41 39 41 29 41 13 41 13 41 27 41 36 41 45 41 22 41 18 41 24 41 24 41 23	11.9 18.4 46.2 43.7 57.8 159.4 13.6	.4 99 66 55 55 в. 00 55 77 33 88 44 77 44 22 44 11 м.
				·	C	ORR	ECT	ions							INSTRU	JMENT R					
			COR. T	- 1	cor.	- 1	m.	1	n.	<i>c</i> .	ZENITH POINT.	COINC.			Α.	B.	C. D.	Mean.	BAR.	THER	Ex.
June	15, at 1	64	s. +47.33	8	s. +0.09	20 +	s. -0.198	s	396	+0.247	0 0 1".64	r. 40,122	Z_{0}		h. 14.7 279°51′ 6″.2 15.6 7.7 18.0 7.0 18.5 20.0 6.5	4.0	3.0 8.9 5.2 10.0 5.0 9.0	6.28	1. 29.914 29.906 29.888 29.886 29.884	73.0 72.2 70.3 70.3 69.5	70.7 69.6 67.5 67.4 66.4

	de.	sı	CON	DS (OF T	'RAN	SIT	s.							Mean Right	Mean South
Number.	Magnitude.	I. III.	111.	IV.	v.	vi.	vII.	10.	11.	Т.	a.	MICROMETER.	D.	d.	Ascension, 1850.0.	Declination, 1850.0.
Z	≥ =								ı							
			Zor	ne XX	XVI.	Ju	une 1	5.	н.	<i>D</i> .=−40 [°]	49 50.0.	n'=-70″.00.	n"=-14	1.57. (0	Continued.)	
21	9		15.5	30.6	44.6				Carpainteconn	h. m. s. 15 21 30.32	+59.02	r. IV. 7 36.250		_63.74	h. m. s. 15 22 29.34	$4\mathring{1} 2^{'} \ 50^{''}\!\!.47$
22	9					24.0				$21\ 54.89$	59.03	VI. 5 46.152	20 51.27	63.68	$22\ 53.92$	41 11 44.95
$\frac{23}{24}$	9			• •	5	$8.22 \\ 57.01$				23 39.03 23 27.98	59.05 59.03	" 5 43.250 " 7 41.554	22 32.13 8 52.09	63.39 63.40	$24 \ 38.08$ $24 \ 27.01$	41 13 25.52 40 59 45.49
25	7.8	24.8 39.4				1				27 8.60	59.06	IV. 7 44.882	6 56.67	62.80	28 7.66	40 57 49.47
26	8	1 1	1	1	51.2			• •		$28 \ 36.92$	59.07	" 6 41.530	14 46.19	62.55	29 35.99	41 5 38.74
27	7 9	• • • •	1	1	44.05	- 1	- 1		• • •	29 29.54	59.12	" 3 39.890	36 17.15	62.39	30 28.66	41 27 9.54 41 33 10.94
28 29	9	6.821.3	5		48.0 5.02					$30 \ 33.20$ $32 \ 50.78$	59.14 59.15	V. 2 44.696 I. 3 31.920	42 18.72 40 54.05	62.22 61.91	31 32.34 33 49.93	41 31 45.96
30	6.7	48.0	1		1		اه .	- 1		33 17.12	59.14	VI. 4 41.395	29 26.04	61.72	34 16.26	41 20 17.76 м.
31	7.8	19.8 34.8	49.0	4.0	18.3	33.0 4	8.0			36 3.91	59.19	IV. 1 36.800	52 47.37	61.24	37 3.10	41 43 38.61
32	8	23.0 38.								38 7.14	59.17	" 4 42.690	28 40.96	60.88	39 6.31	41 19 31.84
33	9	29.2 44.0 28.5 43.0	1		1 1	42.55	1	- 1		44 13.24 46 12.13	59.23 59.24	VI. 3 37.170 IV. 4 39.460	37 51.71 30 33.49	59.86 59.39	$\begin{array}{c} 45 \ 12.47 \\ 47 \ 11.37 \end{array}$	41 28 41.57 41 21 22.88
34 35	9		31.2		23.03					46 12.13	59.24	V. 5 43.346	22 28.90	59.39	48 8.44	41 21 22.88
36	5.6	35.0 49.	3	19.0	33.2	47.8	2.4			48 18.75	59.26	IV. 4 44.270	27 46.21	58.99	49 18.01	41 18 35.20 в.
37	9	10.5 25.5						- 1	٠.	52 54.07	59.29	" 4 46.188	26 39.50	58.12	53 53.36	41 17 27.62
38 39	$\begin{vmatrix} 7.8 \\ 9 \end{vmatrix}$	12.5 27.5 36.0 50.5	1	1 1	1 1		- 1			55 56.55 16 4 19.45	59.34 59.36	" 2 33.530 " 5 38.702	48 47.09 25 10.46	57.51 55.81	56 55.89 16 5 18.81	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
40	8	39.254.								10 23.70	59.45	" 2 35.390	47 42.64	54.57	11 23.15	41 38 27.21 м.
41	8.9	52.0 7.	21.5	36.2	50.5	5.21	19.8			18 36.06	59.46	" 5 37.660	25 46.08	52.84	19 35.52	41 16 28.92
42	6	33.448.			((1	- 1			20 17.24	59.48	" 3 36.055	38 30.57	52.49	21 16.72	41 29 13.06
43	9	13.0 27.			1 1	26.54		1		22 57.02	59.50	VI. 3 39.336	36 36.42	51.94	23 56.52	41 27 18.36
$\frac{44}{45}$	9	29.3 45. 4.0 18.				$rac{42.85}{17.03}$				$31 \ 13.59$ $32 \ 47.85$	59.57 59.58	IV. 4 36.361 " 3 41.240	32 21.21 35 30.33	50.15 49.79	32 13.16 33 47.43	41 23 1.36 41 26 10.12
46	8	22.5 37.			1 / 1	1				35 6.60	59.58	I. 4 41.980	29 5.45	49.29	36 6.18	41 19 44.74 м.
47	8	54.5 9.		38.0	1 1	- 1				35 38.13	59.57	IV. 5 45.172	21 25.42	49.17	36 37.70	41 12 4.59
48	8 8.9	49.0 4.			1	16.0 3	- 1	• •	• •	35 46.54	59.58 59.60	V. 4 40.622 II. 4 36.540	29 52.80 32 14.61	49.14 48.54	36 46.12 39 32.56	41 20 31.94 41 22 53.15
49 50	9	30.545.		i						38 32.96 39 14.12	59.59	IV. 5 47.332	20 10.41	48.38	40 13.71	41 10 48.79
51	9	ll.			55.0	9.62	24.0			39 40.36	59.60	V. 4 44.632	27 33.41	48.29	40 39.96	41 18 11.70
52	9			48.4	3.5	18.2				40 48.75	59.63	IV. 3 40.062	36 11.25	48.04	41 48.38	41 26 49.29
53	9	1 1			32.0			- 1	٠.		59.64	VI. 3 31.860	40 56.27	47.93	42 16.77	41 31 34.20 m.
54 55	$\begin{vmatrix} 7.8 \\ 8 \end{vmatrix}$	37.5 52.	1	1	$\begin{array}{c} 45.5 \\ 36.0 \end{array}$	- 4				$\begin{array}{c} 42 \ 30.96 \\ 47 \ 21.42 \end{array}$	59.64 59.67	IV. 3 29.210 I. 6 32.350	42 28.65 20 5.18	47.65 46.57	43 30.60 48 21.09	41 33 6.30 m. 41 10 41.75
56	9	21.								47 50.48	59.63	IV. 6 33.388	19 29.37	46.46	48 50.11	41 10 5.83
57	9	49.0 3.	5 18.3	33.2	47.2	2.4			٠.	56 32.95	59.69	" 3 44.160	33 48.77	44.45	57 32.64	41 24 23.22
58 59	$\begin{vmatrix} 7.8 \\ 9 \end{vmatrix}$	47.8 3.		1	1		- 1		• •	58 31.99 17 0 2.76	59.74 59.75	" 3 34.190 V. 2 41.382	39 35.47 44 14.21	44.00 43.65	59 31.73 17 1 2.41	41 30 9.47 41 34 47.86
6 0		34.7 49.								2 18.58	59.76	IV. 3 34.442	39 26.79	43.12	3 18.34	41 29 59.91
61	9	.			12.0	26.44	11.0			2 57.30	59.74	VII. 5 35.952	26 45.62	42.98	3 57.04	41 17 18.60
62	9	16.5 31.	5 46.0	1.0	15.2	30.44	14.2			8 0.75	59.80	IV. 1 38.478	51 49.24	41.77	9 0.55	41 42 21.01
63	9				51.5				٠.	9 37.08	59.77	" 4 34.550	33 23.93	41.34	10 36.85	41 23 55.27
64 65	8	41.356.			$\frac{1.0}{40.0}$					10 46.64 13 25.36	59.80 59.79	" 2 40.262 " 4 39.090	44 53.15 30 46.24	41.12 40.50	11 46.44 14 25.15	41 35 24.27 41 21 16.74
66	9	11.000.	1	1		- 1	- 1	- 1		14 1.24	59.78	VI. 5 45.530	21 12.65	40.35	15 1.02	41 11 43.00
67	8	17.5 32.	2 46.4	0.5	15.2	30.0			٠.	16 0.93	59.79	IV. 5 47.752	19 55.65	39.88	17 0.72	41 10 25.53
68 69	$\begin{vmatrix} 9 \\ 9 \end{vmatrix}$	• • • •			$\begin{array}{c} 34.0 \\ 10.0 \end{array}$				• •	18 20.60 20 55 31	59.83 59.81	V. 3 40.700 IV. 5 46.670	35 48.92 20 33.24	39.32 38.72	19 20.43 21 55.12	41 26 18.24 41 11 1.96
69 70	6		40.8	32.5	47.0	1.81	16.5			20 55.31 21 32.68	59.81	V. 6 44.725	12 55.14	38.58	22 32.48	41 11 1.50 41 3 23.72 m.
71.	8	36.						- 1		23 4.92	59.83	IV. 5 43.726	22 15.56	38.20	24 4.75	41 12 43.76
72	8.9	1								27 53.68	59.83	" 6 46.360	11 58.54	37.04	28 53.51	41 2 25.58
73	8.9	48.5 3.	2 18.0	32.8	47.0	2.0	17.0	• •		17 29 32.64	59.90	" 2 38.644	45 49.23	36.67	17 30 32.54	41 36 15.90
	<u> </u>		<u> </u>	<u></u>							<u></u>					

er.	Magnitude.	SECONDS OF TRANSITS.	Т.		MGDOMEWED	D.	d.	Mean Right	Mean South
Number.	Magn	1. II. III. IV. V. VI. VII. 10. 11.	1.	a.	MICROMETER.	р.	u.	1850.0.	1850.0.
		Zone XXVI. June 15. H.	$D = -40^{\circ}$ 4	19 50.0.	n'. ==70.00.	n".==-14".	57. (C	ontinued.)	
74	9	9.0 23.4 38.0 52.4	h. m. s. 17 31 38.06	*. +59.87	r. IV. 5 40.540	$-24^{\prime} 6^{''}\!\!.27$	-36.18	h. m. s. 17 32 37.93	41 14 32 35
75	8	34.5 48.5 3.4 18.0	32 34.13	59.90	" 2 40.718	44 37.14	35.96	33 34.03	41 35 3.10
76	9	$ \begin{vmatrix} . & . & 48.0 \end{vmatrix} \ 3.0 \begin{vmatrix} 17.0 \begin{vmatrix} 31.5 \end{vmatrix} \ 46.0 \end{vmatrix} \ . & . \end{vmatrix} \ . & . \end{vmatrix} $	34 17.11	59.87	III. 5 46.005	20 56.42	35.53	35 16.98	41 11 21.93
77	8	$\begin{vmatrix} 33.0 & 47.5 & 2.0 & 17.0 & 31.2 & 46.0 & & . & . & . \end{vmatrix}$	35 16.70	59.87	IV. 5 43.407	22 26.84 33 41.60	35.28	$36\ 16.57$ $38\ 28.23$	41 12 52.12 41 24 6.35
78 79	8	44.0 59.2 14.0 28.0 43.0 25.0 40.3 55.0 8.2 39.0 53.0	37 28.32 39 9.23	59.91 59.93	II. 3 44.364 III. 2 45.180	42 2.04	$\begin{array}{c} 34.75 \\ 34.36 \end{array}$	40 9.16	41 32 26.40
80	9	38.0 52.0	39 37.72	59.93	IV. 2 45.040	42 6.91	34.25	40 37.65	41 32 31.16
81	8		39 47.72	59.94	VI. 2 39.626	45 14.94	34.20	40 47.66	41 35 39.14
82	8.9	$ 31.5 46.0 0.6 15.0 29.8 44.5 58.5 \dots \dots $	$42\ 15.16$	59.91	IV. 5 36.490	26 27.33	33.64	43 15.07	41 16 50.97
83	6	$ 24.0 39.0 53.8 8.0 22.8 \cdot \cdot 52.0 \cdot \cdot \cdot \cdot $	46 8.23	59.96	" 1 40.050	50 54.42	32.77	47 8.19	41 41 17.19 в.
84	8	18.2 33.1 47.7 2.5 17.0 31.2 46.2	48 2.33	59.96	" 2 37.550	46 27.27	32.21	49 2.29	41 36 49.48
85	9	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$50 \ 37.46$	59.96	" 4 33.738	33 52.22	31.58	51 37.42	41 24 13.80
86	9	$ 5.0 \dots 38.8 52.5 8.0 22.0 \dots \dots $	53 38.40	59.97	V. 3 43.550	34 9.78	31.10	53 38.37	41 24 30.88
87	9	38.0 52.5 7.0 21.5 36.5 51.2 5.2	55 21.76	59.99	" 2 34.436	48 15.83	30.43	56 21.75	41 38 36.26
88	$\begin{vmatrix} 6.7 \\ 6 \end{vmatrix}$	$ \begin{vmatrix} 43.3 & 58.2 & 12.7 & 27.3 & 42.0 & 56.3 & 11.0 & . & . & . \\ 51.4 & 6.0 & 20.0 & 35.0 & 49.4 & . & . & . & . & . & . \\ \end{vmatrix} $	59 27.30	59.99 59.99	IV. 4 36.272 " 4 37.711	32 24.29 31 34.08	$29.41 \\ 28.91$	$\begin{array}{cccc} 18 & 0 & 27.29 \\ & 2 & 35.03 \end{array}$	41 22 43.70 41 21 52.99
90	$\begin{vmatrix} 8.9 \end{vmatrix}$	$\begin{vmatrix} 51.4 & 6.0 & 20.0 & 35.0 & 49.4 & . & . & . & . & . & . \\ 20.0 & . & . & . & 4.0 & 18.2 & 33.0 & 47.5 & . & . & . & . \end{vmatrix}$	18 1 35.04 2 3.82	59.99	" 5 34.220	27 46.17	28.80	3 3.81	41 18 4.97
91	9	3.0 17.4 32.0 46.5 1.0	32 46.58	60.04	" 6 38.996	16 14.26	21.52	33 46.62	41 6 25.78
92	9	$\begin{bmatrix} . & . & 45.5 \end{bmatrix} \begin{bmatrix} 1.0 \end{bmatrix} \begin{bmatrix} 15.3 \end{bmatrix} \begin{bmatrix} 30.0 \end{bmatrix} \begin{bmatrix} 44.8 \end{bmatrix} \begin{bmatrix} 59.2 \end{bmatrix} \begin{bmatrix} . & . \end{bmatrix}$	34 15.34	60.09	" 2 37.092	46 43.36	21.14	35 15.43	41 36 54.50
93	9	25.5 40.0 55.0 9.3	$34\ 25.52$	60.07	" 4 32.835	34 23.65	21.11	35 25.59	41 24 34.76
94	9	47.0 1.816.230.445.3	37 16.17	60.09	" 3 34.302	39 31.62	20.44	38 16.26	41 29 42.06
95	7.8	41.856.411.025.539.854.6 9.0	39 25.48	60.06	" 5 41.615	23 28.92	19.91	40 25.54	41 13 38.83
96	8	15.229.844.258.513.227.5	40 44.14	60.05	" 6 41.210	14 57.47	19.61	41 44.19	41 5 7.08
97	9	51.0 6.0	$42\ 21.91$	60.08	VII.3 44.302	33 43.60	19.23	43 21.99	41 23 52.83
98	9	10.5 25.0 40.0 54.2 9.0 23.8	44 39.79	60.09	IV. 2 45.555	41 48.86	18.67	45 39.88	41 31 57.53
99	8.9	24.5 39.5 54.2 9.0	47 8.71	60.07	III. 5 37.992	25 41.84	18.09	48 8.78	41 15 49.93
100 101	9 9	23.0 37.2 51.8 6.4 44.5 58.8 14.0 28.0 42.8 57.2	47 22.64 49 13.57	60.10 60.11	IV. 3 33.030 " 2 36.595	40 15.78 47 3.53	$18.03 \\ 17.58$	48 22.74 50 13.68	41 30 23.81 41 37 11.11
102	9	8.5 23.4 37.8 7.2 22.0 36.4	50 52.61	60.09	V. 3 36.268	38 23.22	17.19	51 52.70	41 28 30.41
103	9	3.0 17.5 32.0 46.8	53 2.88	60.09	" 3 34.618	39 20.40	16.68	54 3.97	41 29 27.08
104	8.9	58.212.827.442.056.711.226.2	57 42.12	60.10	IV. 3 34.362	39 29.57	15.57	58 42.22	41 29 35.14
105	6.7	$\begin{bmatrix} . & . & 16.2 & 31.0 & 45.2 & 59.5 & 14.5 & 29.0 & . & . & . \end{bmatrix}$	19 1 45.32	60.05	" 7 41.342	8 59.73	14.62	19 2 45.37	40 59 4.35
106	9	36.0 50.5 $ 5.2 20.0 34.0 49.0 $ $ 3.5 $	4 19.78	60.09	" 4 37.639	31 36.56	14.00	5 19.87	41 21 40.56
107	8.9	46.0 0.8 15.2 30.0	7 30.06	60.11	" 2 41.450	44 11.93	13.25	8 30.17	41 34 15.18
108	9	9.0 23.5 7.5 22.0 37.0	7 52.93	60.12	V. 1 40.890	50 25.16	13.18	8 53.05	41 40 28.34
109 110	$\begin{vmatrix} 8 \\ 8.9 \end{vmatrix}$	57.2 11.5 26.0 41.0 10.0 24.5	16 40.81	60.07	IV. 6 36.368 " 5 39.722	17 45.77 24 34.74	$11.11 \\ 10.80$	17 40.88 18 59.11	$\left \begin{array}{cccccccccccccccccccccccccccccccccccc$
110	8.9	$ \begin{vmatrix} 15.5 & 30.0 & 44.2 & 59.0 & 13.3 & 28.0 & 43.0 & & . \\ 43.0 & 58.0 & 12.5 & 27.2 & 42.0 & 56.5 & 11.0 & . & . & . \\ \end{vmatrix} $	17 59.03 23 27.21	60.08	II. 3 36.290	38 22.36	9.52	24 27.31	41 28 21.88
112	8	$\begin{bmatrix} 43.036.8 & 12.327.242.036.311.0 & & \\ 24.038.8 & 53.0 & 8.0 & 22.237.051.8 & & \end{bmatrix}$	24 7.84	60.10	IV. 3 39.498	36 31.00	9.27	25 7.94	41 26 30.27
113		55.0 10.0 38.8 53.4 8.0 22.4	27 38.86	60.10	II. 3 37.800	37 29.72	8.56	28 38.96	41 27 28.28
114	8	21.5 36.2 51.0 5.0 20.0 35.0 49.5	28 5.51	60.11	IV. 3 31.510	41. 8.77	8.45	29 5.62	41 31 7.22
115	9		28 40.41	60.13	VI. 2 32.693	49 16.13	8.31	29 40.54	41 39 14.44
116	8	$ 27.2 42.0 56.4 11.0 25.4 40.2 54.8 \dots$	37 11.03	60.08	IV. 4 40.178	30 8.43	6.35	38 11.11	41 20 4.78
117		46.0 1.0 15.0 29.2 44.0 58.8 13.0	40 29.60	60.07	" 5 41.225	23 42.63	5.61	41 29.67	41 13 38.24
118		22.0 36.2 51.2 20.4 49.6	46 5.82	60.08	" 3 44.430	33 39.46	4.43	47 5.90	41 23 33.89
119	1	19.2 34.0 48.5 3.0	47 33.90	60.09	" 2 43.902	42 46.45	3.98	48 33.99	41 32 40.43
120 121	$\begin{vmatrix} 9 \\ 7.8 \end{vmatrix}$	30.0 45.0 59.2 14.0 28.2	48 44.74 50 12.42	60.06	" 5 43.282 " 5 42.148	22 31.15 23 10.55	$\frac{3.73}{3.38}$	49 44.80 51 12.48	41 12 24.88 41 13 3.93
121	1	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	56 25.03	60.06	" 3 42.148 " 3 40.150	36 8.21	$\frac{3.36}{1.97}$	57 25.09	41 26 0.18
123	1	. 13.0 27.0 41.0 55.4 10.2 24.5	57 41.25	60.03	V. 6 36.980	17 24.36	1.68	58 41.28	41 7 16.04
124	1	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	19 59 5.86	60.08	1	44 58.68	1.35	$20 \ 0 \ 5.94$	41 34 50.03
								THE STATE OF THE S	
	<u> </u>				<u> </u>				

Number.	Magnitude.		SEC	ONI	os (OF	TRAI	TISN	S.	Т.	a		MICROMETER.	D.	đ.	As	n Right	De	n So	
Nu	Ma	1.	п. п	1.	ıv.	ν.	VI.	vII. 1	0. 11.							183	60.0.	183	0.0.	
						Zor	ne XX	VII.	Jun	е 17. H.	D.=	27 26	20′.0. n′.=	=-40 ["] .84. 1	n."=-	8.00.				
1 2 3	9 •9 9					15.5	$\begin{bmatrix} 46.25 \\ 5 \\ \\ 5.0 \end{bmatrix}$	0.0	1	56 2.98	$\begin{vmatrix} +59 \\ 8 \end{vmatrix} = 59$.48	r. V. 2 43.680 IV. 4 40.154 III. 4 39.010	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	-37 ["] .9	27 15 2 10 5	m. s. 26 20.75 57 2.46 58 39.69	27 56	5 39 ["] .9 5 59.7 7 38.8	9
4 5 6	9 7 9	50.5	36.0 48	. 2	$1.0 \\ 8.5$	 13.0 40.5	$\begin{vmatrix} \dots & 2 \\ \dots & \ddots & \\ 1 & \dots & 1 \end{vmatrix}$	5.2 .		$58\ 48.05$ $16\ 2\ 0.77$ $2\ 28.20$	59 7 59 59	.47 .51 .50	VII. 6 37.140 IV. 3 42.943 " 4 42.220	17 16.75 34 22.88 28 51.32	36.4 35.7 35.0	47 5 73 16 51	$ \begin{array}{r} 69 & 47.52 \\ 3 & 0.28 \\ 3 & 27.70 \end{array} $	27 44 28 1 27 55	13.2 18.6 46.9	22 31 z. 33 z.
7 8 9 10	8.9 8 9	29.4	42.0 .	. 4	3.0	55.2 19.(1 1	0.4		3 43.01 6 6.71	t 59 t 59	.50 .50 .50 .51	" 5 36.620 " 5 39.050 " 5 47.400 V. 5 35.830	26 17.52 24 53.62 20 5.19 26 44.80	35.3 35.3 34.7 34.0	32 75	3 35.61 4 42.51 7 6.21 7 28.91	27 51 27 46	3 13.1 48.9 5 59.9 3 39.4)4 z)4
11 12 13 14	8 7 9 7.8		36.2 48 	. 5	1.5	3.8	25.53 16.22	$8.0 \\ 8.3$.		8 0.64 8 51.34	59 59	.55 .52	III. 6 44.342 IV. 2 35.710 V. 4 44.078 IV. 7 43.020	13 8.31 47 18.05 27 47.10 8 2.95	34.3 34.3 34.3	30 10	9 0.63 9 0.19 9 50.86 20 58.13	28 14 27 54	2.6 12.3 141.2 154.3	35 z. 20 z.
15 16 17 18 19	9 8 5 9	56.2 5.2		$\begin{array}{c c} . & 1 \\ 2.6 & 5 \\ .0 & 3 \\ . & 4 \end{array}$	$8.5 \ 5.0 \ 3.2 \ 2.5$	30.0 7.0 46.0 55.0	$egin{array}{c} 42.85 \ 19.63 \ 58.01 \ \dots \ 1 \ \dots \ \end{array}$	$\begin{bmatrix} 5.2 \\ 2.0 \\ 0.5 \\ 9.2 \end{bmatrix}$.		21 17.99 22 54.83 24 33.40 24 42.47	59 5 59 6 59 7 59	.59 .56 .58 .59	V. 3 37.330 IV. 5 46.558 " 4 45.218 " 3 40.488 II. 5 35.322	37 36.76 20 34.22 27 7.75 35 47.71 27 2.30	31.3 30.3 30.3 29.6	10 2 73 2 85 2 81 2	22 17.58 23 54.41 25 32.98 25 42.06 28 49.20	28 4 27 47 27 53 28 2	1 27.8 7 24.9 3 58.1 2 38.0 3 51.9	36 95 z 10 92
20 21 †22 23	9 9 9 9 8.9		21.033	. 4 4	6.0	58.2 5.2 26.0	210.82 218.03 38.25	$\begin{bmatrix} 3.0 \\ 0.5 \\ 1.0 \end{bmatrix}$.		28 45.90 29 53.18 31 13.50	59 59 59 59	.57	IV. 7 32.989 V. 6 41.394 IV. 1 40.172 " 3 42.838	13 49.43 14 50.14 50 35.52 34 26.50	29.3 29.3 28.3 28.3	38 2 11 3 31 3	29 45.47 30 52.76 32 13.14 34 4.82	27 40 27 41 28 17	38.8 39.2 24.3	81 z 25 z 83 z
24 25 26 *27	7 8.9 9 8	0.657.8	$ \begin{array}{r} 13.2 \\ 26 \\ 10.2 \\ 22 \\ \hline 1.2 \\ \hline 13 \\ \hline 1.2 \\ \hline 13 \\ \hline 1.2 \\ \hline 13 \\ \hline 1.2 \\ \hline 13 \\ \hline 13 \\ \hline 13 \\ \hline 13 \\ \hline 13 \\ \hline 14 \\ \hline 15 \\ $	$\begin{array}{c} 0.03 \\ 0.83 \\ 0.5 \\ 0.0 \end{array}$	$8.0 \\ 5.2 \\ \cdot \cdot \cdot$	50.2 47.2 • •	$\begin{bmatrix} 2 & 3.0 & 1 \\ 2 & . & . & 1 \\ . & . & . & . \end{bmatrix}$	5.2 . 2.5 .		34 38.09 36 35.15 40 26.03 40 44.50	59 5 59 3 59 5 59	.64 .64 .60	" 2 36.644 " 3 33.992 I. 7 37.130 IV. 6 37.972 " 6 34.462	46 45.78 39 32.07 11 26.06 16 48.34 18 49.62	28.0 27.0 26.0 26.0	05 3 61 3 74 4 66 4	35 37.73 37 34.79 41 25.63 41 44.11 43 2.92	28 13 28 6 27 38 27 43	33.8 319.6 312.8 35.0 35.9	8 3 z 68 80 z 00
28 29 30 31	8 9 9		38.5 51 	.0	1.0	• •	$\begin{bmatrix} 28.2 & 4 \\ . & . & 2 \\ 36.0 & 37.8 \end{bmatrix}$	6.0		42 49.85 45 11.47	5 59 7 59	.64 .66	" 4 35.716 " 3 36.326 V. 3 38.092	32 35.96 38 11.47 37 10.47	26 25 25	17 4 51 4	13 49.49 16 11.13 16 12.84	27 59 28 4	22.1 57.0 56.0	1 3)8
32 33 34 35	8.9 8.9 8		58.8 11 29.0 .	.0	7.0	 59.0	11.5	1.0		48 23.64 48 53.76 49 46.78	59 5 59 5 59	.69 .66	VII. 5 39.868 II. 2 36.385 IV. 2 40.534 " 5 36.875	24 25.00 46 54.66 44 29.94 26 8.73	25.4 24.8 24.1 24.3	35 4 73 4 52 5	16 53.07 19 23.33 19 53.42 50 46.43	28 13 28 11 27 52	14.6 2 53.2	51 57 25
36 37 38 39	9 8 8 9		10.2 25.0 37	.23 .3	$\begin{array}{c} 4.0 \\ 5.0 \\ 0.0 \end{array}$	46.0 47.2 2.2	15.0	$\begin{bmatrix} 1.0 \\ 2.0 \\ . \end{bmatrix}$		52 34.89 54 49.90	59 59 5 59	.68 .64 .68	" 2 42.580 " 6 39.260 " 3 41.003 " 3 42.890	43 20.71 16 3.88 35 29.90 34 24.70	24.3 24.0 23.8 23.3	09 5 84 5 80 5	51 29.42 52 33.38 53 34.57 55 49.65	27 42 28 2 28 1	5.0 2 47.9 2 13.7 8.0)7 ′4 00
40 41	$\frac{9}{8.9}$	17.5	30.542				$\begin{bmatrix} 54.6 \\ 2 \\ \end{bmatrix}$			10 55 55 05	1		V. 3 36.688 II. 4 45.022	35 58.90 27 14.41	23.1 22.3	H	56 29.25 58 55.05		42.0 56.9	
		I	1 1		(COR	RECTIO	ons.						INSTRU	MENT	READING	s.	1		•
			COR. TO	о п	iouri	LY				ZENITH					CIR	CLE.			THER	RMOM.
			CLOCK		COR		m.	n.	с.	POINT.	COINC.			Α.	в.	с. р.	Mean.	BAR.	At.	Ex.
June 1	7, at 10	6h	*. +48.42	0	+0.0)25	*. +0.198	$^{s.}_{+0.39}$	$6 \begin{vmatrix} s \\ +0.2 \end{vmatrix}$	47 359° 59′ 58′.16	r. 40.154	Zone XXV		8 293° 12′ 0′.6 0 1.4 2 2.4		11".4 7".5 14.0 9.0	6.25	g i	73°.0 72.2 71.0	69°.0 68.0 65.7
					-	1	Double													

er.	itude.	SECONDS OF TRANSITS.						Mean Right	Mean South
Number.	Magnitude.	т. п. пт. гу. у. ут. уп. 10. 11	Т.	a.	MICROMETER.	D.	d.	Ascension. 1850.0.	Declination. 1850.0.
		Zone XXVII. June 17. I	I. $D = -27^{\circ}$	26 ['] 20 ^{''} .0.	n'==-40".84.	n'.= -8.	′00. (С	ontinued.)	
42	9	12.525.0 49.5	h. m. s. 16 58 24.86	+59.70	IV. 3 43.232	—34 1292	-22.42	h. m. s. 16 59 24.56	28° 0′ 55″.34
43	8.9	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	58 41.06 17 3 38.56	59.66 59.67	VII. 6 41.230 IV. 7 39.373	14 55.49 10 8.93	22.36	59 40.72	27 41 37.85
45	8.9	21.033.245.258.010.223.035.0		59.69	" 5 46.260	20 44.56	$21.15 \\ 20.81$	17 4 38.23 5 57.67	27 36 50.08 z. 27 47 25.37 z.
46	8.9	39.251.8 4.0 17.0 41.0	1	59.68	" 7 41.200	9 5.84	20.30	8 3.82	27 35 46.14 z.
47	8	53.0 5.5 18.5 30.0 7.0	8	59.69	" 6 40.660 " 4 41 420	15 15.48	20.20	8 29.95	27 41 55.68
49	8.9	9.3 22.0 46.5 58.7 11.2 23.4 .		59.72 59.72	" 4 41.420 " 5 40.160	29 18.97 24 15.28	$19.64 \\ 19.10$	10 46.18 12 51.46	27 55 58.61 27 50 54.38
50	6.7	18.231.043.255.5 7.820.633.0	12 55.64	59.73	" 3 45.550	32 52.79	18.85	13 55.37	27 59 31.64 z.
51	9	$ \cdot \cdot \cdot \cdot \cdot \cdot 23.0 35.5 48.0 \cdot \cdot .$	14 10.64	59.76	" 2 36.352	46 55.91	18.53	15 10.40	28 13 34.44
52	7.8	11.0 23.8 36.0 48.5 0.5 13.2 25.5	15 48.42	59.77	" 1 41.290	49 56.91	18.12	16 48.19	28 16 35.03 z.
*53 54	9	36.5 49.0 1.5 26.0 39.0	1	59.75	" 3 39.099	36 35.67	17.77	18 13.66	28 3 13.44
55	9	$egin{array}{ c c c c c c c c c c c c c c c c c c c$	18 24.19 20 27.99	59.75 59.79	VI. 3 41.133 IV. 1 39.442	35 25.31 51 0.76	$17.42 \\ 16.95$	19 23.94 21 27.78	$\begin{array}{ c cccccccccccccccccccccccccccccccccc$
56	9		1	59.76	" 3 44.800	33 18.72	16.68	22 30.48	27 59 55.40 z.
57	9	$\begin{bmatrix} \cdot \cdot \end{bmatrix} \cdot \begin{bmatrix} 28.0 & 41.0 & \cdot \end{bmatrix} \cdot \begin{bmatrix} \cdot \cdot \end{bmatrix} \cdot \begin{bmatrix} \cdot \cdot \end{bmatrix} \cdot \begin{bmatrix} \cdot \cdot \end{bmatrix}$	R .	59.76	VII.3 45.030	33 10.44	16.64	$22\ 40.50$	27 59 47.08
58 59	8 9	$oxed{6.0} \ \cdot \ \cdot \ 31.0 43.0 55.5 \ 8.2 21.0 \ \cdot \ \cdot \ 36.0 39.0 51.0 \ \cdot \ \cdot \ \ \ \ \cdot $	24 43.36	59.78	IV. 3 34.570	39 12.07	15.85	25 43.14	28 5 47.92
60	9	$\begin{bmatrix} 36.0 & 39.0 & 51.0 & . & . & . & . & . & . & . \\ . & 4.0 & 16.0 & 29.0 & . & . & . & . & . & . \end{bmatrix}$		59.79 59.78	II. 2 44.428 IV. 3 38.842	42 16.82 36 44.53	15.25 15.13	28 3.43 28 28.55	28 8 52.07 28 3 19.66
61	7		27 45.45	59.77	V. 4 39.461	30 26.61	15.06	28 45.22	27 57 1.67
62	8		28 33.00	59.81	IV. 1 37.050	52 23.38	14.85	29 32.81	28 18 58.23 z.
63	8.9	39.2 52.2 4.5 16.7 29.0 54.0	30 16.77	59.76	II. 5 44.503	21 45.11	14.42	31 16.53	27 48 19.53 z.
64 65	9	$\begin{bmatrix} \cdot \cdot \end{bmatrix} \cdot \begin{bmatrix} \cdot \cdot \end{bmatrix} \begin{bmatrix} 34.0 & 46.0 & 58.5 \\ 59.5 & 59.5 \end{bmatrix} \begin{bmatrix} 59.0 & 59.5 \\ 59.5 & 59.5 \end{bmatrix} \begin{bmatrix} 59.0 & $	1	59.79	IV. 3 35.650	38 34.78	14.33	31 33.40	28 5 9.11
66	7.8	52.5 5.0 17.3 29.6		59.81	" 2 35.462 " 5 44.390	47 26.66 21 49.17	13.93 13.72	33 4.73 33 51.43	28 14 0.59 z. 27 48 22.89
67	9	$ \cdot \cdot \cdot $		59.80	" 3 33.516	39 48.48	13.12	35 9.37	28 6 21.85 z.
68	9	$ \cdot \cdot \cdot \cdot 44.0 \cdot \cdot 8.5 21.0 \cdot \cdot \cdot \cdot $	34 56.27	59.79	" 4 36.830	31 57.49	13.17	35 56.06	27 58 30.66 z.
69 *70	9 6.7	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	8	59.79	1. 4 34.693	33 10.48	12.87	37 3.90	27 59 43.35
71	8.9			59.77	IV. 5 47.350 " 2 40.080	20 6.92 44 47.10	12.59 12.25	38 7.31 $39 22.58$	27 46 39.51 28 11 19.35
72	9	33.045.458.010.2		59.81	" 3 36.535	38 4.21		40 32.83	
73	9	31.0 43.4 55.6 8.3 21.0		59.78	" 5 47.110	20 15.19	$11.94 \\ 11.63$	40 32.83	28 4 36.15 27 46 46.82
74	9	16.2 28.8 41.2 53.2 5.8 18.6 31.0	42 53.58	59.81	" 3 42.840	34 26.43	11.05	43 53.39	28 0 57.48
75 76	9 7	8.6 21.4 33.6 46.0 58.2 10.8	i	59.81	" 4 38.160	31 11.56	10.56	45 45.82	27 57 42.12
77	9	$\begin{bmatrix} 36.2 & 49.0 & 51.8 & 14.0 & 26.0 & . & . & . & . \\ . & . & . & . & 19.5 & 32.0 & 44.0 & 57.0 & . & . & . & . \end{bmatrix}$		59.82 59.83	" 3 40.722 " 3 36.628	35 39.59 38 1.00	$\begin{array}{c} 10.16 \\ 10.09 \end{array}$	47 13.60 47 31.78	28 2 9.75 28 4 31.09
78	9	$ \cdot \cdot \cdot \cdot 28.0 41.0 53.0 5.5 \cdot \cdot \cdot \cdot \cdot $		59.83	" 2 45.235	41 49.04	9.78	48 40.51	28 8 18.82
79	9	$ \cdot\cdot \cdot\cdot 29.0 42.0 54.0 6.3 $	B	59.84	" 2 47.390	40 34.61	9.77	48 41.49	28 7 4.38
80 81	9	$\begin{vmatrix} \cdot \cdot & \cdot & 39.0 & 51.0 & 3.4 & \cdot & 28.4 & \cdot & 1.5 & 54.0 & \cdot & 29.0 & \cdot & 1.5 & 1$	5	59.83	" 3 40.678 " 4 43.682	35 41.10	9.48	49 51.01	28 2 10.58
82	8.9	12 225 2		59.82	1 10 000	28 0.78	9.25	50 41.47	27 54 30.03
83	9.9	· · · ·		59.81	" 5 37.888 " 4 40.154	25 33.75 30 2.69	8.79	52 24.64 53 0.31	27 52 2.54
84	7.8	$\begin{bmatrix} \cdot \cdot & \cdot & 48.0 & 0.5 & \cdot & \cdot & \cdot \\ \cdot & \cdot & 3.0 & 15.2 & 28.0 & 40.0 & 52.4 & 5.0 & \cdot & \cdot \end{bmatrix}$		59.82 59.81	" 4 40.154 " 5 42.825	22 43.19	$8.63 \\ 8.51$	53 0.31 53 27.55	27 56 31.32 27 49 11.70
85	9	$ \cdot \cdot \cdot \cdot \cdot \cdot 16.0 29.0 41.4 $	1 _	59.82	" 4 43.710	27 59.82	8.35	54 3.82	27 54 28.17
86 87	8.9	17.0 29.4 42.0 54.2 6.4 19.0 31.2	i	59.82	II. 5 41.060	23 44.08	7.85	55 54.02	27 50 11.93 z.
88	8	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		59.84 59.83	I. 3 44.444 IV. 4 46.810	33 30.72 26 12.73	$\begin{array}{c} 7.30 \\ 6.98 \end{array}$	57 55.75 59 7.73	27 59 58.02 27 52 39.71 z.
89	8	$ \cdot \cdot \cdot \cdot 15.2 27.5 40.0 52.0 \cdot \cdot \cdot \cdot $	1	59.82	" 5 44.900	20 12.73	6.89	59 27.32	27 47 58.42 z.
90	8	$ \cdot\cdot \cdot\cdot \cdot. 50.0 \cdot. 15.0 27.2 \cdot. \cdot.$	58 50.07	59.82	" 5 50.030	18 34.32	6.79	59 49.89	27 45 1.11 z.
91	8.9	$ \cdot\cdot \cdot 51.5 4.0 16.5 29.0 $	18 0 4.07	59.87	" 2 41.290	44 5.31	6.48	18 1 3.94	28 10 31.79 z.
92	8.9	$ \cdot $ 52.0 4.4 17.0 29.2 42.0	k .	59.85	II. 3 38.382	37 0.36	6.13	$2\ 16.79$	28 3 26.49 z .
93	8.9	21 044 055 0 0 0 1 5 0 4 0	1	59.87	IV. 2 31.828	49 32.14	5.90 5.96	3 8.87	28 15 58.04 z. 28 1 3.07
		31.8 44.3 57.0 9.0 21.5 34.0	10 4 9.10	59.84	II. 3 42.510	34 37.71	5.36	18 5 9.02	≈0 I 3.01



Number.	Magnitude.		SEC	ONE	os o:	FΤ	'RAN	SIT	s.		т.	a.		MICROMETER.	D.	d.	li li	Right	1	n Sou linatic	
Nun	Mag	ı.	11. 1	11.	ıv.	v.	vi.	vII.	10.	11.							185	50.0.	185	0.0.	
				Zone	XX	VII		June	17.	Н.	D. =-2	$7^{\circ}\ 26^{'}\ 20$		n.'=-40.'84.	n"=-8	.ő0.	(Continu	red.)			
95	9	34.0	46.45								h. m. s. 18 5 11.41	+59.	86	II. 2 47.052	-40 46.16	- 5.0	9 18	m. s. 6 11.27	1	11.25	
$\frac{96}{97}$	9 7.8				$egin{array}{c} 0.05 \ 1.34 \end{array}$						5 39.80 6 31.34	59.59.59.		IV. 2 45.080 " 5 48.410	41 54.38 19 30.30	$\frac{4.9}{4.7}$	1	6 39.66 7 31.15	1	19.34 55.03	
98	9		.		8.82	1.0	33.34				7 8.58	59.		" 4 43.228	28 16.50	4.5	1	8 8.41		41.07	
99 1 00	8.9		3.31 28.04				17.5				10 27.91 18 10 52.72	59. 59.		V. 1 43.190	44 17.55 48 51.23	$\frac{3.6}{3.5}$		$\begin{array}{c} 11 \ 27.77 \\ 11 \ 52.58 \end{array}$	1	$\frac{41.22}{14.79}$	
		1	1 1	AVAITA AVAITATION	Z	one	XXV	7III.		June 1	8. M.	D. =-	-26°	25' 20.0. n'. =	=70.90.	n'.=-	-6.00.				
1	8			i	8.5		1				16 50 58.69	60.		8	34 49.09	68.2	8	51 59.25		17.30 43.50	
$\frac{2}{3}$	9	1::		- 1	5.05	 57.0		32.0			50 55.06 53 44.91	60. 60.		VII. 3 39.62 IV. 5 37.79	36 15.33 25 35.19	68.2 67.5	i i	51 55.63 54 45.46		$\frac{45.5}{2.7}$	
4	8						1				53 41.32	60.	57	VI. 4 34.50	33 15.81	67.5	Ħ	54 41.89		43.3	
5 6	8.9	· ·	1 1			٠.	٠٠	1		33.7	54 26.30 55 49.69	60.		11. 1 40.57 10. 6 36.64	50 18.73 17 31.99	67.3	1	55 26.89 56 50.24	1	46.19 59.0	
7	$\begin{vmatrix} 9 \\ 8.9 \end{vmatrix}$		1 1					20.3			58 17.11	60.		2. 7 36.75	11 37.24	66.5	8	59 17.65		3.7	
8	7.8		26.03	8.0							17 1 50.43	60.		2. 5 39.44	$24\ 37.71$	65.6	8	251.00		3.3	
9 10	$\begin{vmatrix} 9 \\ 7 \end{vmatrix}$	16 6	$\begin{vmatrix} \cdot \cdot \\ 29.0 \end{vmatrix}_4$		5.5		1	• •		• • •	2 15.66 3 53.13	60.		III. 5 41.39 2. 5 44.67	23 30.86 21 37.04	65.3 65.1	i	3 16.23 4 53.70	1	56.49	
		10.0						• •	• •								ı				
11 12	8	::		9.0	1	· · · · · · · · · · · · · · · · · · ·	6.3	 19.0			10 31.71 11 41.80	60.		2. 2 40.19 IV. 1 42.38	44 40.64 49 17.05	63.2 63.2	Я	11 32.34 12 42.44		$\frac{4.2}{40.3}$	
13	9.10	1	4.21				l				18 28.52	60.		2. 7 40.45	9 29.48	61.6	a	19 29.11	1	51.0	
14	9		5		- 1		1				20 10.36	60.		I. 3 35.70	38 30.72	61.9	8	21 11.00		51.9	
$\frac{15}{16}$	$\begin{vmatrix} 8.9 \\ 8 \end{vmatrix}$		$\begin{vmatrix} 0.5 \\ 19.0 \\ 3 \end{vmatrix}$				49.0				24 24.66 28 43.28			2. 7 36.85 2. 5 40.21	11 33.79 24 11.11	60.1 59.0	H	25 25.27 29 43.92	1	53.9	
17	8.9	::	1		10.0						30 40.10	1		V. 1 37.20	52 15.94	58.6	i i	31 40.79		34.5	
18	8			- 1			• •	19.5			31 42.66	1		IV. 6 33.23	19 30.29	58.3	B	32 43.29		48.6	
19 20	$\begin{vmatrix} 8 \\ 7.8 \end{vmatrix}$		$\frac{56.8}{13.52}$			• •		• •			34 21.40 35 38.29			2. 2 42.78 2. 4 43.59	43 11.16 28 1.47	57.3 57.3		35 22.08 36 38.95	ì	28.8 18.8	
21					-		29.0		1						28 44.09	56.	į.	39 4.92		0.8	
22	7 8						29.0				$38 4.25 \\ 39 42.93$	Į.		VII. 6 33.63	19 16.20	56.	9	$40 \ 43.59$	1	32.5	
23	7						22.0		1		39 57.29	60.	68	" 4 32.92	34 10.27	56.9	29	40 57.97	27 (26.5	
24	8.9	• •	• •	• •	• •	• •	1 1	55.0	1	40.0	41 18.12			9	23 27.20 24 39.85	55.9	1	42 18.78 42 42.58		43.1 55.7	
$\frac{25}{26}$	$\begin{vmatrix} 8.9 \\ 7 \end{vmatrix}$							$\frac{\cdot}{45.5}$	1	49.0	41 41.92 43 8.52		.66 .71	8	48 0.10	55.8 55.4	1	$\frac{42}{42}$ $\frac{42}{30}$		15.5	
27	8						1 1	44.8	1		44 8.07			ii .	9 5.91	55.5	24	45 8.71	26 35	21.1	5
28	8		• •	$\cdot \cdot $	2.0		1 1			• •	46 1.92		.66	i i	18 9.90	54.		47 2.58	1	24.6	
29 30	8	: :	48.0		12.0		51.2	9.6			46 32.58 17 49 12.28	1	.70 .70	9	40 16.76 36 53.79	54.	ă	47 33.28 50 12.98	1	31.4 7.7	
					(CORI	RECTI	ons	•						INSTRU	MENT I	READING	š.			
			007	mc	norr						77		-	and the second s		CIR	CLE.			THER	mom.
			CLOC	- 1	COR		m.	1	n.	c.	ZENITH POINT.	COINC.			Δ.	в.	С. р.	Mean.	BAR.	At.	Ex.
June	18, at	16h	s. +49.3	390	s. +0.0)20	s. +0.198	3 +0	s. .396	$s. \\ +0.247$	359°59′59′56	r. 40,105	Z X	Tone. XVIII.—June 18, 1	h. 6.8 294° 12′ 14′.0	16.0	22'.4 20'.	4 18.20	ı. 29.997	73°.4	70°.1
			1 10.0		, ,,,,		, - 1200	1.0		1	332 00 00.00			1	7.4	$\cdot \cdot \cdot $			29.980	73.0	70.0
															9.0	12.8	14.4 21.	16.80	29.950 29.930	71.6 71.0	69.0

ber.	Magnitude.		SE	CON	NDS	OF	TRA	NSI'.	rs.		Т.	a.	MICROMETER.	D.	d.	Mean Right Ascension,	Mean South Declination
Number.	Magn	ı.	и.	ш.	IV.	v.	vi.	vII.	10.	11.			A CANADA			1850.0.	1850.0.
`				Zon	e XX	CVII	Ι.	Jun	e 18.	I	H. D.=-2	$ \hat{6} \ 25^{''} \ 20^{'}.0. $	n. = -70.9	0. ".=-	6.00. (Continued.)	
31	8.9		35.5			12.0	25.0				$17 {}^{h.} {}^{m.} {}^{s.} 17 {}^{0.07}$	+60.70	2. $4\ 37.51$	31 31 .50	_53.51	$^{h.\ m.\ s.}_{17\ 52\ 0.77}$	26° 57′ 45″.01
32	8						1	58.0	1		$52\ 21.05$	60.71	VII. 3 36.50	38 3.14	53.17	53 21.76	27 4 16.31
33	7						1	54.0		• •	53 17.11	60.69	" 5 37.56	25 42.87	52.93	54 17.80	26 51 55.80
34	7				• •	• •		54.0			54 17.12	60.69	" 5 39.27	24 43.85	52.68	55 17.81	26 50 56.53
35 36	8.9 8	• •	• •		• •	٠.			36.0	$40.3 \\ 42.0$	54 41.20 55 34.21	60.72 60.70	11. 2 45.99 " 3 45.99	41 20.04 32 34.80	52.58 52.34	55 41.92 56 34.91	27 7 32.62 26 58 47.14
37	8						1	17.0	- 1		57 39.99	60.75	VII. 1 35.29	53 21.69	51.82	58 40.74	27 19 33.51
38	8.9							4.5			58 27.79	60.67	" 7 43.13	7 57.19	51.61	59 28.46	26 34 8.80
39	8	17.0	29.0	41.5	1 1	6.5	19.0	31.0			18 2 54.05	60.75	I. 1 43.48	48 38.84	50.48	18 3 54.80	27 14 49.32
40	6				39.0	51.0	3.6				8 38.90	60.74	" 3 34.35	39 17.40	49.00	9 39.64	27 5 26.40
41	9				2.5	14.5		39.5			12 2.45	60.73	2. 4 36.10	32 20.19	48.14	13 3.18	26 58 28.33
42	9		٠.	5.6			42.8		- 1		14 18.01	60.69	2. 7 43.50	7 44.15	47.55	$15\ 18.70$	26 33 51.70
43	7	45.0	57.1	9.5		٠.				[16 21.79	60.71	1. 6 37.54	17 0.60	47.03	17 22.50	26 43 7.63
44	7	• •		٠.	• •			20.5			17 43.62	60.73	VII. 5 39.91	24 21.73	46.68	18 44.35	26 50 28.41
$45 \mid 46 \mid$	7.8 8		$\frac{.}{28.5}$	 40 5	• •	• •	• •		31.0	- 1	18 36.23 21 52.85	$60.71 \\ 60.70$	11. 6 42.52 2. 7 40.58	14 8.60	46.44	$\begin{array}{c} 19 \ 36.94 \\ 22 \ 53.55 \end{array}$	26 40 15.04 26 35 30.54
47	8		20.0				16.0	28.0			21 51.16	69.78	2. 7 40.58 VII, 1 35.575	9 24.95 53 11.80	45.59 45.59	22 51.94	27 19 17.39
48	9.10				1		33.5	1			23 9.07	60.75	" 4 35.87	32 28.38	45.26	24 9.82	26 58 33.64
49	8.9	٠.							31.8		23 37.18	60.74	11. 5 33.50	28 2.54	45.15	24 37.92	26 54 7.65
50	8.9						8.5	20.8			$25 \ 43.81$	60.79	III. 1 37.55	52 3.81	44.59	$24\ 44.60$	27 18 8.40
51	9	7.5	20.2	32.3	45.0						30 44.72	60.75	1. 5 36.30	26 25.87	43.30	31 45.47	26 52 29.17
52	9						47.5				32 22.82	60.78	VII. 3 28.70	42 32.48	42.88	33 23.60	27 8 35.36
53	5	٠.					41.0	53.3			$35\ 16.43$	60.78	IV. 2 44.51	$42\ 11.92$	42.12	36 17.21	27 8 14.04
54	8.9				32.0				• •		37 32.21	60.79	" 1 43.71	48 31.09	41.53	38 33.00	26 14 32.62
55	9	• •		1	48.3			• •		٠٠١	38 48.27	60.73	II. 7 43.38	7 48.71	41.20	39 49.00	26 33 49.91
$\frac{56}{57}$	8 8	• •		• •	1	3	$38.4 \\ 53.0$	1		٠.١	39 13.73 40 28.58	$60.80 \\ 60.77$	VII. 1 39.11 IV. 4 39.94	51 9.74 30 8.08	$41.09 \\ 40.76$	40 14.53 41 29.35	27 17 10.83 26 56 8.84
58	6.7		: :		7.5		05.0		1		42 7.77	60.76	I. 5 41.71	23 19.56	40.70	43 8.53	26 49 19.90
59	8						2.0	- 1	1		42 37.80	60.73	IV. 7 43.30	7 51.57	40.21	43 38.53	26 33 51.78
60	8			4.7	17.0	29.2					$44\ 17.03$	60.79	V. 3 36.14	38 15.75	39.78	45 17.82	27 4 15.53
61	9						11.5	24.0			45 46.95	60.78	VI. 3 37.66	37 23.16	39.39	46 47.73	27 3 22.55
- 1	9.10		1	9	56.2				1		47 56.31	60.80	I. 2 35.80	47 12.52	38.83	48 57.11	27 13 11.35
63	9				7.0	19.0	31.5				49 - 6.93	60.75	IV. 6 39.78	15 44.08	38.52	50 7.68	26 41 42.60
- 1	8.9				50.0				- 1]	51 49.97	60.74	I. 7 42.36	8 23.80	37.82	$52\ 50.71$	26 34 21.62
35	7.8	• •	• •	٠.	• •	1	13.0			٠ ٠	57 48.19	60.80	VII. 3 36.89	37 49.63	36.26	58 48.99	27 3 45.89
36 37	7.8	• •	• •	• •	• •	1	55.2		54.0	6.3	$\begin{array}{cccc} 19 & 0 & 30.62 \\ & 0 & 59.37 \end{array}$	$60.77 \\ 60.76$	" 5 46.42 11. 6 41.28	20 36.92	35.57	19 1 31.39	26 46 32.49
88	9				39.0	: :	• •		- 1	0.5	2 39.21	60.76	III. 1 43.36	$14 \ 51.47 \\ 48 \ 43.17$	$35.44 \\ 35.02$	$ \begin{array}{ccc} 2 & 0.13 \\ 3 & 40.03 \end{array} $	26 40 46.91 27 14 38.19
39	7				37.5						3 37.40	60.81	V. 2 46.80	40 52.81	34.78	4 38.21	27 6 47.59
70	9		- 1		44.1						5 44.03	60.79	2. 4 46.47	$26\ 23.05$	34.24	6 44.82	26 52 17.29
71	9.10		26.0	37.6	50.5						9 50.29	60.78	2. 6 37.40	17 5.78	33.21	10 51.07	26 42 58.99
2	9.10	1		- 1							13 45.09	60.80	IV. 3 43.35	34 6.88	32.24	14 45.89	26 59 59.12
3	9.10						38.7	51.0		[14 14.01	60.83	VII. 1 37.69	51 58.77	32.12	15 14.84	27 17 50.89
4	7.8						51.5			[16 26.80	60.77	1. 7 38.27	10 45.04	31.57	$17\ 27.56$	26 36 36.61
5	6.7		1		- 1	1	59.0		1	• •	19 34.37	60.84	2. 1 38.65	51 25.34	30.79	20 35.21	27 17 16.13
6	8.9	• •	• •				• • 25 0	- 1			25 39.74	60.77	IV. 7 36.85	11 34.30	29.27	26 40.51	26 37 23.57
77 78	$\frac{8}{9}$	• •		58.U	±0.33	- 1	$35.0 \\ 11.0$	1			32 10.35 33 46.35	$60.79 \\ 60.80$	I. 5 44.76 IV. 4 43.66	$\begin{array}{c} 21 \ 34.21 \\ 27 \ 59.58 \end{array}$	$27.65 \\ 27.25$	33 11.14 $34 47.15$	26 47 21.86 26 53 46.83
79	9					- 1	37.5				34 13.01	60.79	VII. 5 42.96	22 36.40	27.25	34 47.15 35 13.80	26 48 23.54
30	8							- 1	33.04	8	34 38.25	60.83	11. 2 41.82	43 44.04	27.14 27.05	35 39.08	27 9 31.09
31	7.8										36 47.97	60.80	IV. 4 48.55	25 10.69	26.50	37 48.77	26 50 57.19
32	8.9				40.0			45.5			19 37 8.53	60.84	VII. 1 49.21	45 20.90	$\begin{array}{c} 26.30 \\ 26.42 \end{array}$	19 38 9.37	26 50 57.19
		1					- 1		1	- 1						50 0.01	1102



	de.		SE	CON	DS	OF	TRA	NS	TS.								Ι.		~			
Number.	Magnitude.	ı.	п.	ш.	IV.	!		VII	Ι	11.	Т.	a.		MICROMETER.	D.	d.	I		Right ension,		n Sou dination of the second o	
				Zone	XX	VII	1.	Jui	ne 18.	м	. D.=5	26° 25′ 20	0.00	. n.'=-70.'9	0. n''=-6	5.00.	(C	ontinu	ed.)			
83	8			32.5		57.	0				h. m. s. 19 39 44.88	+60		I. 5 50.70	-18 9".07	—25 ["] .'	77	h. n 19 40	n. s. 45.67	26 43	54.8	4 z.
	8						5 34.		0		40 9.22	60	.83	VII.3 34.40	39 15.66	25.0		41	10.05	27 5		
	8		• •				0	1	. • •	• •	43 57.90	1		IV. 3 49.70	30 27.44	24.	4		58.71	26 56		
86	6	٠.		25.0	38.0		1				45 37.74			V. 6 39.68	15 47.48	24.	ı		38.53	26 41		
1	8 9		• •		٠.		1	42.	- 1		$\begin{array}{ccc} 45 & 41.54 \\ 47 & 5.75 \end{array}$	1	.81 .78	11. 4 39.00 VII. 7 37.66	$ \begin{array}{c c} 30 & 39.74 \\ 11 & 6.07 \end{array} $	24.3 23.9			42.35	26 56		
89	6				• • 47.5	1	12.	1			48 47.78	1	.78	V. 7 39.47	10 3.81	23.	8		$6.53 \\ 48.56$	26 36 26 35		
90	9								1	0	48 50.91			10. 6 39.44	15 55.34	23.			51.70	26 41		
91	8.9							22.	8		50 46.03		.78	V. 7 35.97	12 4.67	23.			46.81	26 37		
92	8.9		٠.	57.0	9.0	21.	5	•	.		54 9.24	60	.79	2. 6 34.28	18 53.52	22.	23	55	10.03	26 44		
93	8			49.5	1.5	14.	$0 \dots $.	.		55 1.72	60	.84	VI. 2 34.00	48 14.84	22.	02	56	2.56	27 13	56.8	6 z.
94	8.9						10	7 15.	1		56 38.08	1		II. 5 37.29	25 52.38	21.	8		38.89	26 51		
95	7.8					9.	$0 \dots $	34.	2	1 1	58 53.34		.78	I. 6 43.68	13 29.14	21.	8		54.12	26 39		
- 1	9.10			37.5		2.	0 14.	5 .	.		20 2 49.91	60	.78	VII. 6 45.56	$12\ 24.22$	20.	13	20 3	50.69	26 38	4.3	9
97	9						0				10 36.90		.78	2. 7 37.25	11 19.98	18.	30		37.68	26 36	58.2	8 z.
1		51.0								1 8	13 28.26			I. 2 36.20	46 58.73	17.			29.10	26 12		
99 100	$\frac{8}{9.10}$		19.8			1	$\frac{2}{9}$.	1	- 1		15 44.36	1		2. 3 38.90	36 39.93	17.0			45.18	26 2		
	$\frac{9.10}{10.9}$	• •	 59 5				$\begin{bmatrix} 0 \\ 1 \end{bmatrix} \dots$				17 26.16 19 17.83	ì	.82 .82	VII. 2 46.69 II. 3 35.89	40 56.39	16.5 16.5			26.98 18.65	26 6		
i		$\frac{14.0}{1}$									25 51.11	60		IV. 1 38.39	38 24.30 51 34.87	14.			51.95	$ \begin{array}{c cccc} 26 & 4 \\ 26 & 17 \end{array} $		
						1		1														
$\begin{bmatrix} 103 \\ 104 \end{bmatrix}$	7	• •	• •		i	1	5 59.	1 -	1		31 35.21	1	.83	" 2 40.55	44 28.70	13.			36.04	26 10		
105	9		 12 በ	 30.5	49 8	54	8 7.		- 1	1 1	31 25.80 33 42.63		.76 .79	VII. 7 46.53 VI. 5 45.10	$\begin{array}{c c} 5 & 59.78 \\ 21 & 22.63 \end{array}$	$\frac{13}{12}$.			26.56 43.42	26 31 26 46		
106	9			10.0					- 1	1 1	36 22.42		.78	2. 6 36.62	17 32.69	12.	N N		23.20	26 43		
107		45.0						- 1	1		37 21.90		.80	I. 4 36.64	32 1.78	12.			22.70		33.9	
108	9				ı		8	1	- 1		39 24.53	1	.79	VII. 4 43.87	27 52.09	11.	1		25.32	26 53		
109	8			47.5		12.	0 24.	5 36 .	6	$ \cdot $	43 59.82	60	.79	2. 4 44.19	27 40.79	10.	71	45	0.61	26 53		
110		14.4							$0 \cdot $		$46\ 51.29$	60	.79	2. 5 36.50	$26\ 19.25$	10.	10	47	52.08	26 51	49.3	5
111		14.0									48 51.20		.76	IV. 7 40.62	9 24.09	9.			51.96	26 34		
112	9.8	٠.	• •	25.0	37.5	49.	$5 \cdot \cdot$	14.	3		58 37.37	60	.81	2. 1 46.40	46 57.70	7.	60	59	38.18	27 12	25.3	0 z.
113	9		42.0		6.5	18.	2 31.	0 43 .	3		21 0 6.37	60	.77	· II. 5 46.58	20 31.49	7.	28	21 1	7.14	26 45	58.7	7 z.
114	8			1	1	1	0 21.			[$2\ 56.83$	1	.82	I. 1 35.27	53 22.38	6.	68	3	57.65	27 18		
115	8	• •	• •	• •	57.0	9.	0 21.	5 33 .	8	• •	21 4 57.00	60	.74	VII. 7 46.25	6 9.44	6.	27	21 5	57.74	26 31	35.7	1 z.
					1	\mathbf{Z}_{01}	ne X	XIX	•	June 2	1. M.	D.=-	39° 4	49 ['] 10		<u>"=</u>	$15\overset{''}{.}00$			The second second		
,	r/	00.0	40.0	F1 ~		00	-		-		10.86.10.00		0-	1 0 47 07	44 4 60	00	., [10.0	15.00	17.00	10.0	
$\begin{vmatrix} 1\\2 \end{vmatrix}$	7 8	28.8			1	1	0 35.		- 1		18 36 12.08 46 6.80		.21	1. 2 41.61 VII. 7 37.32	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	26. 23.	1		15.29		40.8	
3	6						520.				56 50.94	i i	$.15 \\ .23$	II. 1 34.81	53 55.37	23. 21.			54.17		26.8	
4	8.9						43.		1		58 14.39		.15	10. 7 32.60	14 4.11	21.			17.54	1	35.2	
						COR	RECT	rion	s.						INSTRU	MENT	REAL	OINGS				
***********											1		-			CIR					THEF	
			COR		ноп		m.		n.	c.	ZENITH POINT.	COINC.					JUE.	1	<u> </u>	BAR.	THEF	-mom.
															Α.	в.	c.	ъ.	Mean.		At.	Ex.
June 2	21, at 1	6h	+50	.731	+ 0	.008	$^{s.}_{+0.1}$	98 +	s. 0.396	+0.247	0° 0′ 0″.93	r. 40,105	Zo X	one. h. XIX.—June 21, 18. 20.	6 280 51 23.0	22.0 20.0	26.5 28.0	26.0 27.2	24 ["] .38 24.27	1. 29.980 29.976	63°.8 54.5	56°.3
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er.	tude.		SEC	CONI	DS C	F T	'RAN	SIT	s.		т				D.	1	9		Right	1	n So clinati	
Number.	Magnitude.	ı.	и.	ш.	ıv.	v.	vi.	vII.	10.	11.	Т.	a	•	MICROMETER.	D.	d.	e management in the company	1850	ension, 0.0.	}	60.0.	оп,
		,		Zor	ne X	XIX		June	21.	М	. D.=-3	å 49 [′] 10)́0.	n'. == -30 ["] .01.	n."=-15		(Co	ontinu	ed.)			
5 6 7 8 9 10 11 12 13	9.10 9 8 7 8.9 9 8.9	36.5 4.5 52.8	19.0 7.5 31.6	33.2 21.4 30.5	47.0 35.9 44.8 0.8	25.2 34.5 50.0 59.0 14.5 57.0	56.0 16.6 4.7 13.4 10.5 17.0	54.8 31.0 19.0 28.1 			h. m. s. 19 4 26.90 9 11.28 16 19.97 23 47.53 40 35.87 56 44.71 20 4 0.29 6 42.24 20 8 48.24	+63 63 63 63 63 63 63		r. I. 2 36.87 " 5 37.28 VII.3 44.32 IV. 4 37.58 " 5 38.40 I. 5 36.17 10. 5 46.51 11. 1 42.84 VII.5 49.14	-46 50".10 26 0.21 33 43.19 31 38.95 25 21.63 26 38.74 20 39.12 49 15.55 19 8.31	$\frac{6}{6}$.	.61 .01 .34	19 5 10 17 24 41 57 20 5	n. s. i 30.11 i 14.45 i 23.15 i 50.69 i 38.99 i 47.79 i 3.34 i 45.34 i 51.27	41 15 41 23 41 21 41 14 41 15 41 9 41 38	5 19.7 5 28.8 8 10.2 4.2 4 43.2 5 56.9 5 55.7 8 31.6 8 23.9	2 0 9 7 0 4 0
						Zoi	ne XX	XX.	J	une 2	2. H. I	0.=-	28° 2	6 30.0. n.=	—15 ["] .77. r	·.=-	-6.00.					
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 1	8.9 8.9 7 9 9 8 7.8 7.8 9 9 9 9 9 6.7	34.0 20.0 17.0 22.0 24.8 57.5 8.0 17.2 	46.5 33.0 30.0 34.5 37.4 10.5 20.5 30.0 57.2 9.0 5.5 41.0 26.0 26.0	4.2 59.0 45.0 47.2 50.0 23.0 33.1 43.0 9.5 21.2 8.0 53.2 38.5	16.5 11.2 58.0 55.0 2.0 35.8 45.2 55.0 222.0 34.0 31.0 6.2 6.0 51.0	29.3 24.0 14.8 48.0 58.0 7.5 16.0 33.1 18.8 0 3.5 Zon 7.8	24.7 27.0 0.2 10.5 28.3 6.0 47.2	54.5 49.0 33.0 39.8 12.8 41.0 18.2 43.8 43.2 28.6		34.0	17 1 24.70 5 16.80 7 11.45 8 57.90 9 55.08 9 59.74 13 2.30 14 35.43 16 45.50 17 55.13 18 3.37 18 40.72 20 22.07 21 33.87 22 30.78 23 20.75 24 6.18 26 5.80 27 29.90 17 29 51.05	61 61 61 61 61 61 61 61 61 61 61 61 61 6	.88 .86 .84 .88 .89 .90 .88 .85 .84 .87 .88 .86 .89 .90 .91 .89 .90 .88	V. 1 40.120 IV. 3 43.010 V. 5 38.992 III. 2 46.470 I. 2 38.790 VI. 2 31.812 IV. 3 34.678 " 5 46.682 " 6 47.515 " 4 42.130 V. 3 45.240 VI. 5 40.711 IV. 4 42.505 " 6 38.875 " 4 33.870 " 3 33.149 V. 2 44.686 IV. 4 45.652 " 3 43.220 " 5 41.590 IV. 1 44.662 " 4 39.165 " 4 39.165 " 4 41.250	50 35.52 34 18.61 24 53.53 41 4.49 45 29.49 49 30.84 39 6.45 20 27.85 10 36.50 28 52.42 33 1.55 23 54.06 28 39.48 16 15.02 33 37.79 39 59.32 42 6.07 26 50.70 34 11.37 23 23.78 -15.17. n	9. 8.	44 02 63 43 41 74 40 92 66 63 49 13 85 64 45 22 88 45 6.00.	6 6 8 8 9 9 10 11 11 14 15 15 18 19 19 19 19 19 19 19 19 19 19 19 19 19	2 26.58 3 18.66 3 13.29 5 59.78 5 56.97 1.64 4.18 5 37.28 7 47.34 8 57.00 5 .25 9 42.59 9 23.95 9 23.95 9 33.95 9 31.80 9 52.93 2 29.13 6 57.10 8 55.84	29 1 28 51 29 7 29 12 29 16 29 5 28 47 28 55 28 59 28 50 29 6 29 8 29 8 28 50 29 5	20.8 3.0 37.5 48.1 212.9 314.2 49.1 10.2 18.4 34.0 35.5 30.5 30.5 30.5 30.5 30.0 30.0 30	5 5 2 z. 2 z. 25 5 9 5 z. 28 z. 88 z. 85 z. 11 77 z. 3 z. 77 z. 4 z. 99 7
						COR	RECT	ons.							INSTRU	MENT	REAI	oings				
			cor.		нопн		m.	9	ı.	c.	ZENITH	COINC.				CIRC	LE.			BAR.	THER	мом.
				CK.	C01	а.					POINT.				A.	В.	с.	D.	Mean.		At.	Ex.
June	22, at 1	6h	+50	.529	+ 0.	004	s. +0.198	+0.	396	*. +0.247	359 59 57.75	40.097	Zo: XX	ne. IX.—June 22, 17.0	. 292° 12′ 8.′6 8.2	10.2 9.5	17.'' ₄ 17.1		13 ^{''} 05 12.50	1. 30.120 30.114	63.8 63.8	56.4 56.0
a	was sort to stand for		on the state of th				owa w orange of a cold															

Number.	Magnitude.	I.	SECOI	NDS OF	1 1	SITS.	11.	Т.	a.		MICROMETER.	D.	d.	N		Right ension,	De	n Sc clinat 50.0.	
			$\mathbf{Z}_{ ext{on}}$	e XXXI.	Jun	ıe 24.	н.	D.=-25°	56 50̈́.0	•	n'.=-15.17.	n'.=- 6'.06	0.	(Conti	nued.)			
4 5 6 7 8 9 10 11 12 13 14 15 16 17	8.9 8.9 7.8 8.9 9 9 9 9 7.8	0.8 35.6 31.3 13.0 58.5	12.8 25.6 48.2 0.8 34.5 46.6 	0 40.0 52 5 37.4 49 5 12.5 24 5 59.0 11 2.0 14 10.6 22 0 8.0 23 5 26.2 38 2 35.0 47 2 35.2 47	5 1.6 1 6 36.8 4 0 23.2 4 1 26.2 3 6 35.0 4 0 32.6 4 2 51.0 15.0 2 4.2 0 59.5 1 1 23.7 3 1	4.2		h. m. s. 15 9 40.06 10 37.44 12 12.57 12 58.86 14 1.92 15 10.55 18 8.18 19 26.49 24 50.36 27 39.68 36 35.07 41 59.37 42 35.69 15 45 35.28	61 61 61 61 61 61 61 61 61 61 61	.29 .32 .32 .31 .35 .31 .36 .37 .34 .36 .37	IV. 6 40.705 " 4 37.668 " 4 39.160 " 6 36.360 " 1 43.155 " 6 39.262 " 1 39.762 " 7 43.255 " 2 45.390 " 7 39.536 " 6 37.460 V. 7 44.791 VII. 2 46.341 «IV. 5 45.890	-15 12".10 31 26.51 30 35.02 17 42.21 48 50.26 16 1.98 50 47.43 7 53.09 41 41.56 10 1.47 17 4.21 6 59.98 41 8.37 20 55.43	8. 8.	52 28 16 00 82 37 17 32 87 40 48 38	11 13 14 15 16 19 20 25 28 37 43	3. s. 41.35 38.76 13.89 0.17 3.27 11.86 9.54 27.80 51.73 41.02 36.43 0.74 37.11 36.67	26 28 26 27 26 14 26 45 26 13 26 47 26 4 26 38 26 7 26 14	38 30.0 38.3 45.3 553.2 553.2 65	03 80 87 26 80 80 80 26 88 34 61
			1	Zone	XXXI	І. Ј	une 24.	. н. <i>L</i>). <u>=</u> -2	28 2	6 10.0. n'.=-	-40.00. n	.= -	-3.16.					
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	7 9 8 9 9 9 9 9 8.9 9 6.7 9 9 9 9 7.8	27.0 2.2 30.0 31.5 41.2 29.0 59.2 37.0 7.0 44.0	34.9 46.0 39.8 52.5 15.0 27.5 	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{bmatrix} & & & & & & & & & & & & & & & & & & &$	6.0 2.5 7.5 0.8 12.5 12.5 2.0 2.0 1.0 1.0	225.0 533.2 	17 30 1.15 31 58.55 36 4.88 37 39.84 38 52.97 40 6.49 41 20.98 43 7.33 43 9.02 16.23 46 18.70 48 6.27 48 24.33 50 37.25 53 14.45 55 15.07 56 14.13 56 21.40 58 19.24 59 43.47 18 1 24.50 3 13.71	61 61 61 61 61 61 61 61 61 61 61 61 61 6	.78 .77 .84 .84 .87 .80 .81 .78 .80 .81 .86 .80 .86 .84 .81 .86 .83 .83	IV. 5 41.810 " 6 44.185 " 1 36.210 " 6 40.380 " 1 43.276 " 2 36.370 " 7 43.498 I. 5 44.098 IV. 3 47.850 " 6 46.050 II. 7 39.328 IV. 6 36.752 VII. 5 37.031 IV. 1 36.131 " 6 37.290 " 1 41.105 " 3 40.282 VI. 3 36.211 " 6 33.250 " 2 35.530 " 4 42.020 II. 5 38.922	23 13 36 13 8.76 52 47.77 15 20:23 48 43.62 46 50.60 7 41.43 21 53.98 31 28.52 12 4.34 10 5.37 17 25.54 25 58.14 52 50.49 17 6.98 49 58.62 35 48.04 38 10.56 19 26.45 47 19.46 28 53.27 24 53.05	37. 36. 36. 35. 35. 35. 34. 34. 33. 32. 32. 32. 31. 31. 30.	36 52 19 94 69 43 06 05	33 37 38 39 41 42 44 44 47 49 49 51 54 56 57 57 59 18 0	2.93 0.32 6.72 41.62 54.81 8.33 22.75 9.13 10.83 18.01 20.48 8.07 26.14 39.11 16.25 16.93 15.97 23.24 21.05 45.33 26.33 15.53	29 19 28 42 29 13 28 34 28 48 28 58 28 46 28 44 28 52 29 19 28 43 29 14 28 55	9 56.1 9 34.5 9 34.5 9 6.4 9 2 6.4 9 3 36.5 9 3 36.5 9 3 39.0 9 49.7 9 49.7	12 29 442 56 66 69 77 77 77 77 77 76 61 61 61 63 63 63 63 63 63 63 63 63 63
			,	COL	RECTIO	ons.						INSTRU		READ	INGS.			тнеі	RMOM.
			COR. TO	HOURLY COR.	m.	n.	c.	ZENITH POINT.	COINC.			Α.	В.	c.	D.	Mean.	BAR.	At.	Ex.
June	24, at 1	13h	s. +50,453	*. + 0.002	s. +0.198	s. +0.396	s. +0.247	o° o′ o″.12	r. 40,093	Zon XX	te h. XI.—June 2414.9 15.3 15.8	294°41′57″.9 56.9	58.7 58.1		655 64.6		1. 30.138 30.134 30.128	70.0	67.0

Number.	Magnitude.	SECONDS OF		Т.	a.	MICROMETER.	D.	d.	Mean Right Ascension, 1850.0.	I	Sout ination	- 1
		Zone XXXII.	June 24. H.	D. =-28 [°] 2	26 10.0.	n'.=40.00.	n'.=- 3'.1	6. (Co	ontinued.)			
23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 **50	9 9 9 7 9 8 9 9 8 8 9 9 9 9 8 8 9 9 9 9	$\begin{array}{c} . \ . \ . \ . \ . \ . \ . \ . \ . \ . $	0 6.4 19.0	h. m. s. 18 6 0.00 4 41.55 5 46.75 6 51.74 8 50.10 9 51.24 10 25.91 13 37.72 17 55.73 19 58.84 21 21.28 23 40.06 26 32.45 28 43.75 30 46.39 32 49.59 33 56.50 35 4.53 46 5.70 49 33.65 52 2.75 55 16.09 57 2.14 19 6 20.94 8 58.37 12 28.32 18 26.48 19 25 38.66	\$. +61.83 61.86 61.85 61.86 61.84 61.88 61.88 61.88 61.88 61.88 61.88 61.88 61.88 61.88 61.88 61.88 61.88 61.88 61.88 61.88	VI. 7 35.360 V. 4 37.116 IV. 5 40.690 " 3 39.270 " 3 31.817 VI. 6 33.445 IV. 2 43.250 V. 5 38.250 IV. 5 36.835 " 7 39.750 " 1 39.695 " 7 37.992 IV. 7 36.480 " 4 38.528 " 7 41.650 V. 3 36.210 IV. 4 42.008 VII. 2 48.078 IV. 4 44.400 " 5 39.740 " 1 38.320 " 5 38.310 " 4 41.770 " 1 39.505 " 1 33.778 " 1 41.430	-25 45.31 12 22.47 31 42.78 23 52.05 36 24.98 40 42.45 19 19.72 42 52.89 25 16.35 26 5.24 9 50.87 50 47.31 10 51.62 11 43.89 30 53.97 8 45.23 38 10.65 28 53.78 40 6.70 27 31.17 24 24.89 51 34.81 25 14.34 29 2.00 50 53.81 54 11.64 49 47.37 34 15.31	-30.69 30.55 30.32 30.08 29.67 29.46 29.33 28.65 27.73 27.29 27.01 26.51 25.90 24.56 24.32 24.08 21.72 20.98 20.46 19.77 19.40 17.44 16.88 16.16 14.91 13.43	h. m. s. 18 7 1.83 5 43.35 6 48.59 7 53.57 9 51.95 10 53.10 11 27.73 14 39.58 18 57.57 21 0.68 22 23.09 24 41.94 27 34.27 29 45.57 31 48.24 33 51.40 34 58.37 36 6.38 47 7.57 50 35.50 53 4.60 56 17.98 58 3.99 19 7 22.79 10 0.26 13 30.21 19 28.37 19 26 40.52	28 52 28 39 28 58 28 50 29 3 29 7 28 45 29 9 28 51 28 36 29 17 28 38 28 38 28 35 29 4 28 55 29 6 28 54 28 50 29 18 28 51 28 52 29 19 9 10 20 20 16 20 0	3.02 23.10 32.13 4.65 21.91 59.05 31.54 54.08 42.53 27.88 23.82 27.52 19.32 28.97 19.79 44.97 27.86 38.42 2.15 55.35 4.58 43.74 29.44 20.69 37.80 12.28	z. z. z. z.
	1	Z	one XXXIII. July	1. H. I	O. == -25°	56 30.0. n.=	=-25.00. r	″. = −3″.7	0.			
1 2 3 4 5 6 7 8 9 10	8.9 9 8 7.8 9 9 9 9	11.2 23.2 35.2 47 27 32.2 9 53.1 5.5 17.6 30.0 56.5 9.3 21 38.0 49 	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	32 56.60 36 29.91 37 9.07 37 37.50 38 32.76 40 51.18 42 21.59	66.5 66.5 66.5 66.5 66.5 66.5 66.5	3 V. 2 41.650 1 IV. 5 46.530 2 III. 6 36.130 5 IV. 3 32.722 4 VI. 4 33.922 6 ' 2 36.600 8 IV. 5 42.515 6 '' 2 44.892	23 41.01 43 48.38 20 31.02 17 47.82 40 11.50 33 33.52 46 42.72 22 49.69 41 56.44 41 17.49	23.29 23.17 22.48 21.82 21.69 21.61 21.43 21.00 20.70 20.68	15 29 41.86 30 21.85 34 3.11 37 36.43 38 15.62 38 44.04 39 39.32 41 57.71 43 28.15 15 43 37.28	26 40 26 17 26 14 26 37 26 30 26 43 26 19 26 38	41.55 23.50 39.64 3.19 25.13 34.15 40.69 47.14	z. z.
							INSTR	UMENT RI		1		
					No. of the latest section of the latest sect		Α.	B. C	D. Mean.	BAR.	At.	Ex.
					X		h. 17.4 292 12 2.2 18.2	.		30.104 30.100 30.100 30.086	68.0 67.5	65°.5 65.0 64.5 63.7

Der.	Magnitude.		SECO	OND	os of	TRA	NSI'	rs.		Т.	a.		MICROMETER.	D.	d.		Right ension,		an Sc clinat	
ramper.	Magi	ı.	11. 11	ı. I	v. v	. VI.	VII.	10.	11.	* •			miono mai anti-	D.	u.	185	,	1	50.0.	
			2	Zone	XXX	KIII.	$\mathbf{J}\mathrm{u}$	ly 1	. н	. D.=-	-25° 56′ 5	30 ^{′′} .0.	n'. == -2500	. n'=-3		Continu	ied.)			
11 8	3.9		56.0 8	.020),432.	.8 45.0				h. m. s. 15 44 20.47	7 +66	s. .57	r. IV. 2 45.132	-41 ['] 48 ^{''} .16	20'.32		m. s. 5 27.04	26 38	38 ^{''} .4	48
- 1	.8		6.0 17		i	1	i	1		45 30.02		.54	III. 5 45.550	21 4.82	20.09		6 36.56	1	7 54.9	
3 9						. 12.2			• •	45 47.89	i i	.54	IV. 5 42.708	34 12.71	20.04		6 54.43	1	1 2.7	
$\begin{array}{c c} 4 & 9 \\ 5 & 8 \end{array}$			$\begin{array}{c c} \cdot \cdot & \cdot \\ 35.447 \end{array}$. 0.2		1		$46 \ 35.64$ $48 \ 59.82$		$.54 \\ .54$	" 5 40.782 " 6 46.040	$ \begin{array}{c cccc} 23 & 49.56 \\ \hline 12 & 5.65 \end{array} $	$19.88 \\ 19.41$		$742.18 \\ 06.36$) 39.4 3 55.0	
6 8		~0.~	1			0.038.2	1	5		49 13.67	1	.58	" 3 36.280	38 8.69	19.36		0.30 0.25		1 58.0	
7 9) :		26.038				i	i		50 50.48	1	. 59	II. 2 32.530	49 3.30	19.06		1 57.07		5 52.3	
3 9	- 1		45			1			• •	$51\ 57.20$.55	I. 6 40.720	15 9.00	18.83		2 - 3.75	1	57.8	
$\frac{9}{3}$	i		$\frac{38.2}{22.0}$.		1	1	l		• •	53 2.50		.55	IV. 5 46.592	20 28.88	18.61		4 9.05		7 17.4	
	3.9	9.2	22.0 34		1			٠.		54 46.39		.58	" 3 41.540	35 7.01	18.26		5 53.97		55.2	
$\begin{bmatrix} 1 & 9 \\ 2 & 8 \end{bmatrix}$	- 1	• •	1	- 1	- 1	. 18.0	1		• •	54 53.53		.59	" 3 33.702	39 37.71	18.23		6 0.12		25.9	
$egin{array}{c c} 8 & 8 \\ 8 & 9 \end{array}$.9	• •	$\begin{array}{c c} \cdot \cdot \cdot \\ 32.144 \end{array}$	4.56		38.8			4.4	55 14.22 56 56.69		.59 .60	" 3 40.270 " 2 40.205	35 50.86 44 38.36	$18.16 \\ 17.82$		$\begin{array}{ccc} 6 & 20.81 \\ 8 & 3.29 \end{array}$		2 39.0 1 26.1	
7	ì		35.348						1.7	16 0 0.07		.60	" 3 43.972	33 43.00	17.02 17.20		$\frac{3.23}{1.6.67}$		30.2	
- 1		39.5	52.0 .	. 17	7.0 .		53.5			1 16.69	i	. 62	I. 1 43.590	48 32.64	16.94		2 23.31		5 19.5	
6 9			55.0 .						• •	1 19.31		.61	IV. 2 40.820	44 17.08	16.92		225.92	1	4.0	
			37.0 49	- 1	- 1	1	l i		• •	5 1.53		. 63	" 1 36.605	52 34.20	16.14		8.16		20.3	
$\frac{8}{9} \frac{8}{9}$	- 1		$ \begin{array}{c c} 46.0 & 58 \\ 58.0 & . \end{array} $	i	1	1	59 O	• •		14 10.78 14 22.39	1	. 65 . 62	I. 1 39.180 VII.4 39.220	$\begin{bmatrix} 51 & 4.94 \\ 30 & 30.31 \end{bmatrix}$	$14.19 \\ 14.17$		5 17.43 5 29.01		7 4 9.1 7 1 4.4	
9	- 1		20							15 32.91	1	.60	IV. 6 38.442	16 28.03	13.90		39.51	1	3 11.9	
. 9		30.0	42.5 .		. 19.	.0				18 6.82	66	. 59	" 7 36.960	11 28.25	13.35	19	3.41		3 11.6	
2 1	- 1		42.054							19 6.30		.60	" 7 41.290	8 58.75	13.13		0.13.41 $0.12.90$		5 41.8	
8 8	5	27.5	40.0 52	.0 4	.2 16.	128.8	40.6			21 4.21	. 66	.61	" 6 39.788	15 41.53	12.71		2 10.82		24.5	
- 1	- 1	ì	59.3 11						• •	24 24.05	1	. 67	" 1 39.640	50 49.37	11.97		5 30.72	1	31.3	
$\begin{bmatrix} 5 & 9 \\ 5 & 9 \end{bmatrix}$		1	$\begin{bmatrix} \cdot & \cdot & \cdot \\ 50.0 & 2 \end{bmatrix}$			5 25.0 4 38 6				24 56.17 28 14.43	i i	.62 .66	V. 6 44.496 IV. 2 40.731	12 58.95 44 20.14	11.85		$\begin{array}{ccc} & 2.79 \\ 9 & 21.09 \end{array}$	1	40.8	
7 9			$28.0 _{39}$							29 51.88		. 63	" 6 45.390	12 28.11	$11.12 \\ 10.75$) 58.51		8.8	
3 9			49.0 1							32 13.75		.69	IV. 1 37.760	51 54.31	10.22		3 20.44	3	34.5	
9			3.0 .							$32\ 27.20$	1	. 69	" 1 37.640	51 58.45	10.18	33	33.89	1.	38.6	
7	.8	52.8	17	.5 30	0.0 42.	054.0	6.3	٠.		33 29.72	66	.66	. 3 42.946	34 18.43	9.94	3	4 36.38	26 30	58.3	37
1 8			2.5 15							35 27.01	1	.65	" 5 3 8.140	25 20.82	9.50		33.66			
$\begin{vmatrix} 9 \\ 8 \end{vmatrix}$			45.858						• •	37 10.00		.68	" 2 47.247	40 35.12	9.11		3 16.68	1		
9			$23.836 \\ 5.217$							39 48.23 40 29.36		.67 .66	II. 4 36.880 IV. 5 38.905	31 51.34 24 54.39	$8.51 \\ 8.36$) 54.90 1 36.02		3 29.8	
9	- 1		3.5 15		- 1	1 1				41 28.00		.69	II. 3 32.850	40 6.98	8.13		2 34.69		32.1 45.1	
9				. 49	.5 2.	0 14.2				41 49.66		. 69	IV. 2 43.140	42 56.98	8.05		2 56.35	26 39	35.0)3
9		• •							40.0	42 32.69	1	.67	VII. 4 34.920	32 58.80	7.88		39.36		36.6	
$\begin{array}{c c} 3 & 9 \\ 0 & 9 \end{array}$		· · · · · · · · · · · · · · · · · · ·			1 '	$\begin{array}{c}253.0\\057.8\end{array}$				44 28.25 46 33.58			IV. 3 44.230 " 2 37.970	33 34.09 45 55.52	$\begin{bmatrix} 7.43 \\ 6.96 \end{bmatrix}$		5 34.93 7 40.28		0.11.5 $0.32.4$	
9			1	- 1	.0	1 1				16 48 5.62	1	65	" 7 38.622	10 30.84	6.60		12.26		3 32.4 1 7.4	
-				-	COI	RRECT	IONS	•						INSTRU	MENT RE	DINGS	\.			
															CIRCLE.				THEI	RM (
			CLOCK.	- 1	OURLY COR.	m.	n	ı.	c.	ZENITH POINT.	COINC.			Α.	В. С.	D.	Mean.	BAR.	At.	
			s.	-	s.	s.	8.		s,	0 / "	r.	Z	one h .					т.		-
7 1, at	t 13h.	••••	+55.312	+		+0.213	+0.	298	+0.330	0° 0′ 0′.65	40.101	XX	XIII.—July 1, 15.4 16.5	294 42 2.2	10.2 14.0			29.846	77°.0 . س	7
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er	itude.		SE	CON	DS (OF '	TRAN	SITS.		#				-	•	9	Right	1	n So	
Number	Magnitude.	ı.	п.	ш.	IV.	v.	vi.	vII. 10.	11.	Т.	a.		MICROMETER.	D.	d.	Asc 1850	ension,).0.		clinati 0.0.	.on,
		-			Zoi	ne X	XXIV	7. Ju	ıly 7.	Н. Д.:	=-4i̊	5 1	10.0. n.=-1	5.00. ". =	=19.91.					
1 2	9 8.9	5.2	20.0	35.0	49.3	4.0	19.0			h. m. s. 15 40 43.53 44 49.52	+72. 72.	16 18	II. 6 35.962	18 3.78	$-11\overset{''}{.}44$ 10.72	15 41 46	s. s. 55.69	42 9		60
3 4 5	9 9 8.9 9	$\frac{31.2}{54.8}$	$\substack{46.0\\9.2}$	$0.8 \\ 24.5$	16.03	30.2 • •	$\frac{45.2}{9.2}$			44 52.83 46 15.67 50 39.25	72. 72. 72.	19 22	V. 7 34.350 IV. 6 33.970 III. 5 39.750	13 6.38 19 13.23 24 38.51	10.71 10.46 9.68	47 51	5.01 27.86 51.47	42 4 42 10 42 15	$\frac{33.6}{58.1}$	59 9 м.
6 7 8 †9	7.8 9 7	2.2	17.1 	32.0	46.4	2.0	59.5 1	$egin{array}{cccccccccccccccccccccccccccccccccccc$		51 15.34 16 3 46.77 4 29.64 16 7 39.75	72. 72. 72. 72.	32 34	IV. 6 43.910 " 3 34.310 VI. 1 36.180 IV. 5 36.070	13 27.20 39 37.65 53 16.75 26 46.81	9.57 7.22 7.08 6.48	16 4 5	27.55 59.09 41.98 52.06	42 4 42 30 42 44 42 18	$\frac{54.8}{33.8}$	87 в. 83
				and a many			ıe XX		July 7	•		ATT ATT	55′ 40″.0. n′.=		n''=-5.6					
1 2	9	3.0	15.2				$9.2 \\ 4.01$	6.1		19 59 44.84 20 2 39.57	71.		IV. 5 43.200 " 2 44.688	22 28.00 42 5.42	19.83 19.19		56.05 50.81	26 18 26 38		
3 4 5	8.9	48.8 47.6	2.1	$14.2 \\ 11.9$	$\frac{26.2}{24.0}$	38.2 36.3	51.0	$\begin{bmatrix} 3.3 \\ 0.9 \end{bmatrix}$		10 26.30 14 24.22 17 50.04	71. 71. 71.	22 19	" 3 37.287 " 5 42.621 " 7 39.670	37 35.84 22 48.02 9 56.52	17.47 16.59 15.84	11 15	37.52 35.41 1.27	26 33 26 18 26 5	$\frac{33.3}{44.6}$	31 31 z.
$\begin{bmatrix} 6 \\ 7 \\ 8 \end{bmatrix}$	10 9 7	$\frac{5.8}{58.7}$	18.2 51.0	30.8 3.2	15.0	$\frac{1}{27.8}$	$\begin{array}{c} 7.01 \\ 40.05 \end{array}$			23 22.13 25 42.65 31 15.46	71. 71. 71.	15	" 5 40.380 " 6 44.180 " 3 40.455	24 5.41 13 11.76 35 46.44	14.64 14.14 12.96	26	33.30 53.80 26.64	26 20 26 9 26 31	5.9	0
9 10 11		35.3	48.0		12.2		8.12 37.04 36.04	9.0		33 43.84 36 12.33 39 11.51	71. 71. 71.	19	" 5 37.366 " 2 35.672 " 5 40.486	25 49.51 47 15.82 24 1.76	12.43 11.91 11.28	37	54.99 23.52 22.65	26 21 26 43 26 19	7.7	3
12 13 14 15	8.9	30.0 43.1 38.0	$42.2 \\ 56.0 \\ \cdot \cdot$	$54.3 \\ 8.0 \\ 3.5$		18.8 41.3	31.1 4 5	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		41 6.69 44 19.77 45 15.56 48 40.62	71. 71. 71. 71.	12 11 16	" 6 45.400 " 6 45.390 " 2 39.780 " 3 34.595	12 29.65 12 29.99 44 54.95 39 8.77	10.89 10.23 10.04 9.35	42 45 46	17.81 30.88 26.72 51.77	26 8 26 8 26 40 26 34	20.5 20.2 44.9	64 z. 12 19 z.
16 17	8.9		29.4	41.4	54.0	5.8	18.03	$\begin{bmatrix} 0.2 \\ 3.0 \\ \vdots \end{bmatrix}$		56 53.71 20 59 56.14	71.	09	" 6 43.155 " 1 40.998	13 47.16 50 4.41	7.72 7.12	58	4.80 7.28	26 9 26 45	34.8	88
					Z	ione	XXX	VI.	July 9.	H. L	•.=-4	å 2	′ı́ 10̈́.0. ṅ.=-	–26.85. n.	=-16.0	00.				
1 2 3 4	8 9 9	$45.0 \\ 47.5$	$\frac{0.5}{3.0}$	$15.0 \\ 17.2$	30.4	$\frac{45.0}{47.0}$	$\begin{bmatrix} \dots \\ 2.2 \end{bmatrix}$	2.0		16 3 47.01 4 30.13 10 32.42 19 54.81	72. 72. · 72. 72.	05 09	IV. 7 40.560 " 5 42.371 " 4 42.595 " 4 37.475	9 25.01 23 3.20 28 45.40 31 44.21	25.86 25.71 24.45 22.45	5 11	59.04 42.18 44.51 6.95	42 31 42 44 42 50 42 53	$\frac{38.9}{19.8}$	1 85
5 6	9 7.8	22.0	36.4 		7.2		7.82	2.8		24 6.95 16 24 38.01	72. 72.		" 4 36.555 V. 7 37.452	32 15.94 11 13.55	21.53 21.41		19.10 50.13	42 53 42 32		
					1	COR	RECTI	ons.						INSTRU	MENT RE	ADINGS	•			
			COR		HOUR	1	m.	n.	c.	ZENITH POINT.	coinc.			A.	B. C	D.	Mean.	BAR.	THER	Ex.
July 7	7, at 12	2h	+59	.985	s. 0.0	022	s. +0,213	s. +0.298	s. +0.330	0° 0′ 1″.70	r. 40.110	Z_0	one XXIV.—July 7, 15.6	. 278°51′ 1″.8	0.1 3.	3 57.0	0.55	1. 29.956	79°.0	73°.7
				† 1	Moon	too bi	right for	observat	ion.			XX	16.2 19.8 XXV.—July 7, 20.0 21.0	294 41 58.9	59.0 60.	3 55.7	58.48	29.962 29.960 29.962	77.6 74.0 72.3	72.7 68.8 68.3

ber.	Magnitude.		SI	ECOI	ND	s o	FΊ	ΓRA	NSIT	rs.		т.				D,	a	H	Right		ın So	
Number.	Magr	ı.	11.	ш.	1	v.	v.	vi.	vII.	10.	11.		a	•	MICROMETER.	D,	d.	B	ension, 0.0.		clinat 50.0.	ion,
				Zo	ne	XX	XV	7I.	Jul	у 9.	Н	I. D.=-	42 21 1	ő.o.	n'. == -26.85	. ń.=-1	$6^{''}_{\cdot}00$.	(Contin	ued.)			
7	8	52.7	8.0	22.8	8 38	$8.0 _{5}$	3.0	8.0	23.2			h. m. s. 16 26 38.15		s. 2.19	r. IV.2 42.000	$-43^{'}\ 56^{''}.21$	-20.98	h. 16 2	m. s. 7 50.34	43° 5	ź 27″. I	19 в
8	9	21.3	36.6	51.0	0 6	$6.0 _{2}$	1.0	36.0	51.0			38 6.08	1	2.20	" 4 42.792	28 38.61	18.43		9 18.28	1	7.0	
9	8.9			326.5								$40\ 42.0$	4	2.20	" 5 43.516	22 22.99	17.85	4	1 54.21	42 43	3 50.8	34
10	7.8								37.0			41 52.09		2.21	" 5 37.002	26 10.18	17.58	R	3 4.30	1	7 37.7	
11 12	8.9								$27.8 \\ 47.2$			43 42.90 48 2.14		2.24 2.25	" 2 44.390 " 3 37.510	$\begin{array}{c} 42 \ 33.01 \\ 37 \ 42.75 \end{array}$	17.17 16.20	R .	455.14 914.39	1	1 0.1	
13	9								19.3			52 34.49	1	2.27	" 2 42.333	43 44.73	15.16	8	3 46.69		8.9 5 9.8	
14	9								35.2			55 50.70	1	.22	" 6 46.313	11 58.84	14.41	8	7 2.92			
15	5.6	27.7	42.5	58.0	0 15	$2.5 _{2}$	7.2	42.8	58.0			17 0 12.70	72	.29	" 2 47.430	40 47.02	13.41	2	1 24.99	1	2 10.4	
16	9			56.0	0 .	$\cdot \cdot _2$	5.5	• •	• •			6 10.89	72	2.26	III. 5 43.690	$22\ 16.96$	12.18		723.15	42 43	39.1	4
17	9			36.0	0 .		5.5	21.0	35.5			6 50.90	72	.27	IV. 5 44.100	22 - 2.86	12.04		8 3.17	42 43	3 24.9	0
18	9										44.0	6 21.60		.27	VII.4 44.781	27 29.00	12.15		7 33.93		51.1	
19	8.9								19.0		$ \cdot\cdot $	18 34.20		.33	IV. 2 40.680	44 42.12	9.61	Я	9 46.53			
20 21	9 5			42.0							• •	22 56.89		2.31	" 4 45.530	27 3.07	8.69	8	4 9.20	i		
21 22	8.9	35.5							55.5	• •	• • •	25 20.40 26 10.99		3.32	" 4 36.180 " 5 38.150	32 29.25	8.19		6 32.72			
23	9	20.0							25.0			26 40.25	i i	29	" 6 37.806	$\begin{array}{c} 25 \ 30.23 \\ 16 \ 55.01 \end{array}$	$8.02 \\ 7.91$		723.23 752.54	1	$648.2 \\ 12.9$	
24	9					- 1					25.8	27 3.06		.34	VI. 3 31.290	41 19.41	7.83		8 15.40			
25	9			25.0								30 40.13		.33	IV. 3 40.301	36 5.35	7.07	8	1 52.46	1		
26	8				4	$4.5 _{5}$	9.3	13.8	28.7			$32\ 44.23$	3 72	.30	V. 6 35.879	18 2.15	6.63	3.	3 56.53	42 39	18.7	8 1
27	9	55.8		25.5	5.	5	5.2					40 40.61	1 72	.33	IV. 4 40.362	30 3.51	4.95	4	1 52.94	42 51	18.4	-6
28	9				5	$7.0 _{1}$	$^{2.2}$					42 56.9		.36	V. 2 38.568	45 55.73	4.46		49.27	1		
29	8.9			12.2	2 2	7.0 4	1.4	57.0				$50\ 26.93$	3 72	.34	IV. 4 36.364	32 22.90	2.87	A	1 39.27		35.7	
30	8.9					- 1	- 1		40.2			56 55.58		2.32	" 6 34.165	$19 \ \ 2.00$	1.47	2	8 7.87	1	13.4	
31	9		1	5	1	- 1		• •		• •		59 46.5		2.36	II. 2 39.818	45 12.11	0.85	8	0 58.93			
32	9	••	• •		•	1	• •	• •	30.0	• •	8.2	17 59 45.69	9 72	2.32	IV. 6 34.694	18 43.40	0.85		0 58.01	42 39	54.2	!5
						\mathbf{Z}	one	XX	XVII		July	9. H.	D.=-	-27° 5	26 10".0. n'.=	=-2500.	n'.=-3	₂₄ .				
1	9	23.0	35.0	48.0	0 .	. 1	3.0					18 5 0.40	+70	.95	II. 2 47.152	-40 37.95	-23.40	18	6 11.35	28 7	11.3	5 z
2	9		1	16.5	5 29	9.04	1.7					5 29.14	1 70	.95	IV. 2 45.170	41 46.52	23.26	8	6 40.09			
3		• •										6 20.60	1	.91	" 6 34.290	18 50.81	23.03	a	7 31.51	27 45		
4	9	• •	٠.						35.0		• •	6 57.74	1	.93	" 4 43.296	28 9.39	22.86	p .	8 8.67			
$\frac{5}{6}$	9		19 9	54.0					13.5			$7 \ 36.35$ $9 \ 6.85$	1	.93	VII.4 38.990 IV. 7 44.650	30 37.79	22.69	i i	3 47.28	27 57		
7	8.9								54.2			10 17.19		.95	" 2 41.002	$\begin{bmatrix} 7 & 1.89 \\ 44 & 10.48 \end{bmatrix}$	22.28 21.96	8	0 17.74 1 28.14	1		
8	8.9								19.2			11 42.09		.96	" 1 43.235	48 44.94	21.58	H	252.98	Į.		
9	8.9			38.0	0 50	0.5		15.2				12 50.48	3 70	.89	" 7 43.398	7 45.17	21.27	8	4 1.37	1		
10	9			5								18 46.50		.95	II. 1 44.056	48 16.46	19.67	19	9 57.45	28 14	46.1	3
11	8.9	38.6	51.3	3.8	3 16	6.0 2	8.0	40.5	•••	• •	• •	18 20 15.90	5 70	.93	IV. 3 39.361	36 20.87	19.25	18 2	1 26.89	28 2	50.1	2 2
			ı		,	C	ORR	RECT	ions.							INSTRU	MENT RE	ADINGS				
				. то		OURL	Y	m.	n		c.	ZENITH	COINC.				CIRCL	Ξ.		BAR.	THER	MON
			0110	оск.		cor.	_		_			POINT.				Α.	в. с	D.	Mean.		At.	Ex
ıly 9	9, at 12	h	+59	.630	_	s. -0.00	04 4	s. -0.215	$\begin{vmatrix} s \\ +0.5 \end{vmatrix}$	298	$s. \\ +0.330$	o° 0′ 1″68	r. 40.106	Zo X V	ne h. XVI.—July 9, 16.	0 278° 21′ 2″.0	0'.0 4'.	0 1.0	1".75	ı. 30.002	81°.0	77
	-				<u> </u>				1, .,	-	,	1 2.30		AA	17.		2.5 5.	1	3.70	30.002	79.5	74
															18.		2.2 5.	- 1	3.77	30.012	78.5	74.
														XX	XVII.—July 9, 18.	1	4.0 4.	1	4.17	30,012	78.5	74
															19.	0 3.8	4.2 6.	5 5.0	4.92	30.020	74.1	77.
																	1 1		1	1		

<u> </u>	itude		SECO	NDS OF	TRAN	ISITS.		TT.			T.	1	Mean Righ	1	an So	
TAUMING!	Magnitude.	ı.	13. III	. IV. V	. vi.	vII. 10.	11.	Т.	a.	MICROMETER.	D.	d.	Ascension 1850.0.	.	clinati 50.0	ion
			\mathbf{Z}_0	ne XXX	VII.	July 9	. Н	D = -2	26 10 ['] .	0. n'.=-25.00	0. n″=-3		Continued.)			
12	9	14.5	26.639	051.5 3	.0 16.5	28.9		h. m. s. 18 22 51.48	s. +70.9	4 IV. 2 37.680	46 ['] 5 ^{''} .23	-18.55	h. m. s. 18 24 2.49	2 28 19	2 33.7	 18
	9			5 6.0 18	.0 31.0	13.0		24 5.89	70.9		44 44.08	18.21	25 16.83	1	1 12.2	
	9		51.0_{10}	$\begin{array}{c c} 0 & . & . & . \\ 0 & 22 & . & 0 & 34 \end{array}$		• • • •	1	$26 \ 15.58$ $26 \ 22.07$	70.9		34 3.76 24 20.88	$\frac{17.63}{17.60}$	27 26.50 $27 32.9$	j.	31.3 48.4	
i	9		10	1 1		 39.859.		27 2.61	70.9		39 52.75	17.60 17.41	21 52.5 28 13.5	}	620.1	
i	8.9		:	48	.0 0.3	13.0		28 35.56	70.9	5 V. 1 37.700	51 56.12	16.99	29 46.5		3 23.1	
	9	10.0	23.0 .		1 1		1	30 47.57	70.9		39 4.45	16.39	31 58.49	i	30.8	
- 1	9					 50.0 8.		30 46.12 31 12.97	70.9 70.8		33 56.81 8 14.70	$\frac{16.40}{16.28}$	$31\ 57.03$ $32\ 23.84$	1	$\frac{23.2}{40.9}$	
- 1	9						j i	32 18.99	70.8	8	20 43.85	15.98	33 29.8		79.8	
	9		45	2 10				33 57.82	70.9	3 IV. 2 39.950	44 46.84	15.52	35 8.75	5 28 1	12.3	86
		51.2	4.016	4 28.5 41	.0 54.0	5.3		$35\ 28.67$	70.8	7 " 7 34.880	12 39.38	15.11	36 39.54	1 27 39	4.4	9
	9			2 3.3 15				37 2.95	70.8		27 51.27	14.69	38 13.84	3	15.9	
- 1	9 8			$ \begin{array}{c c} 2 & 41.2 \\ 0 & 32.2 & 44 \end{array} $		$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1 1	$38 \ 41.06$ $42 \ 32.33$	70.8 70.8		26 52.63 29 33.45	$14.25 \\ 13.20$	39 51.95 43 43.25		$\frac{16.8}{56.6}$	
Į.	9			251.0 .			i 1	43 50.93	70.8		22 40.34	12.85	45 1.80	į.	3.1	
- 1	8.9	1	57.1 9.	4 22.0 34	.5 46.5	59.2		$44\ 21.93$	70.9		52 35.24	12.71	$45 \ 32.85$	Į.	8 57.9	
- 1	8.9	18.0		$055.5 \ . 525.037$		i	1 1	46 55.50	70.8	1	12 21.69	12.01	48 6.35		3 43.7	
1	9 9		0.512.					48 25.03 48 52.73	70.8 70.8	1	24 19.11 29 38.87	$11.62 \\ 11.49$	$49 \ 35.89$ $50 \ 3.61$	1	0.40.75 0.3	
	8.9					1.5		49 24.17	70.9		48 39.73	11.34	50 35.08		5 1.0	
1	9				1	$1.5 \cdot 1.5 $		50 8.50	70.8	1	24 23.70	11.14	50 35.00	1) 44.8	
- 1	9	1	1	8 13.0 25	1 i			$53\ 13.01$	70.8	7 " 4 41.100	29 25.25	10.31	54 23.88	8 27 58	45.5	6
- 1		1	58.211. $43.556.$	$0 \begin{vmatrix} 23.5 \\ 0 \end{vmatrix} 35 $	1 1	$\begin{vmatrix} 0.2 \\ 6.0 \\ . \end{aligned}$	1 1	56 23.23 18 58 8.48	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	1	$ \begin{array}{c cccc} 26 & 41.22 \\ 30 & 3.17 \end{array} $	$\begin{array}{c} 9.45 \\ 8.98 \end{array}$	57 34.09 18 59 19.35		$egin{array}{c} 0.67 \ 22.15 \end{array}$	
		1							1		<u> </u>		И			
				Zone	XXX	viii	Tuly	10 M	n	39° 49′ 90″ 0 n′ -	30 00	n" —1.	4 95			
1		ı	1 1	Zone	XXX	V 111.	July	10. M.	D.=-	39 49 20.0. n.:	==-30 ['] .00.	n".=-1	4.95.			
	8.9		38.0 52.	0			· 	16 52 6.83	71.9	8 2. 1 38.805	51 35.52	28.43	16 53 18.81		23.9	
	8.9			$\begin{bmatrix} 0 & . & . \\ 0 & 58.3 & . \end{bmatrix}$			AD ARCHITECT	16 52 6.83 56 58.39	71.9	8 2. 1 38.805 8 2. 1 43.26	51 35.52 49 0.92	28.43 27.77	16 53 18.81 58 10.37	7 40 38	48.6	9
	8.9 8.9		29.3 44.	0				16 52 6.83 56 58.39 58 6.52	71.9 71.9 71.9	8 2. 1 38.805 8 2. 1 43.26 1 II. 7 37.05	51 35.52 49 0.92 11 30.56	28.43 27.77 27.62	16 53 18.81	$\begin{bmatrix} 40 & 38 \\ 40 & 1 \end{bmatrix}$	48.69 18.18	9 8
	8.9		29.3 44.	0		9.4	AD ARCHITECT	16 52 6.83 56 58.39	71.9	8 2. 1 38.805 8 2. 1 43.26 1 II. 7 37.05 8 I. 3 42.89 3 II. 7 41.80	51 35.52 49 0.92 11 30.56 34 32.62 8 45.68	28.43 27.77	16 53 18.81 58 10.37 59 18.42 17 10 9.54 13 55.86	7 40 38 8 40 3 4 40 24 6 39 58	48.6	9 8 7
	8.9 8.9 8.9 8.9		29.3 44. 48.5 2.	0				16 52 6.83 56 58.39 58 6.52 17 8 57.56 12 43.93 14 17.27	71.9 71.9 71.9 71.9 71.9 72.0	8 2. 1 38.805 8 2. 1 43.26 1 II. 7 37.05 8 I. 3 42.89 3 II. 7 41.80 1 2. 2 36.08	51 35.52 49 0.92 11 30.56 34 32.62 8 45.68 47 16.80	28.43 27.77 27.62 25.75 25.05 24.77	16 53 18.81 58 10.37 59 18.44 17 10 9.54 13 55.86 15 29.28	7 40 38 8 40 1 4 40 24 6 39 58 8 40 37	3 48.69 18.18 1 18.3° 3 30.73	9 8 7 3
	8.9 8.9 8.9 8.9 8	0.5	29.3 44. 48.5 2. 15.1 29.	$ \begin{array}{c ccccc} 0 & . & . & . \\ 0 & 58 & 3 & . & . \\ . & . & . & . \\ . & . & . & . \\ . & . & . & . \\ 44 & . & 0 & 58 \\ 7 & . & . & 32 \\ 243 & . & . & . \end{array} $				16 52 6.83 56 58.39 58 6.52 17 8 57.56 12 43.93 14 17.27 16 43.70	71.9 71.9 71.9 71.9 71.9 72.0 71.9	8 2. 1 38.805 8 2. 1 43.26 1 II. 7 37.05 8 I. 3 42.89 3 II. 7 41.80 1 2. 2 36.08 6 2. 5 43.60	51 35.52 49 0.92 11 30.56 34 32.62 8 45.68 47 16.80 22 20.28	28.43 27.77 27.62 25.75 25.05 24.77 24.31	16 53 18.81 58 10.37 59 18.42 17 10 9.54 13 55.86 15 29.28 17 55.66	7 40 38 8 40 1 4 40 24 6 39 58 8 40 37 6 40 15	3 48.69 1 18.18 1 18.3° 3 30.73 1 .5° 2 4.59	9 8 7 3 7
	8.9 8.9 8.9 8.9		29.3 44. 48.5 2.	0				16 52 6.83 56 58.39 58 6.52 17 8 57.56 12 43.93 14 17.27	71.9 71.9 71.9 71.9 71.9 72.0	8 2. 1 38.805 8 2. 1 43.26 1 II. 7 37.05 8 I. 3 42.89 3 II. 7 41.80 1 2. 2 36.08 6 2. 5 43.60 6 III. 6 33.40	51 35.52 49 0.92 11 30.56 34 32.62 8 45.68 47 16.80	28.43 27.77 27.62 25.75 25.05 24.77	16 53 18.81 58 10.37 59 18.44 17 10 9.54 13 55.86 15 29.28	7 40 38 8 40 1 4 40 24 6 39 58 8 40 37 6 40 12 40 9	3 48.69 18.18 1 18.3° 3 30.73	9 8 7 9 6
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	8.9 8.9 8.9 8.9 8	0.5	29.3 44. 48.5 2. 15.1 29.	0		9.4		16 52 6.83 56 58.39 58 6.52 17 8 57.56 12 43.93 14 17.27 16 43.70 17 40.73 19 10.79	71.9 71.9 71.9 71.9 71.9 72.0 71.9 72.0	8 2. 1 38.805 8 2. 1 43.26 1 II. 7 37.05 8 I. 3 42.89 3 II. 7 41.80 1 2. 2 36.08 6 2. 5 43.60 6 III. 6 33.40 1 " 3 29.25	51 35.52 49 0.92 11 30.56 34 32.62 8 45.68 47 16.80 22 20.28 19 30.12 42 26.58 35 27.90	28.43 27.77 27.62 25.75 25.05 24.77 24.31 24.14 23.86	16 53 18.81 58 10.37 59 18.42 17 10 9.54 13 55.86 15 29.28 17 55.66 18 52.69 20 22.86 17 23 52.00	7 40 38 8 40 1 4 40 24 6 39 58 8 40 37 6 40 12 0 40 32	3 48.69 1 18.18 1 18.3° 3 30.73 7 1.5° 2 4.59 1 14.20 2 10.44	9 8 7 3 7 9 6 4
	8.9 8.9 8.9 8.9 8	0.5	29.3 44. 	0		9.4		16 52 6.83 56 58.39 58 6.52 17 8 57.56 12 43.93 14 17.27 16 43.70 17 40.73 19 10.79 17 22 40.00	71.9 71.9 71.9 71.9 71.9 72.0 71.9 72.0	8 2. 1 38.805 8 2. 1 43.26 1 II. 7 37.05 8 I. 3 42.89 3 II. 7 41.80 1 2. 2 36.08 6 2. 5 43.60 6 III. 6 33.40 1 " 3 29.25	51 35.52 49 0.92 11 30.56 34 32.62 8 45.68 47 16.80 22 20.28 19 30.12 42 26.58 35 27.90	28.43 27.77 27.62 25.75 25.05 24.77 24.31 24.14 23.86 23.21	16 53 18.81 58 10.37 59 18.42 17 10 9.54 13 55.86 15 29.28 17 55.66 18 52.69 20 22.86 17 23 52.00	7 40 38 8 40 1 4 40 24 6 39 58 8 40 37 6 40 12 0 40 32	3 48.69 1 18.18 1 18.3° 3 30.73 7 1.5° 2 4.59 1 14.20 2 10.44	9 8 7 9 6 4 1
	8.9 8.9 8.9 8.9 8	0.5	29.3 44. 	0		9.4		16 52 6.83 56 58.39 58 6.52 17 8 57.56 12 43.93 14 17.27 16 43.70 17 40.73 19 10.79 17 22 40.00	71.9 71.9 71.9 71.9 71.9 72.0 71.9 72.0 72.0	8 2. 1 38.805 8 2. 1 43.26 1 II. 7 37.05 8 I. 3 42.89 3 II. 7 41.80 1 2. 2 36.08 6 2. 5 43.60 6 III. 6 33.40 " 3 29.25 0 2. 3 41.29	51 35.52 49 0.92 11 30.56 34 32.62 8 45.68 47 16.80 22 20.28 19 30.12 42 26.58 35 27.90	28.43 27.77 27.62 25.75 25.05 24.77 24.31 24.14 23.86 23.21 MENT RE.	16 53 18.81 58 10.37 59 18.44 17 10 9.54 13 55.86 15 29.28 17 55.66 18 52.69 20 22.86 17 23 52.00 ADINGS.	7 40 38 3 40 1 4 40 24 5 39 58 3 40 35 5 40 35 5 40 35 0 40 8 0 40 25	3 48.65 18.18 1 18.33 3 30.73 7 1.5 2 4.55 1 14.26 3 10.44 5 11.13	9 8 7 9 6 4 1
	8.9 8.9 8.9 8.9 8	0.55	29.3 44. 	0		9.4	c.	16 52 6.83 56 58.39 58 6.52 17 8 57.56 12 43.93 14 17.27 16 43.70 17 40.73 19 10.79 17 22 40.00	71.9 71.9 71.9 71.9 71.9 72.0 71.9 72.0 72.0	8 2. 1 38.805 8 2. 1 43.26 1 II. 7 37.05 8 I. 3 42.89 3 II. 7 41.80 1 2. 2 36.08 6 2. 5 43.60 6 III. 6 33.40 1 " 3 29.25	51 35.52 49 0.92 11 30.56 34 32.62 8 45.68 47 16.80 22 20.28 19 30.12 42 26.58 35 27.90	28.43 27.77 27.62 25.75 25.05 24.77 24.31 24.14 23.86 23.21 MENT RE.	16 53 18.81 58 10.37 59 18.42 17 10 9.54 13 55.86 15 29.28 17 55.66 18 52.68 20 22.86 17 23 52.06 ADINGS.	7 40 38 8 40 1 4 40 24 6 39 58 8 40 37 6 40 18 9 40 9 0 40 9 0 40 25	3 48.69 18.18 18.33 3 30.77 1.52 2 4.59 14.20 2 10.44 5 11.11	9 8 7 9 6 4 1
	8.9 8.9 8.9 8.9 8 8.9 9 8	0.55	29.3 44	0		19.4	c.	16 52 6.83 56 58.39 58 6.52 17 8 57.56 12 43.93 14 17.27 16 43.70 17 40.73 19 10.79 17 22 40.00	71.9 71.9 71.9 71.9 71.9 72.0 71.9 72.0 72.0	8 2. 1 38.805 8 2. 1 43.26 1 II. 7 37.05 8 I. 3 42.89 3 II. 7 41.80 1 2. 2 36.08 6 2. 5 43.60 6 III. 6 33.40 1 3 29.25 0 2. 3 41.29	51 35.52 49 0.92 11 30.56 34 32.62 8 45.68 47 16.80 22 20.28 19 30.12 42 26.58 35 27.90 INSTRU	28.43 27.77 27.62 25.75 25.05 24.77 24.31 24.14 23.86 23.21 MENT RE. CIRCLE B. C. 22.13 21. 20.7 19.	16 53 18.81 58 10.37 59 18.42 17 10 9.54 13 55.86 15 29.28 17 55.66 18 52.63 20 22.86 17 23 52.06 ADINGS. D. Mean. 5 17'.6 21'.62 9 16.0 20.02	7 40 38 8 40 1 4 40 24 6 39 58 8 40 37 6 40 18 9 40 9 0 40 9 0 40 25 BAR.	3 48.66 18.18 18.38 3 30.77 1.55 2 4.56 0 14.20 2 10.44 5 11.11	9 8 7 9 6 4 1
	8.9 8.9 8.9 8.9 8 8.9 9 8	0.55	29.3 44	0		19.4	c.	16 52 6.83 56 58.39 58 6.52 17 8 57.56 12 43.93 14 17.27 16 43.70 17 40.73 19 10.79 17 22 40.00	71.9 71.9 71.9 71.9 71.9 72.0 71.9 72.0 72.0	8 2. 1 38.805 8 2. 1 43.26 1 II. 7 37.05 8 I. 3 42.89 3 II. 7 41.80 1 2. 2 36.08 6 2. 5 43.60 6 III. 6 33.40 1 3 29.25 0 2. 3 41.29	51 35.52 49 0.92 11 30.56 34 32.62 8 45.68 47 16.80 22 20.28 19 30.12 42 26.58 35 27.90 INSTRU	28.43 27.77 27.62 25.75 25.05 24.77 24.31 24.14 23.86 23.21 MENT RE. CIRCLE B. C. 22".3 21".	16 53 18.81 58 10.37 59 18.42 17 10 9.54 13 55.86 15 29.28 17 55.66 18 52.63 20 22.86 17 23 52.06 ADINGS. D. Mean. 5 17'.6 21'.62 9 16.0 20.02	7 40 38 8 40 1 4 40 24 6 39 58 8 40 37 6 40 12 9 40 9 0 40 9 0 40 9 0 40 9 0 40 9 0 40 9 0 40 9 0 40 9 0 40 9	3 48.66 1 18.18 1 18.37 3 30.77 7 1.57 2 4.59 1 14.20 3 10.44 5 11.11 THERM At. 85.0	9 8 7 3 7 9 6 4 1

er.	itude.		SE	CON	DS (OF 7	ΓRA	NSIT	's.						1	1	ın Right	1	n Sot	
Number.	Magnitude.	I.	п.	ш.	ıv.	ν.	vi.	vII.	10.	11.	Т.	a.	MICROMETER.	D.	d.		scension, 850.0.	1850	linatio	on,
			Z	one :	XXX	VII	Ι.	July	10.	N	ſ. D. = −39	9° 49′ 20″.	o. n'. == -30.0	00. n.=-1	14.95.	(Con	tinued.)			
11	7					30.0	44.5	59.1			h. m. s. 17 15.84	+71.95	7. 10. 7 43.30	_ 7 53.22	23".	$\begin{array}{c c} h \\ 11 & 17 \end{array}$	m. s. 27.79	39° 57′	36.00)
12	7		9.7	23.7	38.0	1					25 38.17	71.98	I. 5 41.67	23 27.69	22.	66	$26\ 50.15$	40 13	10.33	5
13	7				• •		1	36.2			25 52.47	72.03	8	53 6.48	22.	ľ	27 4.50	40 42		
14	7.8		• •	• •		• •	1	9.0			30 25.70	71.96	2	10 31.02	21.		31 37.66	1	12.80	
15 16	8			• •				38.0	$\frac{.}{37.2}$	` . 51 8	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	71.96 72.00	1	12 25.01 33 0.69	$\frac{21.5}{21.5}$		31 6.96 31 44.43	$\begin{vmatrix} 40 & 2 \\ 40 & 22 \end{vmatrix}$	6.8	
17	8.9						5.0	19.7			32 36.51	71.97	1	12 24.56	21.	1	33 48.48	40 22		
18	8.9				58.0	1	1				35 57.87	72.02	i	41 13.45	20.		37 9.89	40 30		
19	7						1	51.0		[36 7.67	72.00	8	29 49.05	20.		37 19.67	40 19		
20	2.3					8.0	22.3	36.7			$36\ 53.57$	71.97	IV. 6 42.75	14 5.49	20.	55	38 5.54	40 3	46.0	4
21	5.6			15.6	30.0	44.0	58.7	13.0			38 29.89	71.97	I. 6 45.49	12 30.29	20.	25	39 41.86	40 2	10.5	4 в.
22	6					l .	1	31.2			39 47.49	72.0	ž.	53 36.61	20.	ì	40 59.54	40 43		
23	8.9		27.5		56.6			39.5			42 56.31	71.99	I. 5 41.97	23 17.34	19.	41	44 8.30	40 12		
24	8.9										45 4.45	72.00	2. 3 48.00	31 34.84	19.	00	46 16.45	40 21	13.8	4
25	5.6							56.0			45 12.59	72.00	1	26 51.55	18.		46 24.59	40 16		
26	9	• •		• •		1	47.0	1		[48 18.07	72.09	3	36 21.55	18.	ı ı	49 30.09	40 25		
27	8		00.0	90 1			1	11.4	٠.		50 28.03	72.0	N .	29 35.57	17.		51 40.04			
28 29	8.9		23.8	38.1	1	1	1	$36.0 \\ 44.0$	• •	• • •	52 52.62 $55 0.98$	72.04 71.96	N .	48 28.97 6 26.73	17.		54 4.66 56 12.94	40 38 39 56		
*30	8.9		35.0	l .		1	30.0	44.0			59 3.82	72.09	9	37 30.69	17. 16.	ŧ	0 15.84	1		
			30.0																	
31	8.9			177		1		44.0		٠.	18 0 0.72	71.99	1	24 28.77	16.		1 12.71	1	4.9	
32 33	8	55 7			32.0	1		$ \cdot\cdot $	• •	• •	$\begin{bmatrix} 2 & 31.73 \\ 4 & 39.17 \end{bmatrix}$	71.9	8	9 20.38	15.	4	3 43.70	39 58		
34	8.9	33.1	$\frac{10.5}{40.7}$	1	1	1	38.0	1			7 9.29	72.03	4	41 14.76 39 55.41	15. 14.		5 51.20 8 21.31		50.0 30.1	
35	8							44.8			8 58.99	72.00	8	30 4.66	14.		10 10.99	1	39.0	
36	6							3.0			20 19.84	71.9	Š.	9 16.44	12.	1	21 31.79			
37	8							20.6		٠.	18 27 37.50	71.9	2. 7 30.34	15 22.99	10.		28 49.46	1	53.8	
						2	Zone	XXX	IX.	J	uly 10. M.	$D.$ \equiv	26 58 10.0. r		n".— 8".	17.				
1	6.7	Ī					9.5	521.7			19 40 44.62	70.7	4 I. 1 37.27	52 15.49	19.	62 19	41 55.36	27 50	45.1	1 в.
2	6.7				• •			i .	l .	24.0		1	0 VII. 4 43.15	28 53.57	19.		42 26.65			
3	7					• •		38.5		• •	43 1.49	70.6	8	20 54.12	19.		44 12.17	j		
4	7.8	• •				• •		25.0	1		43 48.27	70.6	i	6 12.04	19.	8	44 58.93	1		
5 6	8 4.5	: :	9.0		133.4			21.0		• •	44 43.92 46 33.46	70.6	B .	31 10.36 35 15.65	18. 18.		45 54.61 47 44.16	1	39.2 44.1	
7	8.9)			1	22.8		::	48 45.94	70.7	8	40 12.83	18.	1	49 56.64			
8	9		5.7	1		::		1			50 30.38	70.6	ı	36 41.62	17.		51 41.07	1		
9	9		I	i		1	1	1	30.5	1 1	50 35.24	70.6	1	9 14.94	17.	2	51 45.89			
10	6.7	14.4	27.0	39.2	251.7	3.8	3 16.5	5			19 54 51.64	70.6	4 I. 6 40.37	15 25.46	16.	70 19	56 2.28	27 13	52.1	6 z.
														INSTRU	JMENT	READIN	īgs.			
															CI	RCLE.		BAR.	тнен	кмом.
														Α.	в.	с.	Mean.	BAR.	At.	Ex.
													Zone XXXIX.—July 10,	h. 19.7 293° 39′ 43″.5	35.2	36.2 3	5.0 35.47	1. 30,075	81°.5	79,2
												A PROPERTY AND A PROP	,	32.0		1 1	4.0 33.27	8		
l				***************************************	ramenozara, o pa	oca where we	and a serior of	meronogerative	-	mmenson week on the			· · · · · · · · · · · · · · · · · · ·					<u> </u>	<u> </u>	

11 12 13 9	Magnitude.	ī.	11.	1111.	IV.	v.	v1.	vII.	10.		Т.	a.		MICROMETER.	D.	d.			-,		ion,
12 8 13 9 14 8	8.9			į.			1 1		10.	11.								Ascension 1850.0.	1	850.0.	
12 8 13 9 14 8	8.9				Zone	XX	XIX.		July	10.	M. $D. =$	= 26° 58	10.0	n'. —20.00.	n". —817.	(6	ontinu	ied.)			
13 9 14 3	9					46.0	58.0	10.5			h. m. s. 19 56 33.44	+70.		VI. 2 47.74	-40 ['] 22 ^{''} .59	-16".	37 1	h. m. s. 9 57 44.1	.2 27°	38 ['] 48 ^{''} .	96 z.
14 3							30.0			• •	$58 ext{ } 5.23$	70.	- 4	VII. 4 44.42	27 35.17	16.9	N N	59 15.8		26 1.	
	5			$ \cdot\cdot$			42.0			• •	20 3 17.64	70.	A A	IV. 4 37.72	31 26.91	15.9	8	0 4 28.2		29 52.5	
10 (• •	• •	16.8			9.59.53			• •	$4\ 44.67$ $8\ 29.16$	70. 70.	H	II. 4 40.12 I. 3 43.985	30 3.93 33 46.68	15.0 14.3	ž.	5 55.3 9 39.8		28 28.9 32 11.0	
16 8	8			1			252.0				10 27.11	70.	1	" 1 41.45	49 51.10	13.9	ī	11 37.7	4	48 15.0	
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- 1	8				i I		40.8	- 1	1		16 16.07	70.	.58	III. 7 42.92	8 6.66	12.8	88	17 26.6	5 27	6 29.	54 z
19 8	8					21.5	34.0				17 9.26	70.	61	IV. 4 43.09	28 21.43	12.	74	18 19.8	1	26 44.	
20 8	8				23.0	35.2	47.1			• •	$19\ 22.73$	70.	64	I. 1 41.24	49 58.34	12.	16	20 33.3	7 27	48 20.	50 z.
21 8	8.9			١		56.0		21.0			20 43.85	70.	.60	VII. 4 40.30	29 57.48	11.)1	21 54.4	5 27	28 19.3	39 z
22 9	9			26.0	1		1		١		38.35	70.	.62	IV. 2 44.82	42 3.46	11.	75	48.9	7 27	40 25.5	21
23 8	8					43.0	55.5	8.0			$24\ 30.77$	70.	.62	" 2 38.00	45 59.03	11.	13	$25 \ 41.3$	9 27	44 20.	46
	8						5.6				$25 \ 41.02$	70.		V. 6 44.44	13 5.20	11.5		26 51.5	-	11 26.	
	7						49.5			• •	30 24.94	70.	i i	I. 7 36.45	11 49.85	10.		31 35.4		10 10.9	
	8			• •	$ \cdot\cdot $		40.5	• •		• •	34 15.71	70.	1	1. 2 36.97	46 33.78	9.	1	35 26.3	1	44 53.	
	6	• •	• •	٠.	• •		26.5			• •	35 1.70	70.	. 9	VI. 3 38.04	$\begin{bmatrix} 37 & 12.28 \\ 26 & 14.60 \end{bmatrix}$	9.	H	36 12.2		35 31.8 24 34.0	
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- 1	4			1	1 1		$\begin{bmatrix} \cdot & \cdot \\ 6.0 \end{bmatrix}$	 18 0			41 41.09	70.	8	IV. 4 39.89	30 11.97	8.	- 6	42 51.6		28 30.	
	8			1			17.7	1			42 52.70	70.		" 2 39.25	45 15.87	8.	- 1	44 3.2		43 34.0	
	8				25.9						49 25.82	70.		I. 3 38.04	37 12.04	7.5		50 36.3	1	35 29.5	27
36 8	8.9		22.0		46.5						50 46.48	70.	.54	10. 3 34.19	39 24.80	7.)2	51 57.0	2 27	37 41.8	32 z
37 3	5						4.6	17.0			51 39.86	70.	.52	11. 4 41.20	29 25.90	6.8	38	52 50.3	1	27 42.	
1	8.9	٠.					49.0	- 1	l .	• •	$54\ 24.35$	70.	ų.	III. 5 45.42	21 13.78	6.	1	55 34.8		19 30.5	
-	7						42.8			• •	57 17.71	70.	8	I. 1 32.44	55 2.28	5.		58 28.2	1	53 18.5	
40 8	8	• •	• •	51.0	3.4	15.5	28.1	40.5			20 59 3.35	70.	.52	" 2 40.89	44 18.87	5.	70 2	1 0 13.8	37 27	42 34.)
						\mathbf{Z} o	ne XI	L.	Ju	ly 11.	H. D.	43	°21′	50.0. n. = -5	20 ["] .29. n. =		.00				
1 9	9				31.3	46.0	1.3	16.4			16 1 31.03	72.	.18	IV. 6 34.510	18 52.60	19.	32 10	6 2 43.2	21 43	41 2.	 42
- 1		57.7	13.3	1	1		13.5		1		10 43.33	72.		" 7 38.072	10 53.25	18.		11 55.5		33 1.3	
1	9	49.2	5.0	19.8	34.0	50.0	5.3	21.0		[18 34.93	72.	.27	" 5 39.636	24 41.42	16.	63	19 47.2	0 43	46 48.0)5
- 1			43.5	59.0	13.8	29.0	44.0	59.8			22 3.94	72.		" 5 45.578	21 13.85	15.9	6	23 16.2	1	13 19.8	
- 1	9										26 8.58	72.		" 3 38.355	37 18.26	15.	8	27 20.9		59 23.4	
- 1	9	• •		l .	1		31.0				27 0.50	72.		" 4 42.395	28 56.50	15.0	•	28 12.8	- 1	$\frac{51}{16} \frac{1.5}{100}$	
7 9	9	• •	59.5	14.5	30.0	45.0	0.2	15.2			16 27 29.79	72.	.35	" 1 34.580	54 17.89	14.9	90 10	6 28 42.1	4 44	16 22.	19
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•			Zone	XL.	July	11.	Н.	$D = -43^{\circ}2$	í 50″.0.	n'. == -20"29.	n". == -20."	00. (Co	ntinued	l.)			
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5	9					59.1			$54\ 28.20$	70.	99 10. 1 35.70	53 43.29	3.34	55	5 39.19	44 45	36.6	;3
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$\frac{14}{15}$	9				$\begin{vmatrix} 42.054 \\ 7.0 \end{vmatrix}$.		1 1		• •	$\begin{array}{c} 19 \ 41.90 \\ 22 \ 7.08 \end{array}$.27	" 7 38.481 " 4 39.310	10 36.97 30 29.15	$\frac{16}{16}$.			1.17 26.36	28 36 28 56		
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July 2	4, at 1	17h	+8	856	+0.003	+0.079	$\theta \mid \stackrel{s}{+} 0.$	300	$^{s.}_{+0.230}$	0 0 0.17	7. 40.117	Z_0	VI.—July 2421			63.0	1		29.908	78°.0	1
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35 36 37 38	8 7.8 8 9	14.0 29.	42.1	38.0 54.6	48.2 51.0 7.11 18.23	 19.43	$\begin{array}{c} . \ . \ . \ . \ . \ . \ . \ . \ . \ . $			58 48.44 58 51.14 22 1 7.17 4 18.42	19 19 19	.10 .10 .10	IV. 5 36.191 " 4 35.738 " 3 40.345 " 3 40.356	26 29.66 32 32.51 35 49.97 35 49.59	10.9 10.9 10.6 10.1	5 5 5 22	9 7.54 9 10.24 1 26.27 4 37.50	28 52 28 58 29 1	20.6	5 9 2 z.
39 40 41	8.9 8 9	8.3	$\begin{array}{c} 21.0 \\ 16.2 \\ \end{array}$	33.2 	46.0 54.0	 6.21	$egin{array}{c} 1.0 \\ 6.81 \\ 18.23 \\ \end{array}$	9.1 1.1		9 45.93 10 41.53 11 53.57	19 19	.04 .04 .04	" 5 36.843 VI. 4 37.272 IV. 4 34.762	26 7.11 31 39.44 33 6.23	9.2 9.1 8.9	3 1 1 1	0 4.97 1 0.57 2 12.61	28 51 28 57 28 58	$\begin{array}{c} 56.3 \\ 28.5 \end{array}$	9 z. 8
42 43 44 45 46	8.9 9 8 9	48.0	0.7	 13.0	45.0 5 4.0 1 25.8 40.0 5 10.0 2	16.52 62.2	$\frac{28.2}{5.01}$	7.5		14 44.78 15 3.80 17 25.67 17 39.86 21 10.03	19 19 19	.00 .00 .00 .02 .97	" 6 44.996 " 7 43.649 " 5 46.592 " 2 46.863 " 7 38.692	12 42.95 7 38.39 20 30.31 40 50.15 10 29.61	8.56 8.56 8.16 8.16 7.66) 1. 3 1. 2 1.	5 3.78 5 22.80 7 44.67 7 58.88 1 29.00	28 46	26.8 18.4 38.2	9 7 7
47 48 49 50 51	9 9 9	5.5 25.5 56.3 32.3	18.0 238.0 6 844.8	30.3 22.0 57.2	43.0 5	55.5 5	8.0 2 	2.0	• • •	24 43.00 27 3.12 27 34.37 30 9.89 31 3.52	18 18 18 18	.97 .98 .97 .95	" 4 41.350 " 1 42.220 " 3 34.211 " 3 37.912 " 3 32.308	29 18.68 49 22.19 39 21.88 37 14.00 40 27.63	7.16 6.86 6.73 6.4 6.33	5 2 5 2 8 2 1 3	$ \begin{array}{cccc} 1 & 29.00 \\ 5 & 1.97 \\ 7 & 22.10 \\ 7 & 53.34 \\ 0 & 28.84 \\ 1 & 22.47 \\ \end{array} $	28 55 29 15 29 5 29 3	5.8	4 4 z. 6 4
*52 53 54 55	8.9 9 8.9 8	28.9 36.8	41.0 49.2	53.0 1.3 $$ 12.3	6.01 14.02 4 25.23	18.03 26.0 14.25 37.85	31.0 57.0 50.2	9.3 		31 5.86 34 13.94 34 31.77 39 25.13	18 18 18	.95 .91 .92	V. 3 29.992 " 6 42.250 " 4 39.432 IV. 1 36.259	41 47.58 14 17.79 30 24.91 52 48.15	6.35 5.96 5.86 5.25	3 3 7 3	1 24.81 4 32.85 4 50.69 9 44.05	29 7 28 40 28 56 29 18	$\frac{33.9}{3.6}$	0 z. 9 z. 8 z.
56 57 58 59 60	9 8 9 8.9 9	45.0 52.3	$28.2 \\ 57.8 \\ 5.1$	$40.3 \\ 10.2 \\ 17.0$	53.5 23.0 3	$5.81 \\ 35.0 \\ 12.25$	$\begin{bmatrix} 8.3 \\ . \\ . \\ . \end{bmatrix}$	7.5		43 45.22 44 53.28 46 22.74 47 29.93 49 11.68	18 18 18	.88 .89 .85 .85	" 4 37.056 " 2 36.270 " 6 44.341 " 5 41.301 " 5 47.080	31 47.00 46 56.14 13 5.59 23 33.15 20 13.48	4.73 4.66 4.4 4.33 4.19) 4. 1 4: 1 4:	4 4.10 5 12.17 6 41.59 7 48.78 9 30.52	28 57 29 12 28 38 28 49 28 45	40.7 50.0 17.4	4 3 6 z.
61 62 63 64	8.9 9 9			$\frac{.}{30.8}$	43.15 54.0	$\begin{array}{c} 21.03 \\ 55.2 \\ 6.21 \end{array}$	$\begin{array}{c} 34.04 \\ 8.02 \\ 9.03 \end{array}$	1.4		50 8.94 50 8.59 51 43.00 52 53.89	18 18	.84 .85 .83	VI. 3 31.992 IV. 6 36.180 " 5 42.280	31 19.56 40 38.43 17 47.51 22 59.32	4.09 4.09 3.89 3.79	2 56 5 55	0 27.78 0 27.44 2 1.83 3 12.71	28 57 29 6 28 43 28 48	3.58 22.4 31.3	8 z. 5 z. 6
65 66	1							6.5 6.5		55 38.86 23 1 18.93	1	.83 .79	" 3 38.340 " 4 43.092	36 59.24 28 18.47	3.4° 2.90	5	5 57.69 1 37.72	29. 2	42.7	1 z.
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					C	ORRE	ECTIO	ons.						INSTRU	MENT R	EADINGS				
			COR.		HOURL	Y	m.	n.	c.	ZENITH POINT.	COINC.				CIRCI	Е.		BAR.	THER	мом.
July 29	9, at 177	h	+ 9.	228	$^{s.}_{+0.00}$	19 0	s.	s. 0.200	s. 0.330	-	r. 40,120	Zor	ne VII.—July 2917.9	279° 51 2″.5		d'.6 0'.2	Mean.	1. 29.960	At.	Ex.
	.,		1.0.		70.00			0,200	0.000	99.86 86 86	40.120	AL	18.5		1 1	4.6 0.2 8.7 3.8	2.55 5.95	29.960 29.960	76.0 75.2	70.9 70.7
	-						- widele													

Number.	Magnitude.	1.	seco.	NDS OF	1	NSITS.		т.	a.	MICROMETER.	D.	d.	Mean Right Ascension, 1850.0.	De	n Sou clinatic	
			Zoi	ne XLVI	I. J	ul y 29.	М.	D = -46	3 50 10°.0	. n. = -13.00.	n'.=-1	2.85. (Continued.)			
4 5 6 7 8 9 10 11	8.9 9 9	20.0 52.5 24.5	34.2 49. 7.5 22. 5.0 19. 39.2 53. 30.	0 8.2 23. 4.0 18. 2 51. 0 34.0 48. 5 8.2 22. 3 45.2 44. 2 16.0 31.	4 33.2 4 0 0 2.8 3 8 37.2 5 	48.0 17.2 52.1 14.0		h. m. s. 18 5 8.43 13 3.93 19 36.61 20 33.73 23 8.24 26 45.15 28 30.02 18 30 16.18	21.3 21.4 21.4 21.5 21.5 21.5 21.5 21.5	85	-49 29".91 49 59.76 23 8.74 19 26.11 29 1.43 53 41.31 43 42.01 44 6.04	11".49 9.16 7.25 6.97 6.21 5.15 4.64 4.12	h. m. s. 18 5 30.30 13 25.78 19 58.39 20 55.50 23 30.02 27 6.97 28 51.81 18 30 37.97	41 40 41 13 41 9 41 19 41 43 41 33	51.40 18.92 25.99 43.08 17.64 3 56.46 3 56.65 20.16	2 9 8 4 6 5
				Zone :	XLVII	I. Ju	aly 29.	H. D	.=-28°	26 00.0. n.=-	33.67. n.:	$=-7^{''}.00.$				
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29	8 9 9 9 9 9 9 8.9 9 8.9 9 9 8.9	57.5 17.5 8.5 47.3 20.5	25.0 37. 26.0 38	2 3	2	9.5 4.0 22.0 9.5 4.0 555.0 4.0 551.5 		18 34 37.40 35 49.88 35 50.8° 36 4.66 39 35.16 40 32.91 41 14.02 42 55.30 43 53.65 44 46.26 45 32.17 46 47.11 48 25.13 50 19.79 50 15.70 51 27.77 51 32.33 52 26.22 52 44.58 19 48 21.38 48 17.53 49 10.84 50 58.43 52 32.89 53 8.03 54 24.97 55 14.19 57 4.00 19 59 43.47	20. 20. 3 20	55	38 19.20 29 1.35 28 45.14 40 2.81 47 57.09 19 59.68 29 52.82 27 44.38 28 25.07 26 34.57 17 24.14 37 25.46 30 20.24 20 55.49 27 39.39 28 23.28 35 6.27 24 48.93 24 34.86 33 11.42 17 6.30 36 57.69 33 18.76 10 31.00 21 11.13 36 33.14 15 30.21 21 32.34 26 6.44	30.03 29.73 29.73 29.67 28.80 28.57 28.40 27.99 27.75 27.54 27.35 27.04 26.65 26.18 26.20 25.90 25.89 25.67 25.60 12.51 12.52 12.31 11.92 11.58 11.44 11.16 10.98 10.57 9.98	18 34 57.97 36 10.43 36 11.42 36 25.21 39 55.74 40 53.43 41 34.55 43 15.22 44 14.17 45 6.78 45 52.67 47 7.64 48 45.64 50 40.28 50 36.20 51 48.27 51 52.84 52 46.71 53 5.07 19 48 41.67 48 37.79 49 31.13 51 18.71 52 53.13 53 28.28 54 45.24 55 34.42 57 24.23 20 0 3.70	28 55 29 6 29 14 28 46 28 56 28 54 28 55 28 43 29 3 28 56 28 54 29 1 28 51 28 59 28 43 29 3 28 59 28 43 29 3 28 59 28 43 29 3	49.23 31.08 31.08 14.87 32.48 25.89 28.25 21.22 12.37 52.82 2.11 351.49 35.50 46.89 49.18 32.16 14.60 123.93 18.82 10.00 30.68 42.58 42.57 44.30 41.19 16.42	8 7 8 9 9 5 5 2 2 7 7 2 2 1 1 9 9 0 z. 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
	,			COI	RECTION	ons.					INSTRU	MENT RE	ADINGS.			
			COR. TO	HOURLY COR.	m.	n.	c.	ZENITH POINT.	COINC.		Α.	CIRCLE.		BAR.	At.	мом. Ех.
* T)	29, at 1	n of t	s. + 9.228	**************************************	1.	s. +0.200	+0.330 from the	359°59′59″86	r. 40.120	Zone h. XLVIII.—July 29, 18.6 20.5		2.8 5.	*1.78	1. 29.960 29.944		70°.5

Number.	Magnitude.	I.	SECO		F TRAN	NSITS.	11.	T.	a.	MICROMETER.	D.	d.	Mean Right Ascension, 1850.0.	, De	an Sout	
4			Zo	ne XLV		July 29		. D.=-2	8° 26 [′] 00′.	/00. n.'=-33.'(37. n."=-	7.00. ((Continued.)			
30 31 32 33 34 35 36 37 38 39 40 41 42 43	9 9 9 8.9 7 9 8	15.0 49.2 17.6 	26.6 38.8 	5 48.2 (8 53.0)	$egin{array}{cccccccccccccccccccccccccccccccccccc$	18.5 37. 30.0	2 50.5 3	h. m. s. 20 0 20.07 1 51.64 2 41.07 5 52.44 6 17.11 7 27.00 14 37.53 15 55.12 16 56.44 17 57.32 18 15.85 21 48.07 22 52.53 23 13.07	+20.2 20.2 20.2 20.2 20.1 20.1 20.1 20.1 20.1 20.1 20.1 20.1 20.1	4 " 2 45.223 4 VII. 2 44.706 1 IV. 4 40.570 8 VI. 6 43.815 7 IV. 7 40.625 6 " 5 37.600 8 " 2 43.786 6 " 4 37.292 8 V. 1 37.545 3 VI. 5 49.341 3 IV. 4 41.290 4 " 3 32.778	-17 6.61 41 48.57 42 6.08 29 47.27 13 25.23 9 24.48 25 42.64 42 38.18 31 40.57 52 5.40 18 56.90 29 22.45 40 13.09 39 52.51	- 9".85 9.52 9.34 8.65 8.56 8.31 6.78 6.51 6.29 6.08 6.01 5.26 5.04 4.97	h. m. s. 20 0 40.28 2 11.88 3 1.31 6 12.65 6 37.29 7 47.17 14 57.69 16 15.30 17 16.60 18 17.50 18 35.96 22 8.20 23 12.67 23 33.21	29 1 28 55 20 1 28 55 20 1 28 55 20 1 20 1 20 1 20 1 20 1 20 1 20 1 2	3 16.46 7 58.09 8 15.42 5 55.92 9 33.79 1 49.42 8 44.69 7 46.86 8 11.48 5 2.91 5 27.71 6 18 13 5 57.48	z. z. z.
44 45 46 47 48	9 9 8 8	14.8 57.3	0.5 12. $27.8 40.$ $22.0 34.$ $10.2 22.$	$7 \begin{vmatrix} 25.3 \\ 38 \end{vmatrix} 38 \\ 47.1 \begin{vmatrix} 59 \\ 35.0 \end{vmatrix} 47 $	3.0 50.6 9.8 12.8	12.6		25 25.45 26 52.80 27 47.34 28 35.08 20 31 25.48	20.1 20.1 20.1 20.1 20.1 20.1	3	39 32.31 40 3.36 33 56.95 47 41.41 30 47.17 38 32.06	4.57 4.50 4.20 4.00 3.84 3.26	25 45.58 27 12.92 28 7.47 28 55.18 20 31 45.58	29 0 29 0 29 1 28 50	5 57.48 6 7.86 0 1.15 3 45.41 6 51.01 4 35.32	z.
		1	1 1	Zo	one XLIX	Х. А	ugust i	11. H.	D = -4	10° 19′ 50″.0. n′.=	=-25.83.	n".=-12	.00.			
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	9 9 8 8.9 8 9 9 9 9 6 9 9 8 8	57.4	8.0	8 41.4 50 0 53.0 6 2 41.0 53 6 27.8 45 	1.0	24.5 24.2 30.2 7.0 		17 48 33.57 50 36.75 53 41.38 59 52.52 18 2 40.96 5 27.89 4 46.95 7 58.28 13 22.12 20 32.19 26 19.96 32 51.56 33 23.59 36 51.91 37 42.64 40 2.82 41 21.64 18 43 47.60	23.3 23.3 23.3 23.2 23.2 23.2 23.2 23.2	4 " 4 41.923 0 " 6 36.000 6 " 7 44.858 4 " 1 42.930 4 " 7 38.426 6 VI. 6 38.200 4 IV. 7 40.680 5 " 4 43.930 6 " 1 42.209 1 " 3 41.926 8 " 3 39.713 0 " 2 37.410 1 " 6 43.560 7 V. 2 44.000 8 IV. 1 35.120 5 " 2 39.611	22 13.54 29 5.17 17 56.39 6 55.82 49 10.77 10 39.32 16 39.78 9 20.87 27 55.45 49 35.90 35 3.58 36 20.42 46 29.06 13 33.71 42 39.84 53 42.28 45 12.34 25 32.31	23.85 23.39 22.69 21.30 20.67 20.03 20.19 19.46 18.26 16.64 15.34 13.87 13.75 12.97 12.81 12.26 11.97 11.44	17 48 56.89 51 0.09 54 4.68 18 0 15.78 3 4.30 5 51.13 5 10.21 8 21.52 13 45.37 20 55.45 26 43.17 33 14.74 33 46.79 37 15.02 38 5.81 40 26.00 41 44.79 18 44 10.70	40 44 44 44 44 44 45 44 55 44 15 44 15 41 15 41 15 41 15 41 15 41 15 41 15 16 16 16 16 16 16 16 16 16 16 16 16 16	2 27.39 9 18.56 8 9.08 7 7.12 9 21.44 0 49.35 6 49.97 9 30.33 8 3.71 9 42.54 5 8.92 6 24.29 6 32.81 3 36.68 2 42.65 3 44.54 5 14.31 5 33.75	В.
			COR. TO	HOURLY	м. т.	n.	c.	ZENITH POINT.	COINC.			CIRCLE		BAR.	THERM	om.
Aug. I	11, at 1	81	s. +10.685	s.	$\frac{s}{+0.294}$	s. +0.300	+0.230		7. 40.085	XLIX.—August 11, 1 1 1 1	A	61.8 64. 62.6 64.		30.106 30.108 30.100 30.114	78°.0 7 76.5 7 75.2 6	Ex. 72°.5 70.6 68.0

lber	Magnitude.		SE	CON	DS (OF '	ΓRA:	NSIT	s.		Т.	a.	MICROMETER.	D.	d.	Mean Asce	Right		n Sou linatio	
Number	Mag	I.	11.	ш.	ıv.	v.	VI.	VII.	10.	11.						1850	.0.	1850	0.0.	
				\mathbf{Z} on	e XI	JX.	A	Lugus	t 11.	Н	D = -40	ຶ້ນ 19 50.0.	n'. == -25 ["] .8	3. n'.=-	12.00.	(Continu	ıed.)			
19 20	9			1	1		2 4.0 0 18.8				18 45 35.07 48 49.70	$^{s.}_{+23.09}$ $^{23.08}$	v. 5 37.216 IV. 4 41.828	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{bmatrix} -11^{''}\!.04 \\ 10.34 \end{bmatrix}$	18 45 49	$58.16 \\ 12.78$	40° 46° 40° 49°	8.68	3
21 22	8.9		31.	45.5	5						51 10.13 53 0.13	23.07 23.02	" 4 36.765 " 7 35.340	32 4.34 13 35.93	9.83 9.43	53	33.20 23.15	40 52 40 33	35.36	5
23 24 25	5.6 8.9 9		54.0	8.2	23.0	37.	$ \begin{array}{c c} 2 & . & . \\ 0 & 52 & . \\ 0 & 36 & . \end{array} $	ι			$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c c} 23.01 \\ 23.02 \\ 22.96 \end{array} $	" 5 41.635 " 3 34.866 " 6 38.638	23 25.94 39 8.86 16 24.68	8.45 7.40 7.03	19 2	53.78 45.91 29.94	40 43 40 59 40 36	6.26	3
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5	9 9		$\begin{vmatrix} \cdot & \cdot \\ 21 & \cdot \end{vmatrix}$	33.5			034.	46.7			9 9.81 $13 45.47$	21.04 21.02	" 4 39.888 " 3 43.243	30 9.86 34 10.48	20.55 19.64	2	30.85 6.49	26 25 26 29		
6 7	8						$\begin{array}{c c} 4 & 34 \\ 9 & 2 \end{array}$	447.0			15 10.24 19 37.63	20.98 20.97	" 6 38.623 " 5 44.058	16 24.02 21 58.72	19.36 18.48	3	31.22 58.60	26 12 26 17		
8	7.8		17.	0 29.	041.	4 53	.5 6.	$0 \dots$			21 41.39	20.96	" 5 36.550	26 18.00	18.08	22	2.35	26 21	56.08	8 z.
9 10	8 9		:		1		$.8 14. \\ .5 55.$	$\begin{bmatrix} 0 \\ 7.5 \end{bmatrix}$	2		22 49.73 27 30.55	20.93 20.94	" 7 42.120 " 3 43.025		17.86 16.97		10.66	26 4 26 29		
11	8		1	l.	1		.0 35.				29 10.71	20.90	" 6 47.311	11 24.01	16.66	8	31.61	26 7		
12 13	$\begin{vmatrix} 9 \\ 8.9 \end{vmatrix}$::					.8		: :		$30 7.47 \\ 32 1.44$	20.91 20.91	" 4 43.581 " 3 40.430	28 2.30 35 47.62	16.48 16.13	ā	28.38 22.35	26 23 26 31		
14	8			0 52.	8 5.	0 17	. 4 29 .	2			33 5.10	20.91	" 3 38.715	36 46.81	15.94	33	26.01	26 32	22.75	5 z.
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17	9		ı				.2 57.		• •		39 12.29	20.87	" 3 35.516	1	14.82	1	33.16	26 34		
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														INSTR	UMENT I	READINGS	5 .			
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Number.	Mag nitude.	I.	SE	CON	IDS (OF T		NSIT		11.	Т.	а.	MICROMETER.	D.	d.	Ħ	Right ension,	De	un So clinat 50.0.	
			J	Z	one L		Aug	ust 1	1.	н.	$D = -2\mathring{5}$	55 20.0.	n'.==-22.47.	n'.=-6.0	0. (Co	ontinue	l.)			
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1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	8 10	39.6 42.0	55.0 57.5 	5.0 7.3 51.0 52.0	28.6 9.4	14.0 22.0 	41.2 54.0 34.7 42.2	 54.0 23.5 6.5 	27.6 	· · · · · 45.0	18 8 1.51 9 16.02 9 45.65 10 31.15 14 28.64 17 9.44 19 17.59 19 17.06		2. 5 44.50 II. 1 45.632 VII. 2 41.65 11. 7 38.22 2. 3 32.97 IV. 3 45.39 2. 5 40.24 IV. 4 39.82 11. 4 44.40 I. 5 46.14 " 1 37.27 II. 3 34.95 III. 2 31.5 VII. 7 41.50	21 40.56 47 23.03 43 48.72 10 43.40 40 2.78 32 54.40 24 7.74 30 10.21 27 30.87 20 44.29 52 11.78 38 54.96 49 39.69 8 50.86 37 30.48	-4.00. 34.91 34.65 34.54 34.38 33.56 33.01 32.56 32.50 31.95 31.19 30.93 30.58 30.04 29.46 MENT RE	9 10 14 17 19 19 22 26 27 29 33 18 34	8 23.44 9 37.98 9 7.60 9 53.05 1 50.57 7 31.34 9 39.47 9 38.95 9 57.52 2 41.84 6 25.46 7 44.46 9 26.43 2 4.25 1 49.47	29 44 29 40 29 7 29 36 29 29 29 20 29 26 29 24 29 17 29 48 29 35 29 46 29 5	26.3 20.9 39.4 30.5 43.4 45.9 46.5 19.3 46.1 529.0 513.4 524.0	1 z. 9 1 z. 7 4 3 0 0 0 7 z. 0 z. 2 z. 0 3 7 z.
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120	Magnitude.		SEC	CON	DS	OF	TRA	NSI	TS.		Т,	a.		MICROMETER.	D.	d.]		Right		n So clinat	
· Tammar	Magı	Ι.	11.	111.	ıv.	v.	vi.	VII.	10.	11.	.			MICHOMETER.	D.		New State of the S	1850		1	0.0.	1011
					Zoi	ne L	I.	Aug	ust]	2.	M. D.—2	8 56 3'	13.	n'. == -36 ["] .59.	n'. —4.00.	. (Conti	nued.)			
16 9)			20.0	32.0						h. m. s. 18 36 32.35	$\begin{vmatrix} & & s \\ & +21 \end{vmatrix}$		I. 2 41.65	$-43^{'}48^{''}.72$	29".	03	h. 1	n. s. 5 54 . 19	29° 40	′ ໑ຄ″ຣ	 2Q ,
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	.7		50.5	3.0			40.9			$ \cdot \cdot $	15 15.67	21		2. 3 34.41	39 13.06	20.			37.28	29 35		
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4 7			• •	٠.		• •	24.0				16 58.95	21		" 3 37.94	37 11.48		94		20.22	29 33		
5 8	5	• •	• •	٠.	• •	٠.	• •	34.0	53.0	• •	17 56.36	21	.24	10. 5 44.23	21 49.87	7.	76	18	17.60	29 18	0.7	/6
5 7	- 1	• •	59.31								$21\ 24.11$	21	.24	2. 2 47.47	40 27.28	7.	10	21	45.35	29 36	37.5	51
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	-		THE AMERICAN PROPERTY.			cor	RECT	ions	•						INSTRU	MENT	REAI	OINGS.		The second secon		_
			cor.		HOUR	- 1	m.		ı.	c.	ZENITH	COINC.				CIR	CLE.			BAR.	тнен	RM
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gust 1	2, at	20h.	+10.3	387		009	s. +0.294	+0	300	$^{s.}_{+0.230}$	0° 0′ 2″.11	r. 40.115	Zor LI	ne h. August 1220.6	291° 42′ 1′.0	5.5	$_{5,3}^{\prime\prime}$	6'.0	$\overset{\prime\prime}{4}.45$	30,098	76°.5	*
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Number.	Magnitude.									- 1	m					7	d.	1		Right		n So clinati	uth
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			,		Z	Zone	LII.		Augu	st 13.	Н.	D.=	28° 26	6 00.0.	n'.=-	—20 ["] .88. n."		7.00.			1		
1	9				16.85	29.2					h. m. 18 51 16		s. +21.43	IV. 4	42.769	28′ 31″.32	—1 8	.15	h. n 18 51	n. s. 38.23	28 54	49.4	7 z.
2	9		[]	12.5	25.03		1			• •	52 25		21.42		38.920	24 57.09		.87		46.66	28 51		
3	9 9	• •	1	• •			20.8		٠.	• •	52 53		21.42	×	39.433	24 39.39		.74		17.22 12.26	28 50		
$\begin{bmatrix} 4 \\ 5 \end{bmatrix}$	9 7.8		31.24		56.9		1 1				54 50 55 56		21.43 21.45	H	35.878 37.995	38 25.97 51 49.89	17	.03		12.26 17.81	29 4 29 18		
6	7		18.03								57 49		21.40	i .	38.015	25 28.35		.61		3.85	28 51		
7	9		42.2							[59		21.40	" 4	36.990	31 50.99	16	.27	59	28.57	28 58	7.2	6
8	9	25.7	38.25								19 1 3	3.30	21.41	0	33.880	39 35.01		.81		24.71	29 5		
9	9	٠.			24.23					• • [1 24		21.38	8	32.142	20 8.73		.73		45.74	28 46		
10	8.9		36.4	49.0	1.2	13.8	26.2	• •		• •	7	1.33	21.36	" 4	41.440	29 17.29	14	.40	7	22.69	28 55	31.6	9 z.
11	9				5.21							5.30	21.35	" 4	43.021	28 22.63		.91		26.65	28 54		
12	9				44.2		• •			• • •	9 44		21.34	8	42.272	23 1.32		.76		5.73	28 49		
13 14	9 9	• •		5.0	18.0					• •		3.28	21.34 21.32	п	36.836 46.007	$ \begin{array}{c cccc} 26 & 9.04 \\ 20 & 52.27 \end{array} $.72 .40		14.62 39.20	$\begin{vmatrix} 28 & 52 \\ 28 & 47 \end{vmatrix}$		
15	9		l 1		18.0		56.0	8.0	• •		11 17 11 30		21.32 21.32	B .	47.820	19 49.33		.35		52.04	28 46		
16	9	ł	28.3				30.0	0.0			13 53		21.32	8	38.662	30 53.20		.81		14.70	28 57		
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18	9			- 1	47.05		1 1		1 1		14 46	6.97	21.32		44.156	27 43.43	12	.59		8.29	28 53		
19	9]	• •	15 59		21.32	9	36.822	31 56.75		.31		20.34	28 58		
20	9	• •	49.0	1.4		26.0	39.0	• •	• •	• •	18 13	3.87	21.30	IV. 4	44.160	27 43.30	11	.79	18	35.17	28 53	55.0	9 z.
21	8.9		1 1				32.3				18 7	1	21.34		41.130	50 1.58		.82		8 28.43	29 16		
22	8.9	50.8		1	28.24		1				21 28	1	21.26	И	45.706	12 20.16		.04		49.53	28 38		
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*27	8.9		l 1		19.03			1			26 18	1	21.27	9	43.670	33 56.77		.94		40.14	29 0		
28	8.9		2	$29.0^{ }$	41.85	54.0		19.2		[26 41	1.65	21.26		43.915	33 48.29	9	.85		2.91	28 59	58.1	4 z.
29	9				8.2						28 8	1	21.27		43.965	42 31.95		.51		29.74	29 8		
30	9	• •	• •	39.0	51.2	3.5	• •	• •	• •	• • [28 51	1.30	21.25	" 4	36.168	32 19.35	9	.35	29	12.55	28 58	28.7	0
31	8					25.5	38.0	50.4]	29 12	2.93	21.25	" 4	39.656	30 18.83	9	.21		34.18	28 56		
32	9		42.5 5						• •]	32 - 7		21.25	8	38.575	45 38.14		.61		28.69	29 11		
33	9	• •	[2.5]	15.0	27.5				• •	• •	33 27		21.23	il	34.100	33 30.81		.31		48.74	28 59		
34 35	9		•••	• •	16.5		25.0			• •	36 (37 16	L	$21.21 \\ 21.23$	a	40.263 39.410	29 57.89 45 9.35		.73 .45		21.43 37.85	28 56 29 11		
36	7.8						32.2				38 6		21.19	B	38.550	$\begin{vmatrix} 45 & 9.83 \\ 25 & 9.82 \end{vmatrix}$.26		28.11	28 51		
37	9						4.0				38 38	J	21.21	D.	37.390	37 33.64		.17		59.82	29 3		
38	7		1	- 1	28.24	40.8				• •	39 28		21.21	B	43.118	43 1.26		.95		49.51	29 9		
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$\begin{array}{c c} 40 \\ 41 \end{array}$	9		35.24		$\begin{bmatrix} 0.2 \\ \end{bmatrix}$				• •	• •	42 0 42 18		21.18 21.17	N .	40.380 36.330	29 53.89 26 26.28		.39		21.27 39.54	28 56 28 52		
- 1	9		59.0	1			1				19 45 24		21.17	H	42.202	23 3.73		.64		45.19	28 49		
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er.	Magnitude.		SE	CON	IDS	OF	TRA	NSI'	ΓS.		E.				т.		R	ean Righ	- 1	ean S	
Number.	Magn	I.	п.	111.	IV.	ν.	VI.	vII.	10.	11.	Т.	a	•	MICROMETER.	D.	d.		Ascension 1850.0.		eclina 350.0.	
						Zon	e LIII	ί.	Aug	gust 1	З. Н.	$D. \equiv -$	-40°4	9 30.00. n'.=	-23.00.	n". = -	-15.86.				
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3	9						0 41.0		٠.	• •	9 11.8	1	1.96	" 6 38.042	16 48.79	17.	8	9 33.89	1	6 35.	
4 5	8.9						$249.8 \\ 259.0$				11 20.8 14 29.8		1.96 1.92	" 5 41.181 " 5 42.456	$23 \ 45.46$ $23 \ 1.21$	16. 15.	ž.	11 42.81 14 51.73		3 32. 2 47.	
6	7.8						052.2				15 23.6	1	.92	" 4 46.190	26 40.72	15.	g g	15 45.59	i i	6 26.	
7	9						5 57.2				$21\ 28.0$	i i	.88	" 3 43.892	33 59.29	14.	8	21 49.92		3 43.	
8	9	• •	57.0				0 55.0				22 25.75	1	.83	" 6 42.900	$13\ 59.93$	14.	48	22 47.55	41	3 44.	41
9	8						6	٠.	٠.		26 21.10		87	" 1 33.240	54 52.61	13.	1	26 42.97		4 36.	
10	8.9	• •	58.0	12.0	27.0	41	56.0	• •	• •		40 26.9	$3 \mid 21$.69	" 3 36.900	38 2.39	11.	19	40 48.62	2 41 2	7 43.	58
11	9	1					041.4		٠.		48 12.40	- 1	. 63	" 2 41.346	44 16.69		86	48 34.03		3 56.	
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13 14	$\frac{9}{6.7}$		1				$0 \mid \dots \mid 0 \mid 16.6$	• •			$9\ 30.64$ $10\ 47.44$	- }	.41	" 1 39.528 " 3 39.043	51 13.64		42 99	9 52.05		0 50.	
15	7.8						0.58.0				11 28.6		.39	" 1 43.086	36 47.91 49 10.04		22 12	11 8.81 11 50.00	1	6 24. 8 46.	
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						Zon	e LIV	•	Aug	ust 1	3. H.	D.==-	-27 2	5 30 n.'=	- 6.65. ı	ı".=-	1000.				
1	8						1.2				22 2 36.5		.19	IV. 4 44.400	27 38.04	6.	30 22	2 56.74	27 5	3 14.3	33 2
$\begin{vmatrix} 2 \\ 3 \end{vmatrix}$	8 9	1					312.0 314.0		• •	• • [3 47.14	1	.17	" 5 41.130	23 43.80	6.	Ħ	4 7.31		9 19.9	
4	8						153.0				4 49.09 8 28.19		.18	" 2 37.561 " 2 44.242	46 16.08 42 25.33	$\frac{6}{5}$.	B	5 9.20 8 48.35	1	$egin{array}{ccc} 1 & 52.1 \ 8 & 0.8 \end{array}$	
5	9										9 36.60	- 1	.15	" 3 38.550	36 56.58	5. 5.	Ä	9 56.75		231.9	
6	8		36.0	48.2	1.0	13.2	25.8				11 0.87		.14	" 2 43.601	42 47.43	5.	ä	11 21.01		8 22.6	
7	9	٠.					5				$13\ 47.09$	2 20	.12	" 2 40.015	44 51.33	4.	94	14 7.14	1	0 26.2	
8	7.8	l					27.0			• •	16 1.90	- 1	.08	" 7 37.165	11 27.27	4.	N .	16 22.04		7 1.9	
9 10	9 9						52.1			• • [19 27.18 20 40.55	- 1	.08	" 4 35.632	32 40.86	4.	ă ă	19 47.26 21 0.62		8 15.1	
										• •			١,	" 4 40.694	29 46.00	4.	11	21 0.02		5 20.1	
11	7.8]	37.0							• •	21 1.74		.06	" 5 35.830	26 46.85	4.	8	21 21.80	1	2 20.9	
12 13	9	• •					12.0		• •	• •	25 3.70 $25 47.18$.05	" 2 34.650 " 2 40.050	47 56.64 44 50.13	3. 3.	a a	25 23.75 26 7.22		3 30.3 0 23.7	
14	9						49.0	1.5			26 24.04		.04	VI. 1 42.775	49 12.46	3.	H	26 44.08		$\frac{1}{4}$ $\frac{25.7}{46.0}$	
15	9						45.0				27 20.17	1	.01	V. 6 38.165	16 43.72	3.	9	27 40.18		2 17.1	
16		49.0									29 26.32	20	.02	IV. 2 34.950	47 46.30	3.	25	29 46.34	28 13	3 19.5	55 z
17	8		,				8.22		- 1	[29 43.42		.99	" 6 44.160	13 16.68	3.5	Ħ	30 3.41		3 49.9	
18	5.6	• •	• • 4	18.2	1.0	13.0	26.0		• •	• •	22 32 0.89		.98	V. 5 40.835	23 53.94	3.	00 22	32 20.87	27 49	9 26.9	94
					C	CORI	RECTIO	ons.							INSTRU	MENT	READIN	GS.	,		
			cor.		HOURI	1	m.	n		c.	ZENITH	COINC.				CIF	CLE.		BAR.	THE	RMOM
			croc	К	COR	•				•	POINT.	COINU.			Α.	в.	с. п	Mean.	DAK.	At.	Ex
	t 13, at	20h	$^{s.}_{+10.1}$.32	_s. _0.0	12 -	s. $+0.294$	+0.3	300 +	s. 0.230	0° 0′ 2″50	r. 40.106	Zon LIII	e h. .—August 1319.8	3 279° 51′ 1″.8	4.0	7',1 3	6 4.12	ı. 	.°.	۰
ugus		22		. .	· · .	.		1			3.12			20.8	I		.	ŀ	29,992	79.0	76.
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ugus	***************************************							<u> </u>						21.7 —August 1322.0		6.1	8.2 6		29,960	78.5	75.3

er.	tude.		SE	CON	DS (OF :	ΓRA	NSI'	ΓS.						_	-	D		Right		n So	
Number.	Magnitude.	ı.	11.	ш.	ıv.	v.	vi.	vII.	10.	11.	Т.	a.		MICROMETER.	D.	d.		Asce 1850	nsion, .0.	Dec 185	elinati 0.0.	on,
						Zo.	ne L	v.	Au	gust 18	в. м.	D. = -	-27	55 10"0. n.	-42.00. n.	5.14						
1 2 3	9 9					 30 . :	 542.8			35.5 47.0	h. m. s. 18 29 26.85 31 17.98 31 38.78	19.	.37 .37	r. 11. 5 43.6 VII. 4 44.59 11. 7 40.13	$ \begin{vmatrix} -22 & 13 & 40 \\ 27 & 26 & 20 \\ 9 & 38 & 68 \end{vmatrix} $	39 ^{''} . 39.	56	31	37.35 58.12	28° 18' 28° 23 28° 5	15.7	6
4 5 6 7 8	9 9 8 8.9 8.9			21.2	50.3 34.0 12.6	2.9	59.0		18.3	31.0	33 31.69 35 22.33 37 50.32 40 33.92 43 12.65	19. 19. 19.	.34 .34 .36	VII. 3 33.83 11. 5 36.48 I. 4 39.47 2. 1 39.84 I. 5 41.45	39 34.53 26 18.43 30 23.14 50 43.54 23 27.50	39. 38. 38. 37.	70 18 60	$\frac{35}{38}$	51.06 41.67 9.66 53.28 31.95	28 35 28 22 28 26 28 46 28 19	7.1 11.3 31.1	3 2 4
9 10 11	10 9 9	55.7	 55.7	21.0 8.4	33.5 · · 21.0	46.0 33.3	3 46.0		9.5	 221.9	45 33.52 46 13.28 49 20.93	19 . 3 19 . 3 19 .	.33 .28 .31	VI. 1 44.40 11. 5 42.05 VI. 1 38.28 10. 6 33.45	48 6.65 23 5.99 51 38.10	36. 36. 35.	55 41 75	45 46 49	52.85 32.56 40.24	28 43 28 18 28 47	53.2 52.4 23.8	0 0 5
12 13 14 15 16 17	9 9 9 9 9 6.7	13.3	 26.0	14.3 38.0	26.8 49.2	50.8	3.5	5 15.	9	18.0	50 15.16 19 1 26.94 3 38.49 9 9.23 13 50.89 14 49.41	19 19 19 19 19 19 19 19 19 19 19 19 19 1	.25 .19 .17	10. 6 33.45 V. 1 39.93 " 4 44.37 11. 3 43.302 IV. 1 43.44 1. 6 43.83	19 20.92 50 41.13 27 34.16 34 6.56 48 39.93 13 22.74	35. 33. 32. 31. 30.	22 77 63 69	19 1 3 9 14	34.41 46.19 57.68 28.40 10.06 8.51	28 15 28 46 28 23 28 29 28 44 28 9	24.3 16.9 48.1 20.6	5 z 3 9 z 3
18 19 20 21	9 8.9 9		5.4	10.0	30.5 22.5 	34.8	3			 8 41.6	21 30.46 22 22.50 22 32.78 24 51.55	19 19	.10	" 2 43.27 IV. 3 40.43 11. 2 38.66 " 5 38.47	42 53.83 35 46.88 45 33.29 25 10.69	29. 28. 28. 28.	98 95	22 22	49.57 41.60 51.89 10.61	28 38 28 31 28 41 28 20	$25.8 \\ 12.2$	86 z
22 23 24 25 26	8 9.10 9 9	13.6 39.5	26.3 51.9	38.5 4.2	12.1 17.0 49.3	29.0	1.9 51.8	3 4.	6		31 11.76 36 51.01 38 16.84 40 26.91 41 49.41	18 18 19		VII. 7 45.63 VI. 7 42.19 VII. 7 39.29 " 1 39.16 VI. 5 36.51	6 29.48 8 28.53 10 8.47 51 7.44 26 18.39	27. 26. 25. 25. 25.	14 87 45	37 38 40	20.75 9.97 35.80 45.92 8.37	28 4		7 84 89
27 28 29 30	9 8.9 9					21 45	233.	11.	0		43 43 43 43 43 43 43 43 43 43 43 43 43 4	18 1 18 2 18	.97 .89	VII. 3 40.49 2. 4 42.11 11. 2 46.37 IV. 6 42.37	35 44.47 28 51.53 41 6.98 14 13.40	24. 23. 23. 22.	94 17 17	43 52 52	27.66 51.33 52.43 12.32	28 31 28 24 28 36 28 9	19.4 24.7 40.1	1 '0 z .5
31 32 33 34	8 8.9 9 9			20.8	33.0	45.	0 13.3	0 42. 5 26.	8 0		56 45.08 57 5.09 59 33.17 20 0 48.58	18 7 18 8 18	.90 .84 .84	10. 6 35.12 I. 1 37.31 2. 5 34.53 IV. 5 33.89 11. 7 35.37	18 23.21 52 11.38 27 26.13 27 48.99 12 23.14	22. 22. 21. 21.	34 88 66	57 59 20 1	3.92 23.99 52.01 7.42 53.39	28 13 28 47 28 22 28 23 28 7	$\begin{array}{c} 43.7 \\ 58.0 \\ 20.6 \end{array}$	2 : 1 55
35 36 37 38 39						40.	8 53.0 5	$\begin{bmatrix} 0 & \dots & \vdots \\ 0 & 5 & \vdots \\ \vdots & \ddots & \vdots \end{bmatrix}$	7 14.	7	0 34.58 6 9.08 6 18.70 8 28.20 10 43.00	5 18 0 18 0 18 6 18	.81 .82 .80 .76	I. 3 39.50 11. 2 41.33 10. 3 33.10 VII.5 42.96	36 18.60 44 0.16 39 59.38 22 35.30	20. 20. 20. 19.	71 69 30 87	6 6 8 11	27.86 37.52 47.00 1.82	28 31 28 39 28 35 28 18	49.3 30.8 29.6 5.1	35 38 7
40 41							• •	- 1		7 58.1	14 38.91 20 14 49.51		.70 .75	II. 7 44.65 11. 3 45.13	7 3.51 33 3.39	19. 19.	9		57.61 8.26	28 28		
		-				COR	RECT	TION	s. 		1				INSTR			OINGS				
		7.12000		. то	HOU!		m.		n.	с.	ZENITH POINT.	COINC.			Α.	в.	C.	р.	Mean.	BAR.	At.	Ex
Augu	st 18, a	t 20h.	+7	s. .943	s 0.	017	$^{s.}_{+0.29}$	94 +	s.) .300	+0.230	o° o′ 1″.75	r. 40.110	Zo	one LV.—Aug. 18,	h. 18.5 292° 42′ 41″.0 19.3 20.0 20.2 37.5 21.0 36.5	39.2	46.7 42.2 41.3	43.7 40.2 39.3	43.85 39.72 38.80	30.118 30.130 	74.3	1

er.	itude.		SECO	NDS OI	TRAI	NSITS.		m.			D		Mean	0	į.	n So	
Number	Magnitude.	ı.	п. п	ı. ıv.	v. vi.	vII. 10	. 11.	т.	a.	MICROMETER.	D.	d.	1850	ension, .0.	1850	linati 0.0.	
				Zone LV	7. A	ugust 1	8. 1	D = -	-27 55	10.0. n. —42.0	0. n". —5."14	. (Con	ntinued.)				
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43	9		1 1	1 (36.4		21 59.05	18.	N N	19 28.21	17.93	ı	17.72	28 14		
44 45	8	• •	1 1	$.233.045 \ .013.525$	1 1	• • • •		30 32.87	18. 18.	1	19 1.20 11 18.15	$\begin{array}{c} 16.44 \\ 16.32 \end{array}$	8	$\frac{51.48}{32.07}$	28 14 28 6		
46	8				35.0	$egin{array}{c c} \cdot & \cdot & \cdot & \cdot \\ 17.3 & \cdot & \cdot \end{array}$		31 13.48 32 9.90	18.	8	35 54.47	16.15	H	28.53	28 31		
47	8		7.6 20	.0 32.5 .	1 1		1 1	34 32.51	18.	61 2. 4 37.41	31 33.91	15.74	t .	51.12	28 26	59.6	i5
48	8			.3 11.5 .				35 11.65	18.	2	49 4.65	15.63	9	30.28	28 44		
49	8 8		1 1	.0 56.5	, ,	• • • •	1 1	37 56.48	18.	i i	13 25.40 22,25.53	$\begin{array}{c} 15.15 \\ 15.04 \end{array}$	B .	$15.03 \\ 50.64$	28 8 28 17		
50 51	9.10		19	.7 32.0 44	.031.7	- 1		38 32.08 41 6.65	18. 18.	Ħ	38 20.49	14.60	B	25.23	28 33		
52	9.10					56.0		41 18.55	18.		36 20.05	14.57		37.11	28 31		
53	8			1 1		53.2 11.		41 15.76	18.	1	37 39.78	14.58	i i	34.33	28 33		
54	9				. 24.6			43 59.54	18.	8	39 43.49	14.12	9	18.09	28 35		
55	8				1 1	56.5		$45\ 18.74$	18.	i i	36 50.05	13.90	B	37.27	28 32		
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57 58 :	$\begin{vmatrix} 9 \\ 9 \end{vmatrix}$. 23.0 .	1 1	13.0	1 1	48 22.99 52 5.63	18. 18.	8	23 15.60 22 0.72	$13.38 \\ 12.79$	8	24.09	28 17		
59	8				. 42.0			52 16.94	18.	ů .	27 47.30	12.76	8	35.41	28 23		
60	7		30.0 42	.2		32.0	1 1	$53\ 54.74$	18.	8	23 35.37	12.51	i i	13.19	28 18		
61	1 1	27.0	40.0		.0 30.0		1 2	21 3 4.81	18.	9	35 29.55	11.11	8	23.21	28 30		
62	6		• • •	. 5.0 17	.1 29.6	11.1	• •	4 4.55	18.	37 VII. 6 35.23	18 19.81	10.96	4	22.92	28 13	40.7	1 2
				:	Zone LV	TI.	Lugust	29. M.	D = 4	1 19 50.0. n.	==35.39. n.	== 13.00.					
1	9			. 12.0 26	4 .	56.0		18 31 11.81	20.	74 10. 2 45.45	41 50.63	32.83	18 31	32.55	42 2	13.4	
2	9		10.725				1 1	33 40.04	20.	8	10 50.81	32.29	A	0.69	41 31		
3	9			1 1		25.5		33 41.39	20.	68 10. 5 42.50	22 55.37	32.29	34	2.07	41 43	17.6	6
4	9.10			i	. 24.5			34 54.94	20.	8	25 18.34	32.01	B	15.62	41 45		
5 6	$8.9 \\ 9.10$	• •	96 0 41	.0 55.5 10	1 1	1	0 40.0	35 18.71 37 55.42	20. 20.		43 37.09 9 22.11	$31.92 \\ 31.34$		$39.42 \\ 16.04$	$\begin{vmatrix} 42 & 3 \\ 41 & 29 \end{vmatrix}$		
7	1 1	1	57.012	1 1			1	40 26.41	20.		21 13.83	30.79	1	47.04	41 41		
8	8		1	. 14.8 29	1 1	- 1		41 14.78		65 VII.3 46.63	32 20.71	30.61		35.43	41 52		
	10			.6 49.0 3				47 48.68		59 2. 5 37.86	25 36.61	29.17	8	9.27	1		
10	8.7	27.2	41.7 56	.8 11.0 .	. 41.0	55.5 .		51 11.36	20.	61 2. 2 37.14	46 39.80	28.43	51	31.97	42 6	58.2	3
11	8			.1 51.5 6				55 51.62	20.		25 25.51	27.35	8	12.16	41 45		
	$\begin{vmatrix} 10 \\ 7 \end{vmatrix}$		1	.2	1	10 0	1 1	58 21.93	20. 20.	8	44 39.25 47 14.33	$26.88 \\ 26.74$	1	42.49 22.93	42 4 42 7		
13 14	$\begin{vmatrix} 7 \\ 10 \end{vmatrix}$	• •	1 1	. 2.4 17 . 35.0 49	1 1	1		59 2.38 19 5 34.95	20.		31 9.49	25.74 25.34	ě	55.41	42 7		
15				$.2 \begin{array}{ c c c c c c c c c c c c c c c c c c c$			1 8	8 9.81	20.		13 59.71	24.79	ŭ	30.21	41 34		
16	9		38.0 52	.3				24 - 7.06	20.	2	8 13.68	21.46	9 .	27.32	41 28		
17	7.8		· · ·	. 12	2.0 27.0 4	41.5		19 24 37.66	20.	25 10. 7 45.84	6 19.64	21.28	19 25	17.91	41 26	30.9	2
				CO	RRECTI	ons.					INSTRU	JMENT RI	EADING.				
			COR. TO	HOURLY				ZENITH				CIRCLE	: .			THER	RMO:
			CLOCK.	cor.	m.	n.	c.	POINT.	COINC		Δ.	в. с.	. р.	Mean.	BAR.	At.	E
	00 st 01	1 <i>h</i>	s. +7.93	s. +0.010	s. +0.273	s. +0.347	s. +0.230	o° o′ 2″.51	7. 40.107	Zone LVI.—Aug. 29	h. 18.5 279° 21′ 6″.8	9.1 9.	0 9'.0	8.48	1. 30.072	76.5	75
1g. 5	20, 111 22		<u> </u>				<u> </u>				19.0	.		• . •		76.2	
ug. 5																CO F	1 77/
ug. 5											19.3			4	30.070	76.5 76.0	1
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Number.		1	ЮĽ	CON	IDS C)F '.	Γ RAI	ISI	rs.				er control				Mear	n Right	Mea	an Sc	outh
	Magnitude.	ı.	II.	III.	IV.	ν.	VI.	VII.	10.	11.	Т.	a.		MICROMETER.	D.	d.	ii .	cension,	İ	eclinat 50.0.	ion,
				Z	Zone I	LVI.	. A	Lugu	st 29		$\mathbf{M.} D. = 4$	1 19 50	ő.o.	n'. ==35.39.	n".==13.00	. (C	ontinued	,)			
18	8.9			39.5	54.0	9.0					h. m. s. 19 26 54.25	s. +20.		VI. 4 45.65	-26 55".82	-20".8	h.	m. s. 7 14.52	41° 4	7 6".7	71
19	8						54.2				27 24.71	20.	- 8	VII. 1 45.32	47 49.96	20.7	7	745.03		8 0.7	
20	9						15.0				28 45.80	20.	N N	" 6 48.5	10•41.29	20.5	9	9 6.02	1	0 51.8	
21	9						23.5				29 53.77	20.	8	" 1 45.16	47 55.48	20.2	Н	0 14.06	1	8 5.7	
22	9				[32.8	48.0	2.6			32 18.39	20.	.23	" 4 43.56	28 8.42	19.7	0	2 38.62	1	3 18.2	
23	8	59.7	14.5	29.0	44.0	58.0	13.5	28.2			34 43.86	20.	.22	IV. 3 37.82	37 27.92	19.2	9 3	5 4.08		7 37.2	
24	9.10	١	43.5		13.0		42.6				37 12.97	20.	.18	VII. 5 34.50	27 33.99	18.7	9 3	7 33.15		7 42.7	
25	8			42.0	56.51	11.3	26.3	41.0			39 56.65	20.	.21	III. 1 35.14	$53\ 44.82$	18.2	N	0 16.86		3 53.0	96 в.
*26	5				4	48.7	3.5	18.1		[44 33.85	20.	16	VI. 1 32.33	$55\ 22.57$	17.3	8	4 54.01	1	5 29.9	
27	9			59.5	5	29.0					48 14.39	20.	04	V. 7 34.95	12 39.43	16.6	8	8 34.43	i	2 46.0	
28	9.10						59.5	- 1			49 29.69	20.	00								
29	9.10						34.0		• •	• •	49 29.69 52 4.48	$\frac{20}{20}$.		VII.3 34.46 " 4 41.13	39 24.52 29 33.16	16.3	H	9 49.77	1	30.8	
30	8		1 1	¥9.J	1 1		9.0	· · · · · · · · · · · · · · · · · · ·			56 39.53	$\frac{20}{20}$.	9	VI. 1 34.85	29 33.16 53 54.65	$15.8 \\ 15.0$	H	$2 24.52 \\ 6 59.57$		9 39.0 9 50 6	
31	8.9				1 1		3.0			9	57 52.69	20.		11. 1 38.41	51 49.58	13.0 14.7	į.	6 59.57 8 12.71		3 59.6 1 54.3	
32	9		1 1	- 1	1 1		15.7	1			20 0 46.45	19.	i i	VII. 6 41.39	14 48.50	14.2	3	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	i		
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34	8						26.0				13 56.42	19.		VII. 1 43.69	48 46.51	11.8	i i	$4\ 16.26$	1	3 48.3	
35											16 24.13	19.		V. 7 41.53	8 50.81	11.4	g .	6 43.87		552.2	
36			1		10.72		1 1				19 10.62	19.	H	VI. 3 44.54	33 33.73	10.9	R	$9 \ 30.37$	i	34.6	
37	9				1		49.2				21 19.88	19.		VII. 4 40.51	29 54.85	10.50	N	1 39.60		55.4	
				1									1								
38	7.8		1 6	- 1	0.5		1		• •	• • [23 0.56	19.	R	VI. 2 46.42	41 17.79	10.28	19	$3\ 20.24$	3	1 18.0	
39	8.9	• •					!		• •	• •	23 9.66	19.	8	VII. 7 45.78	6 22.33	10.2	N .	3 29.32		522.5	
40							52.8		• •	• •	27 23.19	19.	9	I. 5 39.61	$24 \ 36.25$	9.59	8	7 42.83	1	4 35.7	
41		52.8			36.5				• •	• •	29 36.66	19.	8	VI. 7 40.15	9 38.50	9.1.	¥	9 56.25	1	37.6	
42	9	•••					26.54	- 1	• •	• •	34 57.88	19.		2. 4 40.39	29 58.37	8.28	R	5 17.45		56.6	
43			1	1	1		l		1	• •	36 4.55	19.	8	VI. 2 40.65	44 38.39	8.1	i i	6 24.13	i	4 36.4	
44	8.	٠.					58.21 53.0			• •	41 29.05	19.	R	VII. 7 43.34	7 47.32	7.2	8	1 48.50	1	7 44.5	
45	8.9	• •								• •	43 23.52	19.	ā	" 5 50.80	18 7.08	6.9	8	3 42.96	1	3 4.0	
$\begin{vmatrix} 46 \\ 47 \end{vmatrix}$	$9.10 \\ 8.9$				14.0^{2}			- 1		• •	47 13.94	19.		VI. 6 33.69	19 16.38	6.3	ii .	7 33.34		12.7	
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2	9		44.0	59.0		28.0	43.1				19 6 13.55	16.	52	V. 6 45.530	12 25.86	34.10	A .	6 30.07		9.9	
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			Zone	e LVII.	Sep	tembo	er 9.	н. р.=-	40° 51′ 1	1ο້.°0.	n'. == -40'.0	0. n".=-	15.06.	(Contin	nued.)			
4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 40 41 41 41 41 41 41 41 41 41 41 41 41 41	7.8 9 8 8.9 9 9 9 9 9 9 9 9 9 9 9 9 9	16.00	28.5 43.2 0.8 15.2 . 48.0 59.0 13.2 28.0 42.1 13.0 45.1 31.0 45.1 31.0 45.1 31.0 45.1 31.0 45.1 31.0 45.1 31.0 45.1 31.0 45.1 31.0 42.0 57.2 12.1 36.0 13.2 28.2 37.0 42.0 57.2 12.1 36.0 32.3 31.8 0.3 2.5 50.0 42.0 56.1 44.0 58.0 44.0 56.0 44.0 56.0 44.0 56.0 45.0 55.0 12.1 26.5 55.0 12.1 26.5 55.0 12.1 26.5 55.0 12.1 26.5 55.0 12.1 26.5 55.0 12.1 26.5 55.0 12.1 26.5 55.0 12.1 26.5 55.0 12.1 26.5 55.0 12.1 26.5 55.0 12.1 26.5 55.0 12.1 26.5 56.8 11.0 0.2 15.0	0 37.5		 27.4 		h. m. s. 19 11 20.85 16 38.10 16 42.91 18 0.90 20 58.37 24 30.55 26 2.45 27 28.22 29 57.35 33 47.32 40 0.55 40 46.32 44 37.25 48 33.41 50 27.06 50 5 47.17 11 59.27 13 35.17 13 59.84 15 14.22 23 4.41 24 32.84 31 5.11 22 0 11.31 5 12.80 6 18.84 7 9.29 11 41.38 15 26.20 15 29.92 15 40.12 17 49.44 22 17.64 24 57.54	6 +16 16 16 16 16 16 16 16 16 16	s	TV. 4 46.113 " 2 42.522 VII. 4 47.061 IV. 3 43.459 " 1 35.288 " 3 34.265 " 2 40.388 V. 6 36.940 IV. 6 36.743 " 7 44.728 " 3 40.556 " 5 42.068 " 3 38.053 " 5 39.212 V. 5 42.172 II. 5 47.200 V. 2 41.851 IV. 1 37.698 " 5 41.755 " 5 45.360 " 5 26.818 " 7 47.598 " 3 32.460 " 5 37.553 VI. 6 35.310 IV. 2 45.350 " 7 38.093 " 3 34.800 " 2 32.850 " 7 44.647 " 6 40.840 " 6 40.676 " 4 36.910 II. 5 46.395 III. 5 44.940 V. 5 45.050 IV. 6 35.290 " 6 43.970 " 5 44.513 VI. 3 33.749 IV. 6 46.144	-26 43'.18 43 36.25 26 8.58 34 14.18 53 43.25 39 34.39 44 50.95 17 24.74 17 31.61 6 59.83 35 54.98 23 13.00 37 22.36 24 52.51 23 9.33 20 14.05 43 59.69 52 19.08 23 23.78 21 18.42 32 4.08 5 19.87 40 37.34 25 50.06 18 21.44 41 57.98 10 50.94 39 15.58 49 13.48 7 2.63 15 8.99 15 14.64 32 2.67 20 42.16 21 32.86 21 29.06 18 22.37 13 20.04 21 47.64 39 51.94 12 4.42	- 32.98 31.84 31.82 31.54 30.90 30.17 29.84 29.54 29.02 28.23 27.42 26.94 26.79 26.01 25.22 24.84 23.79 23.62 23.58 23.09 21.90 20.76 20.46 20.39 20.16 18.76 18.51 17.39 5.78 5.78 5.78 5.78 5.78 5.79 5.79 5.80 5.81 5.91 6.05 6.51	19 1 1 1 1 1 1 2 2 2 3 3 3 2 2 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	m. s. 1 37.36 6 54.59 6 59.36 8 17.36 1 14.84 4 46.99 6 18.85 7 44.61 0 13.65 4 3.55 7 55.83 0 16.73 1 2.54 4 53.40 1 2.54 1 3.02 2 15.11 3 50.96 4 15.62 5 30.02 3 20.06 4 18.52 1 20.72 0 25.56 6 26.94 6 3 2.98 7 23.43 1 55.44 6 40.19 6 43.91 6 54.10 8 3 2.98 7 23.43 1 55.44 6 40.19 6 43.91 6 54.10 6 3 3.98	42 34 42 44 42 36 42 42 42 44 42 16 42 16 42 17 42 17 42 18 42 11 42 11 42 11 42 12 41 55 42 31 42 11 42 12 41 55 42 31 42 11 42 22 41 55 42 31 42 11 42 22 42 33 41 55 42 31 42 12 42	7 26.1 18.0 18.0 18.0 18.0 18.0 18.0 18.0 18	09 40 72 15 56 67 98 83 36 60 10 14 15 15 15 16 16 17 17 17 18 18 18 19 19 19 19 19 19 19 19 19 19
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er.	Magnitude.		SE	CON	DS (OF :	rrai	risi	rs.		Т.		-		D.	d.	8	an Right		n South
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			1			COR	RECTI	ons	•		1 1				INSTRU	MENT	READIN	GS.		
			cor.	1	HOUF		m.	2	n.	c.	ZENITH POINT.	coinc.			Α.	CIRC		o. Mean.	BAR.	At. Ex
Sept.	13, at	22h	+3	.439	s. 0.	020	s. _0.356	+0.	.527	s. +0,022	0° 0′ 2′.61	r. 40.110	Z L	None h. VIII.—Sept. 13, 20.2 20.6 20.7 21.5 22.0 22.6 0.5	291°42′50″.2 46.7 45.6	55"0	57".4 51. 	".0 53".40 . 49.90 	1. 30.040 	78°.1 74° 73 73 72 73. 75.3 72.

. -	tude.		SECO	NDS	OF TR	ANSI	TS.							Mean Right	Mean Sou
Tammar.	Magnitude.	I.	II. III	. Iv.	v. v	ı. vii.	10.	11.	Т.	a.	MICROMETER.	D.	d.	Ascension, 1850.0.	Declinatio 1850.0
			Zoi	ne LV	III.	Septe	mber	13.	M. D.=	—28 54 5	0	34.00. n.'=	-3.26.	(Continued.)	
1 8			16	5 50 C	12.025	027 6			h. m. s.	8.	r.	of 00"00	· · · ·	h. m. s.	. 0 / //
$\frac{1}{82} \frac{1}{8}$			0.022.			. 12.9		• •	$\begin{array}{c} 21 \ 27 \ 59.52 \\ 36 \ 34.70 \end{array}$	+12.80 12.72	I. 5 44.77 " 4 40.22	-21 30 ["] .88	-17.74	21 28 12.32	29 16 38.62
$\begin{bmatrix} 2 \\ 3 \end{bmatrix} \begin{bmatrix} 2 \\ 9 \end{bmatrix}$	- 1				11.023				39 58.16	12.66	" 6 39.81	29 55.33 15 39.69	16.52 16.04	36 47.42 40 10.82	29 25 1.85 29 10 45.73
4 10)				59.0 .				43 46.47	12.66	VI. 3 32.15	40 30.94	15.55	43 59.13	29 35 36.49
5 8	3				58.5 10	.9 23.7	7		44 45.87	12.62	VII.5 35.76	26 42.14	15.42	44 58.49	29 21 47.56
6 10	1	• •	• • • •	1 1	1 1			50.3	$45 \ 41.12$	12.63	11. 3.37.62	37 20.94	15.30	45 53.75	29 32 26.24
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8 8	- 1		3.826.						50 38.92	12.60	2. 1 39.08	51 7.92	14.66	50 51.52	29 46 12.58
$\begin{bmatrix} 9 & 7 \\ 0 & 7 \end{bmatrix}$	ł			1 1	9.5 22	1	1		50 56.94	12.56	VII.5 38.96	24 51.61	14.62	51 9.50	29 19 56.23
		1	• • • •			.	55.8	8.3	52 59.27	12.52	11. 6 40.63	15 10.58	14.38	53 11.79	29 10 14.96
1			5.5 37.	1 1	00 -	- 1			53 50.64	12.51	1. 6 41.86	14 28.87	14.28	54 - 3.15	29 9 33.15
$\frac{2}{2} \mid \frac{8}{2}$. 1		0.5 13.		i I		$ \cdot\cdot $	• • •	57 25.68	12.49	2. 4 38.64	30 49.49	13.84	57 38.17	29 25 53.33
$egin{array}{c c} 3 & 8 \\ 4 & 7 \end{array}$			8.8 1.			.0 1.8			57 23.79	12.53	VII.1 36.17	52 48.85	13.84	57 36.32	29 47 52.69
- 1	- 0				8.121			• • •	$\begin{array}{cccc} 22 & 1 & 13.47 \\ & 12 & 55.63 \end{array}$	12.42	IV. 7 45.62 2. 3 39.14	6 28.32	13.39	22 1 25.89	29 1 31.71
6 9					44.2 57				15 31.75	12.34 12.30	2. 3 39.14 I. 4 38.79	36 28.82 30 44.70	$12.10 \\ 11.86$	$\begin{array}{cc} 13 & 7.97 \\ 15 & 44.05 \end{array}$	29 31 30.92 29 25 46.56
7 9	.10	- 1			27.440				17 14.88	12.29	VI. 3 44.01	33 41.20	11.69	17 27.17	29 28 42.89
8 7		9.82			59.8 12				20 47.44	12.24	I. 4 39.40	30 23.67	11.36	20 59.68	29 25 25.03
$9 \mid 9$	- 1	1		1 1		1	42.5	55.0	20 45.73	12.25	11. 3 42.99	34 15.44	11.36	20 57.98	29 29 16.80
$0 \mid 8$.9	5	7.6 10.4	4 23.5	35.5 48	.0 0.6			24 22.99	12.23	VII. 1 40.88	50 6.09	11.03	$24 \ 35.22$	29 45 7.12
1 9			. 56.	5 9.1	21.7 34	.246.6		o constant	27 9 08	12.16	2. 5 47.56	19 54.10	10.78	27 21.24	29 14 54.88
2 7	- 1				24.0 .				30 11.25	12.15	" 3 39.80	36 6.01	10.51	30 23.40	29 31 6.52
3 7	- 1		5.0 57.3	2 10.3	• • •				31 10.03	12.10	IV. 7 37.47	11 9.84	10.43	31 22.13	29 6 10.27
- 1	1			1 1		1	8.8	21.3	31 12.33	12.10	11. 7 35.90	12 2.94	10.43	$31\ 24.43$	29 7 3.37
$ \begin{array}{c c} 5 & 9 \\ 6 & 10 \end{array} $		0.61	3.5 26.0		45.5 58.			• •	34 38.58	12.09	VI. 4 40.26	29 54.19	10.17	34 50.67	29 24 54.36
1		3	$\begin{bmatrix} \cdot & \cdot & \cdot \\ \cdot & 0 & 47 \end{bmatrix}$		12.125			• • •	$35 \ 32.95$ $44 \ 59.62$	12.11 11.96	VII.1 44.88 " 6 36.23	47 47.90	10.10	35 45.06	29 42 48.00
8 9					14.427.				48 1.96	11.95	2. 4 41.36	17 43.40 29 15.57	$9.46 \\ 9.27$	45 11.58 48 13.91	29 12 42.86 29 24 14.84
9 10		1	1		27.5 .	- 1			50 14.94	11.90	VII. 7 37.17	11 19.84	9.14	50 26.84	29 24 14.84 29 6 18.98
0 7	1	7.430	0.1 42.8	3	7.7 20.	633.0			52 55.33	11.92	2. 2 40.50	44 27.26	8.97	53 7.25	29 39 26.23
1 9		8.02	0.6 32.9	45.3	57.8 10.	4			53 45.37	11.84	VII. 7 43.54	7 39.75	8.81	53 57.21	29 2 38.56
2 7	2	23.636	6.1 48.3	3 1.2	13.4 26.	7 39.1			23 0 1.25	11.84	2. 2 43.105	42 57.23	8.56	23 0 13.09	29 37 55.79
3 8		29	2.7 35.9	2 47.9	0.5				1 47.95	11.83	VI. 1 40.21	50 29.51	8.48	1 59.78	29 45 27.99
1 9	0		i		•• •		.)	1	3 11.80	11.78	11. 6 33.19	19 27.64	8.42	3 23.58	29 14 26.06
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			5.347.4		27.7 40.		• •	• •	5 0.26	11.76	V. 6 34.50	18 43.41	8.34	5 12.02	29 13 41.75
- 1	0	i	. 11.0	23.5	$\frac{27.740}{36.2}$.	. 55.0	: :		$\begin{bmatrix} 6 & 15.33 \\ 8 & 23.63 \end{bmatrix}$	11.75	" 5 44.99 IV 3 41.61	21 23.61	8.29	6 27.08	29 16 21.90
3 7	- 1	- 1			18.				8 52.80	11.75 11.72	IV. 3 41.61 VII. 5 47.30	$\begin{bmatrix} 35 & 4.18 \\ 20 & 3.50 \end{bmatrix}$	$8.19 \\ 8.17$	$egin{array}{ccc} 8.35.38 & & & & & & & & & & & & & & & & & & $	29 30 2 37
9	- 1	1			26.5 .				10 14.07	11.71	V. 5 42.79	20 3.50	8.11	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	29 15 1 67 29 17 37.70
7		$\cdot \cdot \cdot$	- 1		13.		1 1		10 48.26	11.70	VII. 6 36.59	17 30.91	8.09	10 59.96	29 12 29.00
1 8.	.9 3	7.4 50	.5 3.6	15.3		.			15 15.51	11.68	2. 3 42.53	34 31.68	7.94	15 27.19	29 29 29.62
9		.			43.0 55.	8 8.1			16 30.46	11.65	VII. 4 41.25	29 19.75	7.90	16 42.11	29 24 17.65
8		$\cdot \cdot \cdot$. 44.5	57.0	8.8 22.	034.7		[20 56.91	11.59	" 7 38.94	10 18.68	7.76	21 8.50	29 5 16.44
10	- 1				• • • •				27 14.78	11.55	2. 3 34.77	38 59.77	7.63	27 26.33	29 33 57.40
5 10	1				• • • •				27 27.94	11.56	11. 2 37.55	46 8.81	7.62	27 39.50	29 41 6.43
5 10 7 8			32.0		32.5 45.				30 44.72	11.49	V. 7 37.95	10 53.19	7.56	30 56.21	29 5 50.75
8 9	4	19).5	44.5	57.045.	0 25 5			$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$11.48 \\ 11.37$	VII. 6 37.95 2. 6 40.01	16 43.95	7.55	32 31.60	19 11 41.50
9	1	7.630	.5 43.0	55.5	8.020.	0			42 44.01	11.35	VII. 6 41.47	$\begin{array}{c c} 15 & 32.40 \\ 14 & 42.38 \end{array}$	$7.48 \\ 7.48$	$42 55.98 \begin{vmatrix} 45 & 6.77 \end{vmatrix}$	29 10 29.88
7		- 1	1	1 1			24.5		53 27.76	11.29	11. 3 35.40	38 37.67	7.53	53 39.05	29 9 39.86 29 33 35.20
1 8				44.3	57.0 9.	1			55 44.35	11.25	VI. 6 31.89	20 13.54	7.56	55 55.60	
2 7.	.	1		1 1		1	55.8	3	56 59.42	11.23	11. 6 34.37	18 46.89	7.57	57 10.66	29 15 11.10 29 13 44.46
3 7					34.7 47.				0 13 21.93	11.10	V. 1 34.55	53 45.17	7.96	0 13 33.03	29 48 43.13
1				l l		1	<u> </u>	NAME OF TAXABLE PARTY.							

Number.	Magnitude.	ı.	SECO	NDS OF		NSITS.		Т.	a	•	MICROMETER.	D.	d.		Right ension,	De	un So clinati 50.0.	
			Zone	e LVIII.	Sep	tember	13.	M. D. ==	—2 8 5 4	á 5ő.	0. n'. == -34.0	00. n". == -	−3 .26.	(Conti	nued.)			
84 85 86 87 88 89 90	9 9 7.8 8 9 8.9 8.9	17.5		$.8\begin{vmatrix} 15.0 \\ 49.5 \\ 2 \\ 53$.0	18.9 . 41.5 . 33.1 .		h. m. s. 0 15 55.79 18 15.13 18 49.52 19 41.30 21 3.60 24 55.35 26 52.49 0 28 56.95	+11 11 11 11 11 10 10	s. .07 .05 .05 .04 .03 .99 .97	V. 3 42.34 III. 7 37.21 VII. 6 32.982 " 7 40.40 " 1 43.15 " 3 33.64 " 2 37.37 " 2 38.23	-34 38".98 11 18.76 19 35.58 9 28.27 48 47.69 39 39.25 46 15.78 45 46.05	-8.06 8.15 8.17 8.21 8.27 8.46 8.55 8.65	0 16 18 19	52.34 14.63 6 6.34 7 3.46	29 6 29 14 29 4 29 43 29 34 29 41	37.0 37.0 316.9 433.7 426.4 345.9 437.7 14.3 044.7	1 z'. 5 z. 8 z. 6 z. 1 z. 3 z.
				${f Z}$ one	LIX.	Sept	ember l	14. H.	D.=-	-40°	19 20.0. n'.=	— 2659.	n".=-11.	00.				
1 2 3 4 4 5 6 6 7 8 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24	8 8.9 9 9 8.9 9 8 8 9 9 8 8 9 7 7 8 8 9 7		46.2 . 44.8 59 57.2 11 41.2 . 9.5 23 46.0	. 41.5 56 .0 4.5 . .2 11.2 26 .2 30.0 44 .2 31.0 . .1 46.5 1 .27.0 41 .0 10.0 . .5 15.0 29	$\begin{array}{c} .0\ 43\ .3\\ .0\ 43\ .0\\ .0\ 55\ .2\\ .2\ 39\ .1\\ .0\ \ 7\ .0\\ .5\ 44\ .2\\ .0\ .\\ .0\ .\\ .0\ 10\ .8\\ .\\ .33\ .5\\ .\\ .5\ .\\ .5\ .\\ .5\ .\\ .5\ .\\ .5\ .\\ .5\ .\\ .0\ 59\ .5\\ .\\ .0\ 59\ .5\\ .\\ .0\ 59\ .5\\ .\\ .0\ 59\ .5\\ .\\ .0\ 59\ .5\\ .\\ .0\ 59\ .5\\ .\\ .0\ 59\ .5\\ .\\ .0\ 59\ .5\\ .\\ .0\ 59\ .5\\ .\\ .0\ 59\ .5\\ .\\ .0\ 59\ .5\\ .\\ .0\ 59\ .5\\ .\\ .0\ 59\ .5\\ .\\ .0\ 59\ .5\\ .\\ .0\ 59\ .5\\ .\\ .0\ 59\ .5\\ .\\ .0\ 59\ .\\ .0\ .$.	25.0		19 2 30.53 4 14.54 13 13.67 17 26.33 20 10.00 37 38.01 41 15.05 42 51.78 43 41.69 45 4.47 48 11.74 49 30.17 50 30.51 57 46.70 58 26.94 20 5 10.39 6 15.06 6 17.70 7 30.45 9 19.34 11 28.32 14 37.58 16 30.18 20 23 33.16	14 14 14 14 14 14 14 14 14 14 14 14 14 1	.03 .96 .91 .90 .83 .62 .64 .58 .55 .58 .41 .44 .29 .29 .32 .28 .30 .29 .25 .19	IV. 3 34.431 " 6 38.333 " 3 44.092 " 2 34.546 " 5 37.362 " 6 38.320 " 2 39.398 V. 5 38.138 " 6 42.438 IV. 3 35.620 " 3 38.876 III. 1 36.418 IV. 6 38.250 " 4 42.181 " 2 35.160 " 7 40.512 III. 5 47.190 VI. 3 41.410 IV. 6 34.040 " 2 36.333 " 1 34.400 " 1 35.760 " 3 43.130 " 2 41.176	39 23.10 16 34.58 33 47.38 48 7.23 25 53.61 16 35.02 45 18.87 25 26.53 14 11.96 38 41.56 36 48.51 52 56.03 16 37.43 28 55.28 47 46.06 9 25.83 20 12.17 35 20.38 19 3.58 47 5.36 54 5.95 53 19.05 34 20.79 44 17.01	25.96 25.53 23.31 22.29 21.62 17.47 16.63 16.26 16.07 15.76 15.04 14.74 14.52 12.90 12.75 11.28 11.05 11.04 10.78 10.38 9.93 9.28 8.89 7.45	4 13 17 20 37 41 43 43 45 50 58 20 5 6 7 7 9	2 45.56 1 29.50 3 28.58 4 41.23 5 22.63 2 9.69 3 6.36 3 56.24 6 19.05 3 26.28 4 4.73 4 4.99 3 1.11 4 41.38 5 24.68 5 29.35 6 32.02 4 4.73 3 3.64 4 2.61 5 51.83 6 44.37 4 47.28	40 36 40 45 40 45 40 36 41 4 40 45 40 36 41 12 40 36 41 7 40 28 40 38 41 6 41 13 41 12 40 53	9 9.0 9 20.1 3 30.6 4 49.5 5 35.2 5 12.4 5 55.5 6 2.7 3 48.0 6 30.7 6 11.9 6 23.5 7 18.8 8 57.1 9 43.2 9 43.2 1 43.2 1 43.2 1 43.2 1 44.4 1 44.4 1 44.4	1 199 в. 22 3 399 00 99 33 22 55 75 58 81 11 12 22 66 44 8 м.
				CO	RRECTI	ons.						INSTRU	MENT REA	ADINGS	•		-	
			COR. TO	HOURLY COR.	m.	n.	c.	ZENITH POINT.	COINC.			Α.	CIRCLE.	р.	Mean.	BAR.	THER	мом.
Sept.	14, at 2	22h	s. +3.248	s	s. -0.356	$\begin{vmatrix} s \\ +0.527 \end{vmatrix}$	*.022	0° 6′ 2″.37	r. 40.106	Zon LI	e A.—Sept. 1419.0 19.2 20.0 20.3	280 21 1".9 1.5 	4.5 12.6		5 ¹ ,72 5.68 6.23	29.940 29.926	81°.8 80.5	78°.5

	nde.		SECO	OND	s of	ŤR#	ANS	ITS	Б.								M	ean Rigl	nt Mea	ın Sc	outh
Number.	Magnitude	I.	II.	ш.	ıv. v	. v	71. v	11.	10.	11.	Т.	a.	•	MICROMETER.	D.	d.	1	Ascension 1850.0.	´	clinat 50.0.	ion,
					Zone	LX		Sel	ptem	ıber 1	4. H. I	0.=-	27 S	31 ['] 30	-25.60. "n	.=3.0	00.				
*1	8	35.5	48.2								h. m. s. 20 35 12.87	+13.	.06	I. 6 43.293	—13 ['] 39. ^{''} 37	-22.5	66 2	h. m. s. 0 35 25.9	03 27° 45	5 31.5	93
*2	9				2.0 45.						$35 \ 32.57$	13.		IV. 4 46.190	26 29.21	22.4	8	35 45.6	1	3 21.7	
3	5.6	$ \cdot\cdot $			9.0 11.		- 1	- 1	• •		35 59.13	13.		" 6 40.340	15 21.70	22.4	8	36 12.1	1	7 14.1	
4	9 9	• •	- 1		$egin{array}{c c} 7.0 & . & 44. \end{array}$				٠.	• •	37 26.76	13. 13.		" 6 41.498 " 6 46.548	14 41.72 11 47.27	22.1 21.9	H	37 39.8 38 44.7	1	33.8 39.1	
$\begin{bmatrix} 5 \\ 6 \end{bmatrix}$	8		- 1							: :	38 31.71 39 2.13	13.		" 2 43.460	42 45.29	21.8		39 15.2	į.	1 37.1	
7	7.8				8.050.			- 1	33.3		39 37.75	13.		VI. 2 37.701	46 4.06	21.	H	39 50.8	1	7 55.7	
8	8		27.03	- 1		i i		- 1			40 52.06	13.		I. 5 41.680	23 17.46	21.4	8	41 5.0	1	8.9	92 z.
9	9		4	8.0	1.0 13.	2 .		- 1			41 0.80	13.	04	IV. 4 38.450	30 56.56	21.4	13	41 13.8	84 28 5	2 47.9	99
10	8.9		48.0	1	2.5 .	. .					$42\ 12.52$	12.	99	" 7 38.511	10 33.84	21.9	21	42 25.5	$61 \mid 27 \mid 49$	25.0	05 z.
11	7	١١		8.5	34.	0 46	.0				42 21.33	13.	00	" 6 38.932	16 10.31	21.	.8	42 34.3	3 27 48	3 1.4	49 z.
12	9				0.3 2.	- 1		- 1			43 50.38	12.	.98	" 6 46.452	11 50.62	20.9	8	44 3.3		3 41.5	-
13	9	13.5	- 1		1.0 3.	- 1	. .				45 50.87	12.		" 4 42.272	28 44.54	20.3	3	46 3.8	1	35.0	
14	9				0.0		- 1				$46\ 29.74$	12.		" 4 42.462	28 37.99	20.4	R	46 42.7		28.4	
15	9	$ \cdot\cdot $			7.5 30.						47 17.24	12.		" 6 41.270	14 49.58	20.5	В	47 30.1	I	39.8	
16	8	$ \cdot\cdot $	i		8.5 41				٠.		48 28.63	12.		" 2 35.522 " 6 36 149	47 19.41	20.0	Į.	48 41.6	1	9.4	
17 18	9	1 5	27.5	- 1	4.	- 1		- 1	• •	• •	49 51.86	12. 12.		0 00.112	$\begin{array}{c c} 17 & 46.69 \\ 23 & 24.31 \end{array}$	19.7	ä	50 4.7 51 21.9		9 36.3 5 13.8	
19	$\frac{7.8}{9}$				$egin{array}{c c} 9.0 & 21. \ 33. \ \end{array}$					• •	51 9.01 52 10.56	12.		" 5 41.493 " 2 38.430	45 39.02	$\frac{19.3}{19.3}$		52 23.5	1	7 28.3	
20	7				2.0						52 22.20	12.		" 1 38.485	51 28.67	19.3	8	52 35.1	1	3 18.0	
21		99 9		i	9.2^{12}												ı				
22		1 1	1	- 1	$\frac{9.2}{1.5}$: :	53 59.69 55 11.57	12. 12.		" 2 35.550 " 3 40.780	47 18.45 35 32.54	19.0 18.8	8	54 12.6 55 24.4		7.4	
23	9				2.354						57 42.36	12.		" 2 41.520	43 52.23	18.3	9	57 55.2	5	5 40.6	
24	7.8				5.227						58 15.16	12.		" 5 44.810	21 29.70	18.5	Ħ	58 28.0	1	3 17.9	
25	8	23.2			1.013			- 1			21 0 0.78	12.		" 6 48.230	10 49.20	17.9	a a	1 0 13.6	- (2 37.1	
26	9				6.5 59						046.70	12.	.86	" 2 43.545	$42\ 42.30$	17.8	34	0.59.5	66 28 1	4 30.3	14
27	9				17.		.2		٠.		$2 ext{ 4.51}$	12.	81	" 6 43.410	$13\ 35.67$	17.0	52	2 17.3	$32 \mid 27 \mid 45$	5 23.2	29
28	9				9.0						29.06	12.		" 4 45.980	26 36.46	17.6	i i	2 21.8	1	3 24.0	
29	6	32.2	45.0 5	7.21	0.022	2 34	.5	•	• •	٠.	4 9.80	12.	82	" 2 44.990	41 52.41	17.5	26	4 22.6	$62 \mid 28 \mid 13$	3 39.6	67 z.
30	9				4.5 16						$5 ext{ } 4.54$	1		" 4 44.762	27 18.51	17.	11	5 17.3	1	5.6	62
31	9	1 1			2.8				٠.		8 42.58	12.		" 6 33.085	19 32.26	16.4	8	8 55.3	1	1 18.	
32	7.8	11.2			9.0 0				• •	• •	10 48.63	12.		III. 6 34.752	18 34.64	16.	1	11 1.3	1	20.7	
33	8	21.5			$8.211 \\ 5.217$				• •		10 58.65	12.		IV. 5 40.088	24 12.81	16.	a a	11 11.3		5 58.9	
34 *35	9				$\frac{3.217}{3.0}$				• •		12 5.25 12 53.13	12. 12.		" 2 40.890 " 6 41.860	44 14.07 14 29.18	15.9 15.8	1	12.18.0 $13.5.8$		6 0.0 $6 14.9$	
36	9	: :		1	2.024	- 1	1	,.3			12 33.13	12.		" 5 41.860	23 11.60	15.		14 24.5		4 57.1	
37	9				7.159						15 47.04	12.		" 7 39.180	10 10.77	15.3	8	15 59.7		1 56.9	
38	9				30	- 1					16 17.57	12.		V. 2 35.000	47 37.43	15.5	Ä	16 30.2	- 1	22.0	
39	9	• •		1	7.029	.2 41	8 54	1.2			17 16.98	12.	65	" 6 37.570	16 57.27	15.	10	17 29.6	$63 \mid 27 \mid 48$	3 42.3	39 z.
40	8	1	1	9.03	1.2 43	.5 56	. 0.				18 31.24	12.	. 69	IV. 1 39.848	50 41.84	14.9	00	18 43.9	3 28 29	2 26.7	74
41	9				7.0			1			19 46.99	12.		" 1 38.342	51 23.60	14.6		19 59.6	67 28 2	8.2	29
42	9				8.0 20	.0 32	2.3				21 20 07.72	12.	.64	" 5 39.880	24 19.64	14.0	$34 \mid 2$	1 20 20.3	86 27 50	3 4.5	28
][CO:	RRE	CTIO	NS.							INSTRUI	MENT	READI	NGS.	<u> </u>		
																CIRC	LE.			THE	RMOM.
			COR.		cor.	7	m.	n		c.	ZENITH POINT.	COINC.			Α.	в.	с.	D. Mean	BAR.	At.	Ex.
Sent	14, at	22h		248	s. 0.024	s	s. .356	s. $+0$.		s. +0.029	2 0 0 2".71	r. 40,106	†2	Zone. h. X.—Sept. 1420.0	0 / //	,	11	11 11	1. 29.926	80°.5	77.5
гри	,		, 0.2		. 5.021	"	. 550	1.0,		1 0.02	0 2.11	10,100	111	20.4	293 6 3.3	7.6		6.1 7.7	5		
	‡ T	he rec	orded a	irela :	reading	ofthi	is 70r	a he	a baa	n abes	nged six minutes.			21.0 22.0	1	7.3	1	6.6 5.8 6.9	H		
	ΙT	no rec	oraea C	ncie i	caumg .	or till	o zon	c na	a nee	a chai	igeu six inmutes.			22.0 22.6	1		- 1	$\begin{array}{c c} 5.8 & 6.9 \\ . & 7.1 \end{array}$:::
														23.5		0.4				5	
														0.5	3.6	9.4	15.8	7.8 9.1	5 29.882	77.5	74.5

)e	itud	S	ECON	DS OF	TRA	NSIT	S.	т.			70	,	Mean Right	Mean South
Number.	Magnitude.	ı. II.	ш.	IV. V.	VI.	vII.	10. 11.	8	a.	MICROMETER.	D.	d.	Ascension, 1850.0.	Declination, 1850.0.
			Zone	LX.	Septe	mber	14.	H. D. == -2°	7 31 30.0.	n'. == -25.60	0. n'.=3'.0	0. (Co	ntinued.)	
43	9			45.2	258.0	9 9		h. m. s. 21 20 32.98	s. +12.62	v. 6 39.461	-15 ['] 5204	-14.58	h. m. s.	or 47 06 60
44	9	38.		2.5 14.6				1	12.60	II. 6 39.330	-15 52.04 15 56.49	-14.35 14.35	21 20 45.60 22 15.05	27 47 36".62 z 27 47 40.84
45	9			11.223.4				24 11.24	12.60	" 4 43.233	28 11.23	14.02	24 23.84	27 59 55.25
*46	9	39.552.	0 4.6	17.029.1	1			25 16.91	12.59	IV 4 43.910	27 47.95	13.86	25 29.50	27 59 31.81
47	9			6.5 19.0				26 6.47	12.60	" 2 39.740	$44\ 53.74$	13.73	26 19.07	28 16 37.47 z
48	9	5	1	25.037.0		i	• • • •	28 24.74	12.58	" 2 37.689	46 4.58	13.38	28 37.32	28 17 47.96 z
49 50	7 9			10.022.0 $30.242.5$			• • • •	30 9.94	12.54	" 4 45.532	26 51.90	13.12	30 22.48	27 58 35.02 z
51		31.544.			1 1	1		30 30.11 33 9.01	12.54 12.54	" 4 42.252 III. 1 40.515	28 45.23 50 18.52	$13.07 \\ 12.69$	30 42.65 33 21.55	28 0 28.30 z 28 22 1.31 z
52	9		1	6.819.0				33 6.82	12.52	IV. 3 37.632	30 16.32 37 21.27	12.69 12.70	33 19.34	28 22 1.31 Z 28 9 3.97
	9									6				
53 54	9			$egin{array}{cccc} 49.2 & 1.3 \ 21.0 & 33.3 \end{array}$				33 49.04 35 21.14	12.51 12.52	VI. 3 35.622 IV. 1 40.868	38 30.58	12.60	34 1.55	28 10 13.18 z
55	9			21.0 33.6	i I	30.5	į.	35 53.21	12.52	VII. 3 36.220	$50 6.33 \\ 38 9.71$	12.38 12.31	35 33.66 36 5.70	28 21 48.71 28 9 52.02
56	9		i	53.2 5.8	1 8	1		37 53.34	12.44	IV. 6 40.068	15 31.08	12.01 12.02	38 5.78	28 9 52.02
57	9	• • •	12.2	25.0				38 24.83	12.44	" 6 38.255	16 33.72	11.95	38 37.27	27 48 15.67
58	9			53.5 6.0)			38 53.63	12.45	" 4 34.910	32 58.80	11.88	39 6.08	28 4 40.68
59	9			20.0			• • • •	39 7.64	12.44	VI. 5 44.200	21 50.68	11.84	39 20.08	27 53 32.52 z
*60	7 8			1.7 14.0			$\cdot \cdot \cdot \cdot$	41 1.69	12.44	IV. 3 42.020	34 49.72	11.59	41 14.13	28 6 31.31
$\frac{61}{62}$	8			43.056.0 $40.052.1$: : :	$\begin{array}{c} 41\ 43.42 \\ 42\ 39.78 \end{array}$	12.42 12.42	" 4 39.925 " 3 43.169	$30 5.59 \\ 34 10.05$	11.52	41 55.84	28 1 47.11 z
						ĺ					34 10.03	11.38	42 52.20	28 5 51.43 z
63	9	1	1 1	38.250.8	1 1			43 38.35	12.40	" 4 41.350	29 16.39	11.26	43 50.75	28 0 57.65 z
64 65	9 9	1 1	4 1	36.0 48.2	1 1	1	• • • •	46 35.96	12.37	" 4 36.730	31 55.94	10.88	46 48.33	28 3 36.82 z
66	9	I i		$\begin{array}{c c} . & . & 42.2 \\ 24.5 & 37.0 \end{array}$	1 1	ł	• • • •	$\begin{array}{c} 47 \ 29.92 \\ 47 \ 24.51 \end{array}$	12.36 12.34	" 4 43.290 " 6 46.372	28 9.38	10.77	47 42.28	27 59 50.15 z
67	7.8	1 1		46.0	1::	- 1	· · · · · .	50 46.12	12.34 12.35	II. 1 42.661	$\begin{array}{ccc} 11 & 53.38 \\ 49 & 4.27 \end{array}$	$10.78 \\ 10.35$	47 36.85 50 58.47	27 43 34.16 28 20 44.62
68	8			13.0 25.5	1			51 12.91	12.33	IV. 3 37.620	37 21.67	10.33	51 25.24	28 9 1.96 z
69	9	1 1	1 1					51 0.04	12.32	VII. 4 41.300	29 17.77	10.32	51 12.36	28 1 58.09
70	7.8	1 1		55.0		1		53 55.08	12.30	IV. 3 44.278	33 31.76	9.94	54 7.38	28 5 11.70 z
71	8	!!		23.5 35.0	1 1			54 22.91	12.27	" 6 41.428	14 44.13	9.88	$54 \ 35.18$	27 46 24.01 z
72	9	36.549.	0 1.4	13.8 25.8	38.6	51.0	• • • •	22 0 13.76	12.22	" 5 40.437	24 - 0.77	9.12	22 0 25.98	27 55 39.89 z
73	8		12.3	25.0 37.3	50.0			$1\ 24.96$	12.24	" 1 36.483	52 37.82	8.97	1 37.20	28 24 16.79 z
74	6.7			44.056.5			` .	$2\ 44.24$	12.19	" 5 44.680	21 34.19	8.79	2 56.43	27 53 12.98 z
75				55.0			• • • •	3 54.94	12.18	" 6 36.205	17 44.52	8.64	4 7.12	27 49 23.16 z
76	9			$\begin{array}{c c} 57.0 & 9.0 \\ 40.0 & 0 \end{array}$			• • • •	3 56.70	12.20	" 3 32.648	40 13.40	8.64	4 8.90	28 11 52.04
77 78	$\frac{9}{6.7}$			49.0 8.821.0			• • • •	30 48.98	11.91	" 4 35.182	32 49.42	5.33	31 0.89	28 4 24.75
79	9			$56.2 \begin{array}{ c c c c c c c c c c c c c c c c c c c$			·	$31 8.83 \\ 32 56.05$	11.89 11.90	" 6 35.975 " 4 38.872	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	5.29	31 20.72	27 49 27.74 28 2 17.07 z
80	9			48.0 0.8				00 40 00	11.89	" 3 35.985	38 18.16	$\frac{5.11}{5.02}$	$33 7.95 \\ 34 0.18$	28 2 17.07 z 28 9 53.18 z
81	8.9			28.2 40.8				35 28.25	11.86	" 4 44.283	27 34.91	$\frac{3.0z}{4.85}$	35 40.11	26 9 33.16 z 27 59 9.76 z
82	9	1	1 1	35.248.0	1			36 35.63	11.86	III. 3 45.050	33 5.04	4.73	36 47.49	28 4 39.77 z
83	8		2.0	14.226.8	39.0			37 14.37	11.83	IV. 6 42.150	14 19.18	4.66	37 26.20	27 45 53.84 z
84	9			46.5				38 34.13	11.84	V. 3 34.226	39 18.91	$\frac{4.60}{4.53}$	37 26.20	27 45 53.84 z 28 10 53.44
85	8			56.0 8.2				38 56.01	11.85	IV. 2 35.182	47 31.19	4.49	39 7.86	28 19 5.68
86	7.8	35.	0 47.2	1.0 13.2	26.0	38.2		40 0.41	11.84	II. 1 42.018	49 26.50	4.38	40 12.25	28 21 0.88 z
87				28.0 40.0		5.0		42 27.80	11.79	IV. 4 35.600	32 34.98	4.16	42 39.59	28 3 9.11
88				2.515.0				44 2.75	11.79	" 3 34.161	39 21.18	4.01	44 14.54	28 10 55.19 z.
89	9			13.0 25.0				45 13.07	11.75	" 6 40.780	15 6.48	3.91	45 24.82	27 46 40.39
90	8			15.227.2				46 15.23	11.73	" 6 44.916	12 43.64	3.81	46 26.96	27 44 17.45 z
91	9			28.0 40.5				48 28.25	11.76	" 1 36.311	52 43.75	3.61	48 40.01	28 24 17.36
92	9			43.0 55.0	1	-		51 42.73	11.70	" 4 40.440	29 47.83	3.33	51 54.43	28 1 21.16
93	8	16.0 28.	$0 \dots $		18.2	30.3		51 53.13	11.69	VI. 5 43.272	22 22.74	3.31	52 4.82	27 53 56.05
94	9	11.0 23.	5 36.0	48.0 1.0	13.0	1	1	2	11.68	IV. 3 36.863	37 47.84	3.16	54 - 0.02	28 9 21.00
95	9	150 911	0.93 1	36.0	1			22 55 35.82	11.68	" 2 36.440	46 47.76	3.01	$22\ 55\ 47.50$	28 18 20.77

	tude.	S	ECOI	NDS (OF 7	TRA:	NSI.	rs.							Mean Right	Mean Sou
	Magnitude.	ı. II.	III.	ıv.	v.	VI.	VII.	10.	11.	Т.	a.	MICROMETER.	D.	d.	Ascension, 1859.0.	Declination 1850.0.
			Zor	ne LX		Sept	embo	er 14.]	H. $D = -2$	[°] 7 31 30″.0	n'. == -25.	60. n. = 3	.00 (C	ontinued.)	
6 7	.8	53.5 6.	218 9	21 0	43 0	56.0	7.8			h. m. s. 22 56 30.56	s. +11.64	IV. 5 38.550	$-25^{'}$ 5 $^{''}$ 91		h. m. s. 22 56 42.20	27° 56′ 38″.85
7 9	- 1	3.516.	1	3 1		i i	• •	1		23 0 40.70	11.60	" 5 36.410	26 19.86	2.61	23 0 52.30	27 57 52.47
3 9	,		53.0	5.5	18.0	30.5	43.0			1 5.63	11.59	" 5 42.136	23 2.08	2.58	$1\ 17.22$	27 54 34.66
9	- 1			57.6						157.34	11.60	V. 3 42.680	34 26.87	2.52	2 8.94	28 5 59.39
1	i i			56.0			1	1	٠.	2 55.97	11.56	IV. 6 46.120 " 3 40.315	12 2.07 35 48.64	$2.45 \\ 2.27$	$3 7.53 \\ 5 40.00$	27 43 34.52 28 7 20.91
$\begin{array}{c c} 1 & 9 \\ 2 & 9 \end{array}$		$\begin{bmatrix} 51.0 & 3. \\ & \end{bmatrix}$		811.2			• •			5 28.43 $6 11.35$	11.57 11.54	" 3 40.315 " 5 47.172	20 8.15	$\frac{2.27}{2.22}$	6 22.89	27 51 40.37
3 9	- 1	$51.0 \ 4.$								7 28.38	11.54	" 4 43.280	28 9.72	2.13	7 39.92	27 59 41.85
1		39.051.		1 1		1				8 16.14	11.52	" 5 43.285	22 22.39	2.08	8 27.66	27 53 54.47
5 9)			• •	16.2	28.8	51.0			9 3.95	11.51	" 6 40.435	15 18.42	2.02	9 15.46	27 46 50.44
6 6		26.5 39.								13 3.61	11.47	" 6 37.602	16 56.23	1.78	13 15.08	27 48 28.01
7 8	i	13.225.			l	1 1	1			15 50.41	11.46	" 3 42.268	34 41.17	1.62	16 1.87	28 6 12.79
	7.8	3		32.0	l			1 1	• •	16 32.19	11.46	" 3 34.980 " 2 42.261	38 52.87	1.58	16 43.65 18 12.73	28 10 24.45 28 14 58.17
$\begin{bmatrix} 9 & 7 \\ 0 & 8 \end{bmatrix}$		$egin{array}{c c} 24.0 & . \ 44.858. \end{array}$								$ \begin{array}{cccc} 18 & 1.28 \\ 19 & 22.78 \end{array} $	11.45 11.42	" 3 42.291	43 26.68 34 40.41	$1.49 \\ 1.41$	19 34.20	28 6 11.82
$\begin{array}{c c} 1 & 9 \end{array}$	- 1	29.542.		1		1				21 6.90	11.40	" 5 40.969	23 42.39	1.32	21 18.30	27 55 13.71
9 9)	3.3 15.								$22\ 40.64$	11.39	" 3 40.480	35 42.94	1.25	22 52.03	28 7 14.19
3 9	- 1			5.1				• •	• •	23 5.20	11.38	" 3 32.133	40 31.23	1.23	23 16.58	28 12 2.46
$ \begin{array}{c c} 4 & 9 \\ 5 & 9 \end{array} $	- 1	1.2 13.		53.6			30.6			23 53.44 26 38.50	11.37 11.36	" 5 36.130 " 2 42.610	26 29.52 43 14.60	$\frac{1.19}{1.07}$	24 4.81 26 49.86	$\begin{bmatrix} 27 & 58 & 0.71 \\ 28 & 14 & 45.67 \end{bmatrix}$
	- 1	56.0 8.									11.35	2 12.010		1.02	27 44.84	28 18 50.53
$egin{array}{c c} 6 & 7 \\ 7 & 9 \end{array}$	- 1	30.0 0.	i i	38.0	l	1				$\begin{array}{c} 27 \ 33.49 \\ 27 \ 38.35 \end{array}$	11.33	" 2 35.519 " 3 41.595	47 19.51 35 4.48	$\frac{1.02}{1.02}$	27 49.69	28 6 35.40
8 7	- 1		1	1	l	29.5		1 (28 4.74	11.32	VII. 7 38.045	10 49.61	1.00	28 16.06	27 42 20.61
9 9	- 1			53.2						29 53.40	11.32	IV. 4 34.050	33 28.52	0.92	$30 \ 4.72$	28 4 59.44
$0 \mid 9$		• • •	- 1	18.5	ı	1	1	1 1		31 18.39	11.30	" 5 33.910 " 7 36 590	27 46.19	0.86	31 29 69	$\begin{bmatrix} 27 & 59 & 17.05 \\ 27 & 43 & 13.44 \end{bmatrix}$
$egin{array}{c c} 1 & 7 \ 2 & 9 \end{array}$	8.			$16.5 \\ 13.0$		41.5				32 16.55 33 12.98	11.28 11.29	" 7 36.520 " 2 44.160	11 42.61 42 21.08	$0.83 \\ 0.79$	$32\ 27.83$ $33\ 24.27$	28 13 51.87
$\begin{bmatrix} 2 \\ 3 \end{bmatrix} \begin{bmatrix} 3 \\ 9 \end{bmatrix}$		28.240.								36 5.58	11.26	" 4 39.693	30 13.59	0.69	36 17.84	28 1 44.28
$4 \mid 9$	- 1	- 1	- 1	137.8	l .					$36\ 37.72$	11.26	" 1 42.541	49 8.51	0.67	36 48.98	28 20 39.18
5 8	3	• • •	• • •	49.0	1.5	14.0	26.5	$ \cdot\cdot $	٠.	36 49.25	11.23	" 7 43.810	7 30.85	0.66	37 0.48	27 39 1.51
6 9	- 1		1	25.0						$37\ 24.82$	11.23	" 6 45.470	12 24.53	0.63	37 36.05	27 43 55.16
$ \begin{array}{c c} 7 & 9 \\ 8 & 9 \end{array} $								52.0		38 56.02 40 46.66	11.23 11.23	" 3 36.850 " 1 38.406	37 48.28 51 31.39	$0.58 \\ 0.52$	39 7.25 40 57.89	28 9 18.86 28 23 1.91
$\frac{3}{9} \mid \frac{9}{9}$		33.546.								42 10.76	11.23	" 5 36.365	26 21.41	$0.32 \\ 0.49$	42 21.96	27 57 51.90
$0 \mid 9$		46.058.		1		1				44 22.95	11.18	" 5 43.500	22 14.92	0.44	44 34.13	27 53 45.36
1 8		47.859.							٠.	46 24.60	11.16	" 5 45.365	21 10.56	0.39	46 35.76	27 52 40.95
2 9	- 1								٠.	47 35.50	11.15	" 3 39.760	36 7.77	0.36	47 46.65	28 7 38.13
$\begin{bmatrix} 8 \\ 4 \end{bmatrix} \begin{bmatrix} 9 \\ \end{bmatrix}$	i	$36.5 49. \\ 13.$						1 1	• •	49 14.04 31 37.67	11.12 11.11	" 7 41.655 " 3 41.040	8 45.28 35 23.57	$0.32 \\ 0.28$	49 25.16 51 48.78	$\begin{bmatrix} 27 & 40 & 15.00 \\ 28 & 6 & 53.85 \end{bmatrix}$
1 9 5 9	- 1	54.								52 18.21	11.11	" 7 37.445	35 23.57 11 10.71	$0.28 \\ 0.27$	52 29.31	27 42 40.98
3 9		1.								53 26.27	11.12	" 1 38.969	51 11.91	0.25	53 37.39	28 22 42.16
$\frac{3}{7} \frac{3}{8}$		58.	1) 1	l	1				54 22.41	11.12	" 5 36.651	26 11.50	0.23	54 33.50	27 57 41.74
3 9		15.0 27 .	2 39.9	52.0			29.5			56 52.21	11.06	" 3 43.110	34 12.08	0.20	$57 \ \ 3.27$	28 5 42.28
- 1	3.9	10.	0 22.5	5	47.0					57 34.85	11.06	" 3 42.025	34 49.56	0.20	57 45.91	28 6 19.76
i	- 1	49.0 1.							• •	59 26.35	11.05	" 2 44.009	42 26.29	0.17	59 37.40	28 13 56.46
$\begin{bmatrix} 1 & 9 \\ 2 & 9 \end{bmatrix}$	- 1	3.516.			l .	l				$\begin{array}{cccc} 59 & 1.27 \\ 0 & 0.40.39 \end{array}$	11.05 11.03	" 2 37.670 " 6 38.480	$\begin{array}{c cccc} 46 & 5.24 \\ 16 & 25.95 \end{array}$	$\begin{array}{c} 0.17 \\ 0.16 \end{array}$	59 12.32 0 0 51.42	28 17 35.41 27 47 56.11
3 9		55.6 8.								3 32.86	11.03	" 6 33.330	19 23.81	0.10	3 43.86	27 50 53.95
- 1				313.0						4 13.18	11.00	" 7 36.180	11 54.39	0.14	4 24.18	27 43 24.53
5 7	7.8			47.5						4 47.65	10.99	" 7 39.320	10 5.94	0.14	4 58.64	27 41 36.08
6 7	7.8	55.8 8.								6 33.38	10.98	II. 1 40.870	50 6.15	0.13	6 44.36	28 21 36.28
7 8				39.0						6.38.78	10.98	IV. 4 42.450	28 38.40	0.13	6 49.76	28 0 8.53
8 9)	.	.		28.0	40.3	52.8	• •	٠.	0 7 15.51	10.97	V. 1 43.168	48 46.86	0.12	0 7 26.48	28 20 16.98

er.	Magnitude.		SE	CON	DS (OF '	ΓRΑΙ	risi	's.		m					- I		I		Right	1	n Sc	
Number.	Magn	I.	и.	111.	IV.	v.	vi.	vII.	10.	11.	Т.	a.		MICROME	TER.	D.	d.		Asce 1850	ension,	1	clinat 0.0.	ion,
				Zoi	ne L	X.	Sep	temb	er 1	4.	Н. Д.=-	–27° 31′	3 00	. n.'=	=2560.	n.'=3'.	.00.	(Co	ntinue	d.)			
149	9			22.5	36.0	47.0		12.2			h. m. s. 0 8 35.17	+10	.96	IV. 4 44		27 10".65	_ o''.	12	h. n 0 8	ı. s. 46.13	27° 58	40"	77
150	9		55.8		20.5	33.0	45.1				9 20.45	1	¥	" 6 44		13 4.93		11		31.40	27 44		
151	9	47.5									14 24.90	10	.91	III. 2 43		42 31.73		23		35.81	28 14		
152	8		$ \cdot\cdot $			49.5	2.0	14.5		• •	$14 \ 37.16$	10.	.91	IV. 5 48	3.520	19 21.54	0.	23	14	48.07	27 50	51.7	77 z
153	9		51.0					• •			16 16.30	1		III. 2 42		43 16.63	0.	27		27.19	28 14	46.9	90
154	7.8		1 1)		• •		16 35.68	1		IV. 5 40		20 47.17		28		46.57	27 52		
155 156	7.8	19 7	56.9			1	3 12.0				16 47.24	1	1	VI. 6 43	- 1	13 23.79		29		58.13	27 44		
157	7.8	45.7	56.2				51.3		• •		21 21.07			IV. 2 43	1	42 28.60		45		31.92	28 13		
158	9						41.3			[21 26.81 22 16.47			" 5 49		18 49.41		46		37.66	27 50		
					1			55.0	• •				.04	9 46	5.230	32 58.17	0.	51		27.31	28 4	28.0	08 Z
159	8		35.5			1	1		٠.	• •	28 0.38	1	8	" 7 40		9 32.61		88		11.17	27 41		
160	8	1	39.2		1	10.6	1	49.5	• •	• •	29 4.01	1	8		2.338	34 38.76		.95		14.79		9.7	
161	8				6.5	19.0	31.0	43.5	• •		0 29 6.38	10	.78	V. 2 42	2.476	43 19.23	0.	95	0 29	17.16	28 17	50.	18
1 2 3	8 9 9	48.8	1.5	l	10.5	23.0	0		 		19 15 23.20 17 26.75 18 10.47	13 13	.14 .16	VII. 3 40 III. 3 39 V. 1 44	9.27 1.53	35 53.00 36 25.78 48 1.05	18. 17. 17.	.81 .64	17 18	36.36 39.87 23.63	29 35 29 36 29 47	3.5	59 z 69 z
4	9	• •	• •	• •			1	1			18 41.35	1		VII.2 43		41 32.88	17.			54.49	29 41		
5 6	9			• •	10.5		. [24.0	19 14.95	1	.09	11. 6 38	I	16 36.15	17.			28.04	29 16		
7	8	,			10.5	23.0			 99 <i>6</i>	35.5	21 10.49 21 25.99	1	.12 .13	VII. 3 30 11. 2 33		41 40.94	16.	- 8		23.61	29 41		
8		26.2	39.1				1				25 4.03		.04	III. 2 33		$\begin{array}{c c} 48 & 26.50 \\ 10 & 2.45 \end{array}$	16.	8		$\frac{39.12}{17.07}$	29 48		
9		J						45.2			25 7.61	1		VII. 7 4:		8 52.05	$\frac{16}{16}$.	8		20.64	1	38.4 328.0	
10	8		51.4		1	1					28 16.25		.00	III. 7 4		9 4.40	15.	8		29.25	29 8		
11	9	 			 		28.4	40. 9		l l	29 3.28	19	.00		j								
12	9		50.0					52.5			32 15.00	- 1	.98	VII. 6 43 2. 7 33	- 1	$\begin{bmatrix} 12 & 7.30 \\ 12 & 10.79 \end{bmatrix}$	$\frac{15}{14}$.	B B		16.28 27.98	29 11 29 11		
13	8.9						41.5				38 16.48	- 1	.96	2. 4 30		31 52.13	13.			29.44	29 31		
14	9.10	o				1	6 30.3				39 5.15	- 1	.93	VI. 6 38	1	16 27.33	12.	9		18.08	29 16		
15	2								3212	45.5	39 36.17	12	.91	VII.7 40		9 37.63	12.			49.08			
16		9		l		1	0			• •	45 27.50	1	.92	2. 1 43	5.15	47 39.02	11.	.43		40.42	29 47		
17	9				56.5	• •	22.0				46 56.60		.88	VI. 4 40		29 32.46	11.	.11		9.48	29 29	3.3	57
18	9	• •	• •	• •						32.0	46 22.47	3	.89	11. 3 4.	1	35 14.43	11.			35.36			
19 20	10 9		• •	• •	40.9		$\begin{vmatrix} 33.0 \\ 5.5 \end{vmatrix}$	1	• •		48 7.57	1		VII. 4 4	I	29 8.38	10.			20.44			
		• •						• •	٠.	• •	49 40.20	12	.83	VI. 6 39	9.06	15 45.82	10.	.50	49	53.03	29 15	16.3	32
21	8		22.8		1	1	2	• •		· ·	55 47.73		.80	1. 4 39	9.80	30 9.97	9.	.18	56	0.53	29 29	39.3	15 z
22 23	9.10	1			46.8	1	1	• •	٠.	• •	56 46.74	1	.80	II. 3 49	- 1	34 32.36		.96		59.54	1		
23	0					34.	5 47.2				19 58 21.94	12	.81	VII.1 39	9.60	50 51.10	8.	.63	19 58	34.75	29 50	19.7	73
						COR	RECT	ons.						CONTRACTOR CONTRACTOR		INSTRU	MENT	REAL	DINGS				
			cor.		Hou		m.				ZENITH	GOT					CII	RCLE.				тне	RMOM
			CLO	ck.	CO	R.	116.	21	.	с.	POINT.	COINC.				Α.	в.	c.	р.	Mean.	BAR.	At.	Ex
Sept.	15, at 2	22h	**************************************	. 484		021	s. -0,356	+0.	527	$^s. +0.022$	o° o′ 3″.52	r. 40.110	$^{\dagger Zo}_{ m LX}$	ne I.—Sept. 1:	h. 519.3	291° 38′ 46″.8	51.1	50.7	50".2	51".28	1. 30.045	77°.6	69°.
				1				1	<u> </u>	· · · · · · · · · · · · · · · · · · ·					20.3			٠.			30.051	75.8	65.
	† The	e circle	e readi	ng rec	corded	l for t	his zon	e has	been	change	ed three minutes									-			
													1			1	!						

ï.	nde.		SE	CON	DS (OF '	TRA	risn	rs.								Mean	Right	Mea	n So	uth
Number.	Magnitude.	ı.	п.	ш.	IV.	v.	vi.	vII.	10.	11.	Т.	a	•	MICROMETER.	D.	d.		ension,	1	clinati 50.0.	ion,
			\mathbf{z}	one	LXI	•	Sept	embe	r 15.	Ŋ	D = -	-28° 59	20.0	o. n'. = -21''.9	7. " ". = —	$4^{''}_{-}00$.	(Contin	nued.)			
24	7.8		33.5	45.8						• •	h. m. s. 20 1 58.44	+12	8	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	_ 8 24 .03	7′.8	5 20	n. s. 2 11.15	1	51.8	
25 26	9 10		57.0				32.0	- 1		• •	$\begin{array}{ccc} 8 & 6.76 \\ 10 & 22.51 \end{array}$		$.72 \\ .68$	I. 1 38.115 2. 1 39.56	51 42.46 50 51.45	$\frac{6.5}{6.0}$	R	8 19.48 0 35.19	29 51 29 50		
27	8		22.0			• •					10 22.31		.67	III. 3 39.54	36 16.41	6.0	8	0 59.79	29 35		
28	7.8						25.3				11 0.08		.67	VII. 3 32.36	40 24.26	5.9	8	1 12.75	29 39		
29	10				29.7						13 29.70	i	.64	IV. 3 36.33	38 7.39	5.4	R	3 42.34	29 37		
30	7.8		51.2		1 1			• •	• •	• •	15 16.35		.62	2. 4 33.35	33 53.08	5.1	3	5 28.97	29 33		
31 32	8				$\frac{2.2}{7.0}$		32.4	45.0			16 2.07 20 17 7.14		.57 .60	VI. 7 40.74 VII. 3 43.51	9 17.43 33 58.98	$\frac{4.9}{4.7}$	H	6 14.64 7 19.74	29 8 29 33		
		2			Zon	ie L	XII.	Se	epten	nber 1	5. M.	D. = -	-26 5	58 50.0. n.=	—20.82. n	í. — — 7					
1	5								34.5	47.2	20 42 39.09	12	.23	11. 4 41.26	29 22.56	20.3	6 20 4	2 51.32	27 28	32.9	 2
2	9								46.5	59.1	43 50.98	1	.24	" 2 40.40	44 34.03	20.1	i i	4 3.22	27 43		
3	10		53.0				, ·		• •	• •	47 17.98	- 1	.21	III. 1 45.54	47 28.87	19.5	1	7 30.19	1	38.4	
4 5	$\frac{10}{10}$	15.0	27.8	 40 5			7.5	19.7 			47 42.62 49 52.67	- 1	.21	VII. 1 40.62 III. 1 40.35	50 18.55 50 28.19	$19.5 \\ 19.1$	i i	754.83 04.86	27 49 27 49		
6	9				24.0		3			The state of the s	50 24.01	1	.16	IV. 3 39.40	36 24.23	19.0		0.4.00 $0.36.17$	27 35		
7	9		20.0	32.3	44.7				٠.		51 44.73	1	.15	V. 3 35.52	38 38.16	18.8	5	1 56.88	27 37		
8	6.7				38.0		2.8				52 38.08		.13	VII.4 42.52	28 39.61	18.7		2 50.21	27 27		
9	9.10		21.5		1		17 0	• •	٠.		54 46.23	Į.	.12	V. 3 35.46	38 40.28	18.4		4 58.35	27 37		
*10	9						47.2	59.8	• •		55 22.46		.08	" 6 31.60	20 27.48	18.3		5 34.54	27 19	35.7	9
11	ł		51.1		16.0			• •		• •	58 15.88		.10	II. 1 33.77	54 15.38	17.8	K	8 27.98	27 53		
12 13	$\begin{vmatrix} 9 \\ 7.8 \end{vmatrix}$		• •		1)		50.2	l 1	 57.0	9.9	59 25.52 21 0 1.63		.03	VII. 7 33.72 11. 2 42.30	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$17.6 \\ 17.5$	8	9 37.55 0 13.70	27 12 27 42		
14	9				8.3	20.0				3.3	2 8.05		.01	V. 7 46.30	6 8.87	17.3 17.2		2 20.06	27 42		
15	10									18.5	2 9.58		.06	11. 2 40.40	44 34.03	17.2	8	2 21.64	27 43		
16	9			٠.			10.0	22.0			$3\ 45.15$	12	.01	VII. 6 32.79	19 46.13	17.0	7	3 57.16	27 18	53.2	0:
17	1	39.3	52.0	4.0	i 1		• •			• • •	6 16.57	1	.00	IV. 3 43.25	34 11.25	16.7	1	6 28.57	1	17.9	
18	8.9						1		• •		8 38.08	1	.94	2. 7 44.27	7 18.32	16.3	1	8 50.02	27 6		
19 20	9 8.9			• •	• •	٠.	11.8	$\frac{20.3}{23.8}$		• •	8 43.14 9 46.98	1	.94	VII.1 37.69 10. 6 40.45	51 59.77 $15 21.22$	$16.3 \\ 16.2$		8 55.14 9 58.92	27 51 27 14		
		• •		• •		• •															
21 22	9			• •		• •	14.2	$\frac{26.5}{14.6}$			10 49.37 11 37.55	1	.98	VII.1 39.70 " 6 34.76	50 50.02 18 38.08	$16.0 \\ 15.9$	1	$1 1.35 \\ 1 49.47$	27 49		
23	9					• • •				1.0	12 53.19	1	.92	11. 6 39.78	15 44.09	15.9 15.8		3 5.10	$\begin{vmatrix} 27 & 17 \\ 27 & 14 \end{vmatrix}$		
24	9.10								49.5		13 54.13	1	.94	" 2 36.96	46 32.83	15.6		4 6.07	27 45		
25	10				18.0		42.6	1			17 17.88	1	.91	VII.1 41.93	49 33.31	15.2	2	7 29.79	27 48		
$\frac{26}{27}$	$8.9 \\ 9.10$		57.5		$\frac{22.2}{34.7}$		59.4				19 21.95 20 34.67		.83	V. 6 46.17 VI. 1 43.83	12 4.33 48 27.89	$14.9 \\ 14.8$		9 33.78 0 46.55	27 11 27 47		
							RECT										READINGS		~		
				1											INSTRU	CIRC				THER	MO
			COR.	- 1	HOUR		m.	77	ı.	c.	ZENITH POINT.	coinc.			A.	в.	С. р.	Mean.	BAR.	At.	E
Zant	16	2014	. s.		8.		s. 0.050	8.	507	8.	0° 0′ 3′.25	r. 40,110	† <i>Z</i> 0	one h.		45.2	50'.8 42'.7	45,30	r. 30,052	EVE ^O O	
ept.	15, at 9	sish .	+2.	404	-0.0	U2.1 -	-0.356	+0.	521	+0,022	0 0 3.25	40,110	\parallel^{LX}	III.—Sept. 1520.7	40.0			45.25	30,052 30,096	75.0 72.0	64
														22.1 23.1		§	: : : :	43.25	30.104	69.5	57
+ 7	he circ	ele res	ding of	fhic	ZOno I	na≈ h-	een ob	angod	thro	e min	ites from the re	corded		23.3 23.5		: :	: : : :	43.25	30.106	68.3	57
read	ing.	104	ang or			1)		gcu	LINE		nom the re	Januar		0.01.5		· · ·		10 67	30.110 30.108	$67.7 \\ 65.8$	56 55
													11	1.7	36.3	39.6	46.0 40.8	40.67	!		



er.	tude.	8	SECON	NDS (OF T	RAN	SITS.						_	Mean Right	Mean South
Number.	Magnitude.	1.	. 1111.	IV.	v.	vi. v	п. 10.	11.	Т.	a.	MICROMETER.	D.	d.	Ascension, 1850.0.	Declination, 1850.0.
			Zon	ie LX	II.	Sept	ember	15.	M. D.=	—26° 58′ 50		0.82. n' =	—7 ^{′′} .00.	(Continued.)	
28	9.10		. 51.0	3.2	15.52	8.0 40			$h. \ m. \ s. \ 21 \ 22 \ 3.25$	*. +11.86	v. VII. 1 43.63	_48 ['] 34 ^{''} .58	-14.63	$h. \ m. \ s. \ 21 \ 22 \ 15.11$	27° 47′ 39″.21 z.
29	9	29.6 42	- 1		$19.1 _{3}$.		24 - 6.87	11.83	" 3 34.62	39 8.97	14.37	24 18.70	27 38 13.34 z.
30	9		. 55.5		20.4				35 8.08	11.69	V. 7 34.46	12 57.77	13.06	35 19.77	27 12 0.83 z.
31	8	• • •		1 1	21.5				36 9.41	11.68	VI. 7 36.94	11 32.04	12.95	36 21.09	27 10 34.99 z.
32 33	8.9		1	1	1	- 1	1	0 9 9	36 51.62	11.67	VII. 7 37.19	11 23.21	12.87	37 3.29	27 10 26.08 z.
34	9 9			1 1	5		. 50.0	- 1	38 54.56 $40 29.42$	11.65 11.68	11. 6 36.33 VII.1 39.13	17 43.28 51 10.04	$12.64 \\ 12.47$	$39 6.21 \\ 40 41.10$	27 16 45.92 27 50 12.51
35		10.022	1	1 1			- 1		43 47.31	11.65	VII. 1 42.41	49 16.97	12.13	43 58.96	27 48 19.10 z.
1	10		. 38.3				1		46 50.70	11.58	IV. 5 45.37	21 14.39	11.82	47 2.28	27 20 16.21
37	9.10	35.748				.	- 1		48 12.97	11.59	2. 2 40.41	44 33.93	11.68	48 24.56	27 43 35.61 z.
38	7.8	.			4	0 5 59	7		48 15.87	11.55	VII. 7 45.72	6 28.60	11.68	48 27.42	27 5 30.28
39		30.643							52 7.88	11.52	1. 6 40.38	15 23.39	11.31	48 27.42 52 19.40	27 5 30.28 27 14 24.70 z.
40	8.9	59						1 1	54 23.67	11.53	VI. 1 35.54	53 14.22	11.10	54 35.20	27 52 15.32
41		15.328							55 52.56	11.50	V. 3 44.62	33 23.85	10.96	56 4.06	27 32 24.81
42		40.9 53				2.5 54	.9		22 0 17.87	11.44	2. 5 38.50	25 10.99	10.57	22 0 29.31	$27\ 24\ 11.56$
		53.8	į.						3 30.94	11.39	VI. 7 38.38	10 42.33	10.23	3 42.33	27 9 42.56
44	8.9	.		1 1	2				3 55.67	11.43	VII.1 40.55	50 20.96	10.18	4 7.10	27 49 21.14 z.
45 46	8.9	31.444					. 20.0		4 24.60 8 8.56	11.38	11. 6 40.97 2. 6 43.545	15 3.00	10.14	4 35.98	27 14 3.14 z.
47	8		.2 18.5						15 30.65	$11.34 \\ 11.26$	I. 7 41.76	$\begin{array}{c c} 13 & 34.29 \\ 8 & 45.35 \end{array}$	$9.71 \\ 8.87$	8 19.90 15 41.91	27 12 34.00 27 7 44.22 z.
		į	. 1	1 1	j			' '							
48	7.8	.		, ,		1	.5	• •	16 10.56	11.29	VII. 3 36.58	38 1.28	8.79	16 21.85	27 37 0.07 z.
49 50	$\frac{9.10}{7.8}$	• • •	1		17.33		.6		18 30.52	11.28	" 1 34.12 " 7 36.51	54 3.05	8.53	18 41.80	27 53 1.58
	10	47	0.059.0	1 1	i i	0.042			19 5.21 21 11.50	11.23 11.22	III. 6 31.762	11 46.66 20 21.91	$8.46 \\ 8.24$	$\begin{array}{c} 19 \ 16.44 \\ 21 \ 22.72 \end{array}$	27 10 45.12 z. 27 19 20.15 z.
*52	6.7								21 10.61	11.25	10. 1 35.20	53 25.42	8.24	21 21.86	27 52 23.66 z.
53	9.10	.	1	1 1	2				23 3.99	11.22	11. 2 43.01	43 3.86	8.06	23 15.21	27 42 1.92
54	10 6.0	18.8	$24\ 10.85$	11.18	" 6 41.00	15 1.97	7.95	$24\ 22.03$	27 13 59.92
55	9.10		.5 16.6						27 29.02	11.18	" 2 42.58	43 19.62	7.64	27 40.20	$27\ 42\ 17.26$
56	9	27						• •	29 51.97	11.15	2. 3 33.30	39 54.23	7.41	30 3.12	27 38 51.64
57	4	45	ĺ			4.0 47	.0	• •	32 9.68	11.14	I. 1 40.28	50 30.33	7.22	32 20.82	27 49 27.55
58	9.10	50	7 3.0	15.4	27.9 .	.			35 15.49	11.10	" 2 47.44	40 31.51	6.96	35 26.59	27 39 28.47
59	9	• • •			14.72°				37 2.47		VII. 7 47.16	5 38.89	6.81	37 13.51	27 4 35.70
60	8		915 7				10.7	1 1	37 15.03	1	11. 1 46.50	46 54.87	6.79	37 26.12	
61 62	$\frac{9}{9.10}$	50.8 3	- 1	1 (1	1	.5		40 27.95 42 30.55	11.02	VI. 5 46.70 VII. 5 49.96	20 28.31	6.53	40 38.97	27 19 24.84
63	9		- 1	1	1	- 1	.5		42 35.54	$11.00 \\ 11.00$	" 6 40.68	18 35.54 15 13.62	$6.38 \\ 6.37$	$\begin{array}{c} 42 \ 41.55 \\ 42 \ 46.54 \end{array}$	27 17 31.92 27 14 9.99 z.
	- 1	36.5 49							45 14.02	11.01	III. 1 45.24	47 39.28	6.18	45 25.03	27 46 35.46
65	3	.			28.54				$46\ 16.20$	10.99	IV. 2 39.20	45 16.40	6.11	46 27.19	27 44 12.51 z.
66	8	.							$48\ 28.86$	10.95	VII.4 43.67	27 59.91	5.95	48 39.81	27 26 55.86
67	9.10	• • •	• • •		20.0	. 45	.0	• •	49 7.83	10.95	" 3 38.54	36 53.58	5.90	49 18.78	27 35 49.48
68	9.10	11.523	7 36.0	48.0	.				51 48.37	10.92	V. 4 41.76	29 6.16	5.73	51 59.29	27 28 1.89
69	9.10	.					. 46.7	759.0	51 51.04	10.93	11. 3 37.20	37 39.28	5.73	52 1.97	27 36 35.01
70		41.9 54							55 18.97	10.89	2. 3 36.19	38 14.40	5.51	55 29.86	27 37 9.91 z.
71		32							23 2 56.78	10.82	III. 2 40.26	44 39.76	5.12	23 3 7.60	27 43 34.88 z.
72		36							5 0.47	10.78	" 6 42.98	13 54.49	5.02	5 11.25	27 12 49.51 z.
$\begin{bmatrix} 73 \\ 74 \end{bmatrix}$	$8.9 \\ 9.10$.0		$5\ 17.01$ $6\ 59.00$	10.79	VI. 5 43.34 " 4 42.21	22 24.19	5.01	5 27.80	27 21 19.20 z.
75	9.10		1 1				.2		8 9.32	10.77 10.76	VII. 7 36.15	$28 50.57 \ 11 59.13$	$\frac{4.94}{4.90}$	$\begin{bmatrix} 7 & 9.77 \\ 8 & 20.08 \end{bmatrix}$	27 27 45.51 27 10 54.03
76	9.10		i 1				.1		9 35.73	10.75	" 2 34.56	47 56.31	4.84	9 46.48	27 46 51.15
77		.					.0	1 8	11 18.95	10.73	" 5 36.89	26 6.95	4.79	11 29.68	27 25 1.74
78	5		. 52.3				1		13 4.59						
79	9.10						:/ ::		$13 4.59 \\ 14 23.20$	$10.72 \\ 10.69$	" 2 31.76 " 6 33.67	49 33.03 19 15.71	$\begin{array}{c} 4.75 \\ 4.73 \end{array}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	27 48 27.78 z. 27 18 10.44 z.
80	9.10		1 [.7		23 15 11.80	10.68	" 7 32.76	13 56.18	4.73	23 15 22.48	27 18 10.44 z. 27 12 50.89 z.
į	- 1			<u> </u>								22 30.20		20 20 20 10	22 30.00 2.

Number.)OI1.		<i>)</i>	LKAI	NSIT	S.		m			ъ		Mean Right	Mean South
	Magnitude.	Ι.	11.	ш.	ıv.	v.	V1.	vII.	10.	11.	Т.	a.	MICROMETER.	D.	d.	Ascension, 1850.0.	Declination, 1850.0.
			Zo	ne L	XII	•	Sept	embe	r 15.	ľ	D = -	26 58 50.0	0. $n' = -20'$		- 7.00.	(Continued.)	
81	10		38.05	50.0	2.0		27.0	39.5			$\begin{array}{cccccccccccccccccccccccccccccccccccc$	+10.66	VII. 5 47.00	—2 6 1777	- 4.64	h. m. s. 23 18 13.01	27 19 12.41 z.
82	9				36.5	49.0	1 1	• •			19 36.62	10.65	V. 4 37.99	31 16.38	4.61	19 47.27	27 30 10.99 z.
83	$\frac{9}{9.10}$	• •	• •	• •	· · · 48.0	• •	$\frac{12.7}{12.7}$	1	43.15	1	$20 7.70 \\ 26 47.94$	10.64 10.59	11. 6 36.30 VI. 2 38.12	17 44.31 45 53.59	$4.60 \\ 4.52$	20 18.34 26 58.53	27 6 38.91 27 44 48.11
84 85	9.10 7				- 1		$\frac{12.7}{30.5}$				28 5.65	10.59	VII. 2 36.12 VII. 2 42.44	43 24.20	4.52	28 16.22	27 42 18.70
86	8.9	1 1	54.3	1	- 1						32 19.34	10.53	IV. 2 40.94	44 16.28	4.47	32 29.87	27 43 10.75
*87	7	52.4	5.01	[7.3]	30.0			$ \cdot\cdot $		٠ .	36 29.66	10.47	III. 7 47.90	5 13.60	4.45	36 40.13	27 4 8.05
88	9	$ \cdot\cdot $		• •	$\cdot \cdot $	• •		9.8	1	٠ ٠	36 32.81	10.48	VII. 5 48.55	19 24.20	4.45	36 43.29	27 18 18.65 z.
89 90	$8.9 \\ 8.9$		- 1				27.4	40.0		4.0	38 2.74 $38 25.82$	10.47 10.47	" 2 48.18 11. 1 49.98	40 5.92 44 54.65	4.44	38 13.21 38 36.29	27 39 0.36 z. 27 43 49.09 z.
				1		1				1.0							
91	7 9		1		$24.7 \\ 39.6$	37.0	1 1	16.8			46 24.83 47 39.64	10.41 10.38	V. 1 34.60 VII.5 34.78	53 46.77 27 19.82	4.48	$\begin{array}{c} 46 \ 35.24 \\ 47 \ 50.02 \end{array}$	27 52 41.25 z. 27 26 14.31
92 93	6		1				38.0			\Box	49 12.99	10.36	VII. 3 34.18 VI. 4 42.68	28 34.30	4.43	49 23.35	27 27 28.80 z.
94	9]				• •		3.0	49 14.84	10.36	11. 2 46.07	41 18.17	4.50	49 25.20	27 40 12.67 z.
95	7						0.8	13.0	• •	٠ ٠	52 35.95	10.33	VII. 5 43.05	22 34.20	4.56	52 46.28	27 21 28.76
96	5		57.5			$34.0 \\ 45.0$		• •		• •	54 22.00	10.32 10.31	V. 4 36.92 " 6 39.23	31 53.35 16 4.01	4.60 4.62	54 32.32 55 43.59	27 30 47.95 27 14 58.63 z.
97 98	5 3		$\begin{array}{c c} \cdot \cdot & 2 \\ 19.03 \end{array}$								55 33.28 0 3 43.88	10.31	III. 1 37.76	16 4.01 51 57.64	4.82	0 3 54.03	27 14 58.63 Z. 27 50 52.46
99	6			J	- 1		38.8	! !	- 1		4 14.07	10.23	VI. 2 40.60	44 27.91	4.84	4 24.30	27 43 22.75 z.
100	7							25.4			4 48.28	10.22	VII.2 43.73	42 39.60	4.85	4 58.50	27 41 34.45 z.
101	9							١١	23.63	6.0	5 28.31	10.22	11. 7 38.49	10 37.70	4.87	5 38.53	27 9 32.57 z.
102	9							$ \dots $	- 1	5.1	6 57.50	10.21	" 7 42.64	8 14.34	4.92	7 7.71	27 7 9.26
103	6				44.5		9.3	[I			12 44.58	10.16	VI. 7 41.46	8 55.97	5.14	12 54.74	27 7 51.11
104	7	$ \cdot\cdot $	1	• •	• •	٠.		58.8		• •	13 21.94	10.15	VII. 7 45.26	6 44.51	5.16	13 32.09	27 5 39.67 z.
$\begin{array}{c} 105 \\ 106 \end{array}$	$\frac{7}{3}$		12.02	04 1	 36 3	• •	2.8	15.2		٠ . ا	14 38.02 16 36.59	10.14 10.12	" 1 37.71 III. 1 36.26	51 59.08 52 49.47	5.22 5.31	14 48.16 16 46.71	27 50 54.30 z. 27 51 44.78 z.
107	7						12.7	([16 47.88	10.12	VII. 2 38.00	45 57.52	5.32	16 58.00	27 47 52.84 z.
108	3		3.11	15.5			52.6				21 27.82	10.08	III. 1 38.60	51 28.60	5.55	21 37.90	27 50 24.15 z.
109	7			• •		37.0	1	2.0	1	٠.	28 24.83	10.03	VII.3 41.26	35 19.68	5.91	28 34.86	27 34 15.59
110	7	• •	• •	• •	• •	• •	• •	38.0	• •	٠ ٠ ا	28 0.88	10.03	" 2 44.72	42 5.40	5.89	28 10.91	27 41 1.29 z.
111	9		- 1					$ \cdot\cdot $	4	4.0	28 35.88	10.02	11. 3 39.61	36 16.00	5.93	28 45.90	27 35 11.93 z.
112	$\frac{2}{2}$	1 1	56.3	- 1			45.5		1	٠ .	32 20.99	9.99	2. 4 37.67	31 26.76	6.16	32 30.98	27 30 22.92
113 114	$\begin{vmatrix} 2 \\ 2 \end{vmatrix}$	1 1	25.03 44.45				14.6		1	٠ ٠ ا	$36 \ 49.77$ $40 \ 9.50$	$9.96 \\ 9.93$	" 5 44.56 II. 1 43.21	21 41.63 48 49.33	6.47	36 59.73 40 19.43	27 20 38.10 z. 27 47 46.03 z.
115	7						1				40 59.85	9.92	VII. 6 45.51	12 26.81	6.77	41 9.77	27 11 23.58 z.
116	2	1	24.0 3	36.0	48.2		12.8	25.4			44 48.35	9.89	2. 6 43.30	13 42.80	7.07	$44\ 58.24$	27 12 39.87 z.
117							2.3			٠ ٠	48 37.69	9.86	VII. 7 38.52	10 37.24	7.37	48 47.55	27 9 34.61
118		• •					36.0	1 1		٠ ٠ ا	58 11.13	9.79	2. 2 37.60	46 10.94	8.23 8.36	58 20.92 59 42.33	27 45 9.17 27 31 52.53
$\frac{119}{120}$	9		0.5				$57.3 \\ 49.7$				59 32.55 1 0 24.96	9.78 9.78	" 4 35.14 VII. 1 43.96	32 54.17 48 23.19	8.44	1 0 34.74	27 47 21.63
																4 59.96	27 6 53.10
*121 122	$9 \\ 9.10$		26.3				14.0	1		٠.	$\begin{array}{c} 4 \ 50.21 \\ 6 \ 20.74 \end{array}$	9.75 9.73	10. 7 43.23 11. 6 40.50	7 54.23 15 19.26	8.87 9.01	4 59.96 6 30.47	27 14 18.27
123			1							: : 	10 18.56	9.69	2. 1 42.36	49 18.10	9.41	10 28.25	27 48 17.51
	9						48.0				11 23.49	9.69	6 34.04	19 3.27	9.53	11 33.18	27 18 2.80 z.
125		• •					• •				14 26.27	9.67	V. 4 43.11	28 19.54	9.87	14 35.94	27 27 19.41 z.
	9					- 1	40.0			0.5	14 52.41	9.67	11. 3 46.27	32 26.02	9.92	15 2.08 18 25.16	27 31 25.94 27 13 47.34
*127 128	$\frac{9}{7}$		31.1		i	- 1					18 15.52 20 48.08	$9.64 \\ 9.62$	2. 6 41.44 VII.1 33.39	14 47.04 54 28.33	10.30 10.60	20 57.70	27 13 47.34 27 53 28.93 z.
129	8.9		24.33						1		20 48.88	9.61	" 2 38.26	45 48.55	10.84	22 58.49	27 44 49.39
130			43.05								25 7.25	9.60	" 6 31.80	20 20.31	11.13	$25\ 16.85$	27 19 21.44 z.
131	10	4.0	16.42	8.5	41.0		5.2	17.0			34 40.75	9.55	" 7 39.91	9 49.25	12.38	34 50.30	27 8 51.63
	7.8	29.5	4.23	34.0							38 6.49	9.53		7 45.18	12.86	38 16.02	27 6 48.04 z.
133	9.10										38 26.10	9.53	VII.7 39.68	9 57.18	12.90	38 35.63	27 9 0.08 z.
134			8.82						- 1	٠٠	40 33.56	9.50	" 4 39.81	30 13.24	13.20	$\begin{array}{c} 40 \ 43.06 \\ 1 \ 42 \ 21.10 \end{array}$	27 29 16.44 z. 27 48 56.00
135	9	$ \cdot\cdot $	• •	• •	11.5	24.0	36.5	• •	• •	٠٠	1 42 11.62	9.48	VI. 1 41.38	49 52.54	13.46	1 42 21.10	&1 40 JU.UU



er.	itude.		SE	CON	NDS (OF	TRA	NSI'.	rs.						-		1	ean Right	1	n So	
Number.	Magnitude.	1.	11.	ш.	ıv.	v.	vi.	vII.	10.	11.	Т.	a.	MI	CROMETER.	D.	d.		Ascension, 1850.0.		clinat 50.0.	ion,
					Zor	ne L	XIII.	•	Septe	embei	т 16. Н.	D = -	-27 26	00.0. n.=	=-33.00.	n'. ==-	_3.18.				
1	5			9.3	22.0	34.2	246.6	59.0			h. m. s. 18 57 21.85	+12.5	32 IV	r. 5 35.953	$-26^{'}35^{''}.79$	-28.5	21 18	h. m. s. 8 57 34.17	27° 53	2 4" (00 7
2	9		1		1 1		15.8				19 0 50.89	12.3			29 55.65	27.		$\frac{1}{2}$ 1 3.19	27 56		
3	8	1					42.5				1 17.55	12.3	34 V	. 1 35.823	53 0.78	27.		1 29.89			
4	9			14.5	27.2	40.0	52.2				$2\ 27.30$	12.3	32 IV	. 2 35.250	47 29.08	26.3	33	239.62	28 13	3 55.9	91
5	8.9	1			56.5			ı			4 56.64	12.5		. 6 37.115	17 13.11	26.	16	5 8.89	27 43	39.2	27
6	8.9		1	1	1 1		931.5		ı		5 6.70	12.5		7 43.190	7 52.27	26.		5 18.93	27 34		
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8	9		1		1		21.5	1	• •	• •	8 56.64	12.9		3 36.368	38 5.12	25.	¥	9 8.89		30.2	
9 10	$\frac{8.9}{9}$	1	$37.3 \\ 31.0$.1 1		427.0		• •		11 2.12 13 55.99	12.5		7. 1 41.180	49 55.80	24		11 14.38	28 16		
IO	9	19.0	31.0				• •	İ	• •	• •	15 55.99	12.	10 1	. 6 35.244	18 17.74	23.	15	14 8.17	27 44	1 41.4	49
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13	8.9	1					45.0				20 19.73	12.	1	6 35.790	17 58.86	22.		20 31.85			
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17	9.8				1		231.5				23 6.75	12.		I .	51 46.08	21.	H	23 18.92			
18	9									20.5	23 12.07	12.		1 37.307	32 20.31	21.5	8	23 24.20	27 58		
19	9										25 39.44	12.0		5 47.543	19 55.44	20.	8	25 51.52	1		
20	9				1 1		27.0			1	26 2.08	12.1		I	30 52.27	20.	1	26 14.18	27 57		
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22	9	: :		14.0	1		8.6		• •	• •	27 43.70	12.0		3 44.220	23 18.80 33 33.84	$\frac{20.1}{20.1}$	•	27 39.44 27 55.79	27 49		
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25	9				1 1		254.5				30 29.83	12.0		1	26 2.67	19.	2	30 41.89			
26	9				3.0	15.0	27.5				31 2.83	12.0)3 "	1	11 54.15	19.	8	31 14.86		3 13.3	
27	8			· •			43.5	56.0			31 18.65	12.0)7 VI	I. 3 40.292	35 49.31	19.	15	31 30.72	28 2	8.4	46 z
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29	9		1		1 1		1 12.0			٠.	35 46.93	12.0	1	0 0 2 1 1 1 0 0	18 51.84	17.	1	35 58.93			
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31	8.9						48.6				37 23.76	12.0)3 II]	. 3 35.941	39 28.94	17	55	37 35.79	28 5	46.4	49
32	8.9	27.0	39.0	51.5			• •				41 3.96	11.9		. 6 46.082	12 3.39	16.		$41\ 15.90$			
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34	7.8						8.0			٠ ٠	41 43.29	11.9		5 39.516	24 32.65	16.	8	$41\ 55.25$	1		
35	9								• •	٠ ٠ ا	46 34.44	11.9		5 36.602	26 13.31	15.5		46 46.36	l l		
36 *37	9						30.5		• •	٠٠.	47 5.48 47 9.31	11.9		7. 6 35.520 3 42.358	18 8.27 34 37.95	15.		47 17.38 47 21.24			
38	$\frac{3}{5.6}$						1 56.5		• •	٠.	47 31.98	11.8	ı	7 43.816	7 30.73	15.0 14.9	i i	47 21.24			
39	8.9						9.6				49 44.51	11.8	8	6 45.280	12 31.20	14.		49 56.37	27 38		
40	9						12.2				50 47.56	11.9		3 39.615	36 12.96	14.	8	50 59.46			
41	9	1	1		1		2				19 51 28.80	11.8		7 41.250	8 59.38	14.	1	51 40.64			
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42 43 44 45 46 47	5.6 9 8 8.9 9	55.9 32.0	35.8 27.2 7.5 044.1	48.0 39.5 20.0 56.5	$0.41 \\ 52.2 \\ 32.54 \\ 9.0$	26.0 38 12.5 25 4.5 16 14.5 37 34 63.4 6	.5 .8 .0 .0 .0	.1		h. m. s. 19 53 13.5 55 0.4 55 52.0 57 32.3 20 0 9.1	$egin{array}{c ccc} 1 & +15 \\ 7 & 15 \\ 8 & 15 \\ 0 & 15 \\ 1 & 15 \\ \end{array}$	88 87 79	TV. 2 46.300 HI. 2 42.038 IV. 1 45.030 " 6 44.964 " 2 43.890	-41 7".39 43 34.55 47 42.80 12 42.10 42 30.60	-1358 1315 1293 1253 1188	19 5 5 5 5 20	m. s. 3 25.40 5 12.35 6 3.95 7 44.09 0 20.93	28 28 1 27 3 28	7 20".9 9 47.7 3 55.7 8 54.6 8 42.4	70 z. 73 z. 63 48
48 49 50 51 52	9 9 9 9	51.5	$\begin{bmatrix} . & . \\ 47.2 \\ 2 & 3.8 \\ 1.5 \\ 39.5 \end{bmatrix}$	59.0 15.5 14.0	$egin{array}{c} 1.1 & 2 \\ 12.1 & 2 \\ 28.5 & 26.5 \\ 4.0 & \end{array}$	23.5 36 24.4 37 	.1 . .2 49 .2 . .8 41	. 6 . 6 		$egin{array}{c} 0 & 41.4 \\ 2 & 11.3 \\ 7 & 12.1 \\ 10 & 28.3 \\ 11 & 26.4 \\ 13 & 4.0 \\ \end{array}$	4 13 7 13 8 13 1 13	1.82 1.76 1.75 1.69 1.68	" 2 45.240 " 6 32.511 " 3 37.590 " 5 43.180 10. 5 43.730 IV. 2 38.105	41 44.00 19 52.19 37 22.91 22 26.17 22 6.46 45 50.45	11.75 11.40 10.19 9.41 9.18 8.80	· 1	0 53.23 2 23.10 7 23.92 0 40.07 1 38.09 3 15.72	27 4 28 27 4 27 4	$egin{array}{cccc} 7 & 55 & 5 & 5 & 5 & 5 & 5 & 5 & 5 & 5 $	59 z 10 z 58 64 z
53 54 55 56 57 58	9 8.9 8.9 8.9 8	30.4 44.6 29.5 59.6	36.4 43.0 57.2 242.0 512.5	48.5 55.2 9.5 54.0	$egin{array}{c} 1.01 \\ 7.31 \\ 22.03 \\ 6.81 \\ 37.0 \\ \hline \end{array}$	$ \begin{array}{c} 0.332 \\ 34.046 \\ 9.031 \\ \end{array} $. 1	.0 .		14 46.1 18 1.1 19 7.4 20 21.8 22 6.7 24 36.9	7 11 5 11 5 11 5 11 1 11 9 11	68 63 60 60 63	" 3 38.520 " 4 40.432 " 5 47.380 " 5 43.388 " 1 43.189 II. 6 42.015	36 50.78 29 48.28 20 1.12 22 19.00 48 46.41 14 23.86	8.40 7.63 7.37 7.09 6.68 6.12	1 1 1 2 2 2	4 57.85 8 12.78 9 19.05 0 33.45 2 18.34 4 48.53	28 1 27 5 27 4 27 4 28 1 27 4	2 59.1 5 55.9 6 8.4 8 26.0 4 53.0 9 29.9	18 91 49 09 z 09 z
59 60 61 62 63 64	9 8 9 7.8 8 9	2.6	56.0 56.0	 27.5 8.2	29.6 4 47.5 40.0 5 20.5 3		.5 6 .4 25 .8 58 .3 16	.6 .4		24 43.1 25 29.6 28 47.6 30 40.0 31 20.7 32 39.4	1 11 7 11 5 11 2 11 1 11	.53 .54 .57 .54 .52 .47	IV. 7 38.956 V. 5 50.382 IV. 1 35.370 " 1 43.888 " 3 31.812 VII. 6 34.610	10 18.59 18 17.40 53 16.51 48 22.25 40 42.50 18 39.39	6.09 5.92 5.17 4.74 4.60 4.30	2 2 3 3	4 54.70 5 41.15 8 59.24 0 51.59 1 32.24 2 50.88	27 4 28 1 28 1 28 1	6 24.6 4 23.3 9 21.6 4 26.9 6 47.1 4 43.6	32 z 58 z 99 z 10 z
65 66 67 68	9 9 9 7.8	31.6		2.2	$\begin{vmatrix} 16.0 \\ \cdot \end{vmatrix}$	8.2 48 25		. 2 .		35 14.60 35 15.9° 35 23.70 20 36 0.54	7 11 3 11	.44 .47 .44	II. 6 34.208 IV. 6 40.900 " 4 36.032 " 5 45.462	18 53.52 15 2.47 32 20.24 21 7.37	3.73 3.73 3.70 3.57	3	5 26.10 5 27.41 5 35.23 6 11.98	27 4 27 58	4 57.2 1 6.2 8 23.9 7 10.9	20 94 z
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1 2 3 4 5 6 7	8 9 7.8 7 8.9 7.8		18.5 2.2 21.0 56.0	33.0 16.2 35.2 2.0 10.5	$31.04 \\ 50.1 \\ 16.53 \\ 25.03$	$egin{array}{cccc} 2.0 & 16 \ 5.2 & . \ 4.2 & 19 \end{array}$.4 .			21 50 35.2 56 47.56 22 1 30.93 1 49.99 5 16.66 7 24.96 22 10 13.48	11 3 11 2 11 5 10 0 10	.23 .10 .03 .02 .96 .94 .89	IV. 5 37.965 " 7 42.244 " 7 40.330 " 7 37.452 " 7 45.352 " 7 38.274 V. 7 35.423	25 33.27 8 25.55 9 32.09 11 12.16 6 37.56 10 43.53 12 22.60	4.12 3.76 3.50 3.48 3.32 3.22 3.08	22 3 3	0 46.48 6 58.60 1 41.96 2 0.94 5 27.61 7 35.84 0 24.37	40 58 40 59 41 0 40 56 41 0	5 17.3 8 9.3 9 15.5 9 55.6 9 26.7 2 5.6	31 59 54 88 75
]	<u>-</u>	C	ORREC	TION	s.	1		1			INSTRU	MENT RE					
			cor.		HOURLY	Y m		n.	c.	ZENITH POINT.	COINC.			Δ.	B. C	1	Mean.	BAR.	At.	Ex.
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er.	tude.		SE	CON	NDS	OF	TR	ANS	ITS	•	m			D.	d.	Mean Right Ascension,	Mean South
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8	8.9		44.0	58.2	13.	027.	241	.8 .			h. m. s. 22 18 12.85	+10.77	r. IV. 5 42.439	-22 ['] 57 ^{''} .84	— 2 ["] .79	h. m. s. 22 18 23.62	41° 12′ 40″.63
9	9			2.4					- 1		20 17.08	10.72	" 6 45.470	12 26.66	2.71	20 27.80	41 2 9.37
10	9		24.0				0 23	.0	$\cdot \cdot$		25 53.57	10.64	" 5 48.325	19 33.15	2.57	$26 ext{ } 4.21$	41 9 15.72
11	9		35.0	48.8				- 1	i		27 3.73	10.62	" 6 40.126	15 32.33	2.54	27 14.35	41 5 14.87
12	7		• •	1	1	- 1	1	0.015 0.545	- 1	.	27 31.79 28 1.41	10.61 10.62	" 6 37.680 VI. 4 36.722	16 57.23 32 5.68	$2.53 \\ 2.52$	27 42.40 28 12.03	41 6 39.76 41 21 48.20
$\frac{13}{14}$	7 7.8			$\frac{47.2}{24.0}$					- 1		34 38.81	10.48	IV. 7 48.150	5 0.27	2.40	34 49.29	40 54 42.67
15	7.8	1		43.5	1				1		35 58.36	10.50	" 2 42.584	43 29.78	2.37	36 8.86	41 33 12.15
16	8			1.2					-		46 15.88	10.34	" 1 34.906	53 51.05	1.64	$46\ 26.22$	41 43 32.69
17	9		3.0	17.0	31.	5 .	. 1	.0	. .		54 31.74	10.17	" 7 37.270	11 18.43	0.73	54 41.91	41 0 59.16
18	7	١	25.0	39.8	55.	$0 \mid 9$	224	.0	. .		54 54.65	10.18	" 1 45.380	47 46.77	0.68	55 4.83	41 37 27.45
19	9							.0 5		1	55 21.36	10.18	" 1 45.322	47 48.77	0.63	55 31.54	41 37 29.40
20	9	5	34.0						- 1		58 2.81	10.11	" 6 38.338	16 34.55	0.32	$58\ 12.92$	41 6 14.87
21	9							.4			23 0 17.71	10.08	" 6 41.390	14 48.47	0.10	23 0 27.79	41 4 28.57
22	7		1	1		i	- 1	.5			1 37.26	10.06	" 3 42.920	34 29.29	0.12	1 47.32	41 24 9.41 в.
23	9	1		1	1	1	1	.0		$\cdot \cdot \cdot$	6 6.72	9.99	" 5 37.980 " 3 34.681	25 32.75	0.18	6 16.71	41 15 12.93
24	9	• •	1	1		- 1	- 1	.2	- 1		7 49.79 9 42.01	$9.97 \\ 9.94$	" 3 34.681 " 1 43.785	39 15.77 48 42.09	$0.21 \\ 0.24$	759.76 951.95	41 28 55.98 41 38 22.33 в.
$ \begin{array}{c c} 25 \\ 26 \end{array} $	6 9		1	1		- 1	Ļ	.2 .	- 1		13 50.23	9.86	" 4 39.300	30 36.43	0.24	14 0.09	41 20 16.72
27	9							.2			16 22.93	9.82	VI. 5 40.010	24 21.92	0.32	16 32.75	41 14 2.24
												0.77		14 40.95	0.36	19 27.04	
28 29	8.9	• •						.2 .			19 17.27 21 28.32	$9.77 \\ 9.73$	IV. 6 41.600 III. 7 35.050	12 35.46	0.35	21 38.05	41 4 21.31 41 2 15.81
30	9	• •						.2			21 50.97	9.73	IV. 6 35.400	18 16.70	0.34	22 0.70	41 7 57.04
31	8.9			1		- 1		.0	1		24 57.35	9.69	" 1 40.150	50 48.67	0.29	25 7.04	41 40 28.96
32	9			1	1		i	.1 .			28 16.32	9.62	" 7 39.600	9 57.27	0.23	28 25.94	40 59 37.50
33	9		41.0					.5			34 9.85	9.53	" 6 33.343	19 28.20	0.14	34 19. 3 8	41 9 8.34
34	7		36.0								36 5.06	9.50	" 2 46.075	41 28.49	0.12	36 14.56	41 31 8.61
35	6.7							.6			37 55.66	9.46	" 7 37.312	11 16.98	0.09	38 5.12	41 0 57.07 в.
36	9							.3			41 29.25	9.42	" 5 42.270	23 3.66	0.07	41 38.67	41 12 43.73
37	9	37.5	52.1	6.6	21.	5					43 21.38	9.39	" 4 41.160	29 31.71	0.07	43 30.77	41 19 11.78
38	9							.527			43 43.13	9.39	" 1 41.526	50 0.59	0.07	43 52.52	41 39 40.66 в.
39	9			1	1	- 1		$\cdot 0$			45 19.18	9.36	" 3 41.604	35 14.96	0.08	45 28.54	41 24 55.04
40	6			1				.2 .	ì		46 35.89	9.34	" 6 34.806	18 37.18	0.09	46 45.23	41 8 17.27 в.
41		1	1	1		- 1	- 1		- 6		52 19.60 52 39.40	9.24	" 7 36.120 VI. 2 45.285	11 58.37 41 55.79	$\begin{array}{c} 0.13 \\ 0.13 \end{array}$	52 28.84 52 48.64	41 1 38.50 м. 41 31 35.92
42 43	7 7.8	::	l .	1	1			$\begin{array}{c c} .0 & 23 \\ .0 & 33 \end{array}$	- 1		53 49.13	9.24	IV. 7 40.478	9 26.98	0.13	53 58.35	41 31 35.92 40 59 7.12 в.
44	9		1	1			- 1				59 11.21	9.14	" 5 38.344	25 20.20	0.20	59 20.35	41 15 0.40
*45	9							.3 18			59 34.90	9.13	" 4 41.570	29 17.28	0.20	59 44.03	41 18 57.48
46	8.9							.3 .			0 0 1 00	9.08	" 1 35.013	53 47.36	0.26	0 2 10.34	41 43 27.62
47	8			18.0	33.	0 47	.2 2	.1 16	.3		3 32.78	9.07	V. 5 42.708	22 48.21	0.29	3 41.85	41 12 28.50 в.
48	9		50.5	5.0	19.	0.			5 19.40	9.05	IV. 5 41.780	23 20.57	0.34	5 28.45	41 13 0.91
49	9				1		- 1	.4	- 1		5 45.98	9.04	" 5 44.032	22 2.34	0.35	5 55.02	41 11 42.69
5 0	9				43.	2 58	.0 12	.2 26	.5 .		6 43.10	9.02	" 5 37.656	25 43.93	0.37	6 52.12	41 15 24.30
51	8		• •		1			.3 32	\cdot 0 .			9.01	" 4 44.602	27 31.86	0.40	7 57.15	41 17 12.26 в.
52	8										10 56.83	8.97	" 7 44.750	6 58.32	0.49	11 5.80	40 56 38.81
53	7.8			27.0							11 41.75	8.96	" 7 44.738 " 2 48.464	6 58.73	0.52	11 50.71	40 56 39.25
54 55	7.8	• •		137.5		- 1		.0	- 1		$\begin{array}{c} 21 \ 52.37 \\ 22 \ 56.11 \end{array}$	8.78 8.77	V. 4 43.980	$\begin{array}{ c c c c c }\hline 40 & 5.51 \\ 27 & 53.53 \\ \hline \end{array}$	$0.94 \\ 0.99$	22 1.15 23 4.88	41 29 46.45 в. 41 17 34.52
55 56	$\frac{9}{8.9}$			1			1	.0	- 1		25 56.43	8.72	1	43 37.77	1.14	26 5.15	41 33 18.91
57	9		1	1	1	1	- 1	.0	- 1		27 32.07	8.72	" 7 38.610	10 31.69	1.14	27 40.79	41 0 12.91
			ļ.					- 1									
58 50	9)	3	1	1		- 1	$.0 13 \\ .8 59$	- 1	3	30 29.78 0 31 15.56	8.66 8.65	1 11.00~	29 16.18 28 18.37	1.37 1.42	30 38.44 0 31 24.21	41 18 57.55 41 17 59.79
59	9	J.Z. C	40.2	0.0	13.	200	.0 44	.009			0 51 15.50	0.03	4 40.210	~O 10.01	1.42	0 31 24.21	41 11 05.19
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ber.	Magnitude.		SE	CON	IDS (OF 7	rrai	ISIT	rs.		т.	a.		MICROMETER.	D.	d.	Mean Asce	Right		n Sou	
Number.	Mag	ı.	n.	ш.	ıv.	v.	vı.	vII.	10.	11.							1850	.0.	1850	0.0.	
1 2	8 9			35.0	51.4 48.0	4.0 59.8	LXV 16.1 12.2			ember	16. H. h. m. s. 1 30 51.41 31 47.53	+ 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	.64 .63	IV. 4 39.080 " 4 36.012	==-15.56. -30 36.79 32 22.76	n."=	h. m 1 31 31	. s. 0.05 56.16	2 [†] 59 28 0	56.89	9 z.
3 4 5 6	9 9 9 8.9		 3 13 .0	$\begin{vmatrix} . & . \\ 25.3 \end{vmatrix}$	37.5 29.5	$10.5 \\ 49.2$	23.0	36.0	• •	• •	33 45.96 33 58.43 36 37.55 38 29.44	8.	.63 .62 .61	" 6 38.656 " 6 35.490 " 6 37.440 II. 2 36.170	16 21.68 18 11.09 17 3.73 46 59.12	13.87 13.84 13.50 13.25	34 36	54.59 7.05 46.16 38.01	27 44 27 46 27 45 28 15	$\frac{44.93}{37.23}$	3 3
7 8 9 10	7 9 9			44.0	1	8.4 25.2	20.3				38 56.12 40 50.77 42 12.97 42 46.62	8.8		IV. 3 588 " 5 37.672 " 5 46.933 " 5 40.500	25 38.20 20 18.28 24 0.55	13.19 12.93 12.75 12.67	39 40 42	4. 59.34 21.53 55.18	27 54 27 48 27 55	11.13 51.03	3 3
11 12 13 14 15	9 9 9 8 9	1.	33.6 16.8 5 13.6	646.0 829.0 626.0	58.5 41.6 38.5 53.8	10.5 54.0 51.0		25.8 			42 48.66 44 58.33 45 41.59 49 38.58 50 53.71	8 8	.56 .54 .54 .52	" 6 38.126 " 5 42.710 " 4 39.115 " 1 42.255 " 6 34.662	16 40.02 22 44.15 30 35.58 49 18.13 18 39.64	12.66 12.36 12.26 11.71 11.52	45 45	57.22 6.87 50.13 47.10 2.22	27 45 27 51 27 59 28 17 27 47	16.55 7.84 49.84	1 z. 4 4 z.
16 16 17 18 19 20	9 9 9			241.0	2.5	10.8 14.6 47.5 2.6	$\begin{array}{c} \cdot \cdot \cdot \\ 23.0 \\ 527.5 \\ 60.0 \\ 14.1 \\ 33.6 \end{array}$	 12.5			50 58.43 52 2.46 52 35.14 52 49.43 54 8.56	8 8 8 8	.51 .50 .49 .49	" 7 36.811 " 4 39.602 " 2 37.170 VII.2 42.256 IV. 1 38.545	11 34.37 30 18.73 46 24.68 43 28.67 51 28.81	11.32 11.51 11.35 11.26 11.23 11.02	51 52 52 52	6.94 10.96 43.63 57.92 17.04	27 40 27 58 28 14 28 11 28 19	5.88 50.08 55.94 59.90	8 z. 8 4 0
21 22 23 24 25 26 27 28 29 30	7.8 9 9 8.9 8.9 9 8 7.8 8	27. 54. 56.	38.3 53.0 56.3 7.0 8.4 4.28.4	2 50 .5 5 52 .6 0 5 .5 2 8 .8 0 19 .5 4 20 .5 8 41 .5	5 5.6 $5 17.8 $ $5 17.8 $ $5 21.2 $ $5 31.5 $ $5 32.6$	31.6 17.5 30.6 33.2 43.6 45.4	3 43.5 6 30.2 9 42.3 1 5 56.4 1 58.0 1 18.5 5 2.5	8.8 10.6 30.8			2 1 13.77 2 3.02 2 18.90 4 5.27 5 17.76 8 21.11 13 31.64 15 33.25 17 53.72 19 27.14	8 8 8 8 8 8 8 8 8	.44 .43 .43 .41 .40 .38 .36 .35	" 2 43.542 " 3 35.250 " 1 43.010 " 4 45.150 " 2 40.421 " 2 48.110 " 4 41.610 " 7 36.090 " 5 46.221 VII. 3 35.702	42 44.51 38 45.63 48 54.52 27 7.10 44 32.38 40 6.74 29 9.36 11 59.30 20 42.90 38 29.68	9.92 9.79 9.75 9.46 9.27 8.78 7.92 7.57 7.17 6.90	2 2 4 5 8 13 15	22,21 11,46 27,33 13,70 26,17 29,51 40,02 41,63 2,08 35,49	28 11 28 7 28 17 27 55 28 13 28 8 27 57 27 40 27 49 28 6	15.42 24.2 36.5 1.6 35.5 37.2 26.8 10.0	2 z. 7 6 z. 5 z. 2 8 z. 7
31 32 33 34 35 36 37	9 8.9 9 8 7.8 9	10. 6.	5 55. 5 22. 0 18.	$\begin{bmatrix} 7.9 \\ \\ 8 \end{bmatrix} 35.0 \\ 31.0 \\ \end{bmatrix}$	220.0 27.5 047.6 043.5	39.8 0.0 55.2 32.0	52.6	$\begin{array}{c} \\ 4.6 \\ \\ \\ 56.2 \end{array}$			20 42.44 22 19.86 22 27.52 24 47.69 25 43.23 26 19.27 2 29 14.97	8 8 8 8 8	.33 .33 .31 .33 .31	III. 3 39.980 V. 4 45.201 IV. 2 45.411 " 7 37.136 VI. 4 45.540	49 25.51 36 2.19 27 5.31 41 39.99 11 23.16 26 53.49 20 57.48	6.69 6.40 6.38 5.96 5.80 5.69 5.16	22 22 24 25 26	50.77 28.19 35.85 56.00 51.56 27.58 23.27	28 17 28 4 27 55 28 10 27 39 27 55 27 49	28.59 31.69 5.99 48.99 19.18	9 9 5 z. 6 z. 8
						COR	RECT	IONS							INSTRU	MENT RE	ADINGS				
			<u> </u>			1		1							12.02110	CIRCLE.				THER	mom.
				ock.	HOU	- 1	m.		n.	c.	ZENITH POINT.	COINC.			Α.	в. с	. р.	Mean.	BAR.	At.	Ex.
Sept.	16, at	22h	+	s. 1.622	s		s. -0.356	+0	.527	+0.022	o° o′ 2″.56	r. 40.094	†Z	Zone h. XV.—Sept. 161.5		11.8 19.		10 ["] /72	30.100	58.°4	52.3 50.5
	†The	readi	ng of	the cir	rcle ha	s beer	n chang	ged th	ree m	inutes f	rom that record	ed.		2.5		1 5			30.074		50.7

Number	Magnitude.	1.	SEO	CON.	DS O)F T	RAN	VII.	'S.	11.	т.	a	•	MICROMETER.	D.	d.	Mean Right Ascension, 1850.0.	De	an Sor eclination	
					Zon	e LX	CVI.	s	Septer	nber	19. M.	D. =	25° 2	25 10.0. n. =	—42 ["] .84. r	=-3.00).			
14 15 16 17 18 19 20 21 *22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39	8.9 9.10 9.10 9.10 10 9.10 10 9.10 10 8 8.9 9.10 10 88.9 9.10 10 9.10 10 88.9 9.10 10 88.9 9.10 10 88.9 9.10 10 88.9 9.10 10 88.9 9.10 10 88.9 9.10 10 88.9 9.10 10 88.9 9.10 10 88.9 9.10 10 88.9 9.10 10 88.9 9.10 10 88.9 9.10 10 10 9.10 10 10 10 10 10 10 10 10 10	46.22 14.55	57.0 58.8 27.1 49.0 14.0 27.5 36.0 32.7 27.0 21.0 	9.2 10.6 39.5 1.0 25.7 9.4 40.0 25.5 47.8 29.8 24.0 53.8 	23.0 51.6 13.2 38.0 21.1 52.0 0.6 0.6 37.6 6.5 6.5 51.0 37.0 44.0 45.0 45.0 45.0 46.0 45.0 46.0 46	35.0 3.7 20.0 33.2 4.5 58.0 9.0 19.0 19.0 5.4 4.5 66.0 68.0 18.0 18.0 18.0 18.0	43.5 12.6 47.1 15.8 37.0 32.0 10.0 2.3 46.0 2.3 10.0 2.3 10.0 27.5 8.1 10.2 7.3 9.3 8.1 10.2 7.3 9.3 8.1 10.2 7.3 9.3 8.1 10.2 7.3 9.3 8.1 10.2 7.3 9.3 8.1 10.2 7.3 9.3 8.1 10.2 7.3 9.3 8.1 10.2 7.3 9.3 8.1 10.2 7.3 9.3 8.1 10.2 7.3 9.3 8.1 10.2 7.3 9.3 8.1 10.2 7.3 9.3 8.1 10.2 8.1 10.	24.8 59.5 28.0 49.4 	23.8	27.6	A. m. s. 19 26 41.99 29 28.90 35 53.38 36 19.00 38 21.37 38 48.13 42 22.91 43 51.48 48 13.06 50 38.17 51 7.57 51 20.29 52 50.38 57 21.36 59 52.05 20 0 45.57 0 53.58 4 37.74 7 0.30 9 42.21 10 36.14 11 15.94 14 56.83 17 6.76 18 51.22 21 37.24 20 43.51 22 19.62 25 5.91 26 2.95 27 43.84 28 45.90 29 42.81 31 45.15 36 56.74 37 2.52 40 12.99 41 29.32 42 8.06 45 21.46	+100	s. 0.37 0.34 0.23 0.21 0.25 0.27 0.18 0.17 0.16 0.13 0.05 0.08 0.02 0.04 0.95 0.95 0.95 0.95 0.88 0.90 0.81 0.78 0.79 0.	VII. 2 34.87 11. 2 37.81 2. 6 35.65 VII. 7 46.48 IV. 3 44.27 VII. 1 41.21 " 6 41.11 2. 5 39.30 " 7 42.30 IV. 1 40.86 VII. 2 31.82 VII. 3 38.48 2. 3 43.00 VI. 4 38.74 VII. 1 36.16 11. 6 36.80 I. 2 38.15 IV. 7 33.15 " 5 44.74 " 6 40.10 VII. 6 41.90 V. 6 37.49 VII. 6 40.35 " 3 32.67 VI. 4 39.15 11. 1 39.42 VII. 7 46.45 V. 7 44.36 VII. 3 43.65 VI. 2 42.25 VII. 6 46.25 " 6 36.71 " 7 41.35 IV. 6 44.21 VII. 5 42.57 " 1 33.53 " 7 45.93 11. 2 43.50 2. 2 43.44	-47 41.41 45 59.26 18 3.01 5 58.40 33 31.98 49 53.97 14 54.82 24 39.37 8 22.39 50 6.35 52 22.82 49 26.12 36 51.63 34 15.13 30 46.40 52 48.40 17 23.06 45 48.15 13 39.07 21 32.15 15 30.02 14 27.53 17 0.14 15 21.09 40 12.21 30 32.26 50 55.19 5 59.44 7 11.89 33 53.05 43 26.80 11 57.33 17 26.77 8 55.57 13 8.08 22 46.83 54 19.25 6 17.37 42 42.82 42 45.13	-41.22 40.55 39.03 38.93 38.45 38.34 37.50 37.16 36.15 35.59 35.47 35.43 35.08 34.10 33.48 33.28 33.26 32.43 31.90 31.30 31.11 30.97 30.17 29.71 29.33 28.75 28.94 28.60 28.02 27.82 27.47 27.26 27.06 26.65 25.61 25.59 24.97 24.73 24.60 23.98	h. m. s. 19 26 52.36 29 39.24 36 3.61 36 29.21 38 31.62 38 58.40 42 33.09 45 1.66 48 23.18 50 48.34 51 17.74 51 30.43 53 0.51 57 31.44 20 0 2.10 0 55.65 1 3.60 4 47.78 7 10.26 9 52.16 10 46.07 11 25.86 15 6.72 17 16.64 19 1.12 21 47.10 20 53.41 22 29.43 25 15.69 26 12.77 27 53.66 28 55.66 29 52.57 31 54.88 37 6.43 37 12.22 40 22.71 41 38.95 42 17.74 45 31.11	26 1: 25 4: 25 5: 26 1: 25 4: 25 5: 26 1: 26 1:	3 32 63 1 49.83 3 52.04 1 47.33 9 29.43 5 42.33 0 26.53 4 8.54 5 51.94 8 8.29 5 51.95 6 7 13.45 1 11.13 0 8.50 2 0.97 7 13.45 1 11.13 1 0 8.50 2 40.31 1 0 80 6 51.54 6 51.	1
41 1	.0	••	44.0		8.3 2 C		ECTI	ons.	• •		20 48 8.26	9.	58	VI. 6 32.2	20 2.77	23.45 HENT REA	20 48 17.84	25 45	36.22	
Sept. 19) at 10	h	COR. CLOC	к.	or.		m. s.	n.	_	c. s.	ZENITH POINT. 6	r.	Zon	ne h. VI.—Sept. 1919.5	Α.	B. C.	D. Mean.	BAR.		Ex.
opu de	. ,		10.0		0.01		. 110	1-0.4	+	v. 0.22	0 0 2.05 4	0.120	LX	VI.—Sept. 19 19.5 20.0 21.0 22.8 0.0 0.3 1.8 2.0		15.0 23.0 		30,208 30,220 30,216 30,222 30,212	69.8 69.0 66.5 65.0 63.8 63.2	63.7 61.0 60.6 58.7 57.0 57.5

er.	tude.	SE	COND	os of '	TRANSI	TS	T			D.	d.	Mean Right Ascension,	Mean South
Number.	Magnitude.	и. и.	ш. п	v. v.	vi. vii.	10. 11.	т.	а.	MICROMETER.	D.	u.	1850.0.	1850.0.
			Zone I	LXVI.	Septe	mber 19.	M. D.=	25 ['] 25 ['] 10. ^{''} 0	. n.=-42.	84. n <u>'</u> =-	3.00. (Continued.)	
42	9		, ,		7 27 . 7 39 .	1 1	h. m. s. 20 50 3.33	$+\ _{9.59}^{s.}$	VII. 4 37.87	-31 16 .23	-23.08	h. m. s. 20 50 12.92	25° 56′ 49″.31 z.
43	8	1			2 43.3 55.	1 1	53 19.13 57 55.14	$9.53 \\ 9.53$	2. 6 42.42 III. 2 41.23	14 9.23 44 2.08	$22.47 \\ 21.61$	53 28.66 58 4.67	25 39 41.70 26 9 33.69
44 45	9 5		1		35.447.	1 1	58 11.08	9.48	VII. 7 38.45	10 35.73	21.56	58 20.56	25 36 7.29 z.
46	10	23.5 35.6	6 (0.3 12.2	25.9	1 1	21 1 0.25	9.50	VI. 2 40.07	44 42.07	21.04	21 1 9.75	26 10 13.11
47	10	19.0					4 43.16 5 23.06	9.43	IV. 5 44.08 VII. 4 41.84	21 54.96 28 59.14	$20.38 \\ 20.27$	4 52.59 5 32.49	25 47 25.34 25 54 29.41 z.
48 49	9 9.10	$\begin{vmatrix} \cdot \cdot & \cdot \\ \cdot \cdot & 58.5 \end{vmatrix}$			1 47.5 59.		9 22.95	9.43	IV. 1 32.97	54 38.87	19.56	9 32.38	26 20 8.43 z.
50	9.10	1 1	1 1			0 - 0 -		9.37	11. 7 33.21	13 36.07	19.51	9 49.82	25 39 5.58
51	10	54.8 6.9	9 19.0 3	1.2			13 31.26	9.34	2. 5 43.27	22 22.25	18.87	13 40.60	25 47 51.12 z.
52	8		:	3.0 15.0	027.5	1 1	15 3.01	9.33	" 5 38.84	24 55.24	18.61	15 12.34	25 50 23.85 z.
53	8.9	• • • •	1			1 1	15 21.93 16 56.31	$9.36 \\ 9.32$	VII. 2 36.90 " 5 34.55	46 31.31 27 23.76	18.55 18.29	15 31.29 17 5.63	26 11 59.86 z. 25 52 52.05
54 55	$\begin{vmatrix} 8.9 \\ 9 \end{vmatrix}$	$ \begin{array}{c c} \cdot & \cdot & \cdot \\ 40.552.5 \end{array}$	1 1		5 20.7 32.	1 1	16 56.31	9.32	IV. 4 39.10	31 5.09	17.90	19 26.27	25 56 32.99
56			1		12000	1 1	20 31.76	9.27	VII. 6 33.55	19 15.89	17.70	20 41.03	25 44 43.59
57	8		2 24.2 3				21 36.31	9.27	IV. 5 38.19	25 18.40 31 59.02	17.53 17.33	21 45.58 22 59.12	25 50 45.93 z. 25 57 26.35 z.
58 59	$\begin{vmatrix} 8 \\ 8 \end{vmatrix}$	25.5	2 37.8 5		26.037.	1 1	22 49.86 23 1.25	$9.26 \\ 9.27$	" 4 36.64 VII. 3 35.29	38 41.78	17.30	23 10.52	26 4 9.08 z.
60	8		1 1			. 11.523.5	1	9.26	11. 5 34.18	27 35.95	17.27	23 25.85	25 53 3.22 z.
61	9.1	$0 \dots \dots$	29.6 4	1.7 53.	$8 \cdot \cdot \cdot $	$\cdot \cdot \cdot \cdot \cdot$	25 41.77	9.20	V. 7 37.12	11 21.92	16.87	25 50.97	25 36 48.79
62	9			40.	3 52.7 5.	0	27 28.29	9.22	VII. 4 33.93	33 32.30	16.59	$27\ 37.51$	25 58 58.89
63			1 1	1.7	1 1	1 1	8	9.18	VI. 6 39.88 11. 2 45.55	15 37.52 41 31.97	16.37 16.29	29 0.85 20 31.90	25 41 3.89 z. 26 6 58.26 z.
64 65				8.020.	132.244.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	01 50 05	9.21 9.18	VII. 4 43.09	28 15.97	16.02	31 17.15	25 53 41.99 z.
66					825.037.		99 0 74	9.15	" 5 45.04	21 21.50	15.74	33 9.69	25 46 47.24 z.
67	1		1 1	1	. 12.0 24.	1 1	80 15 00	9.10	2. 7 39.37	10 3.58	15.33	35 56.94 38 24.38	25 35 28.91 z. 25 45 31.87
68 69		39.0 51. 45.			$\begin{bmatrix} 39.0 & 52. \\ 0 & . & \end{bmatrix}$	1 1	44 0 04	9.09	VII. 5 47.20 VI. 5 38.25	20 6.91 25 16.23	14.96 14.54	38 24.38 41 18.98	25 45 31.87 25 50 40.77 z.
70	1	45.	1 1		38.850	1 1	10 10 07	9.08	VII. 3 41.03	35 23.55	14.39	42 23.03	26 0 47.94 z.
71	9		. 4	11.053.	0 5.6 17.	2	44 40.89	9.05	" 3 35.07	38 49.36	14.05	44 49.94	26 4 13.41
72	8.9				3 12.0 24	.0	1	9.04	" 2 35.73	47 11.71	13.62	47 56.55	26 12 35.33 z.
1	10	25.2 37.					50 2.23 50 26.44	9.02	IV. 1 38.24 VII. 3 35.44	51 36.87 38 36.60	13.31 13.26	50 11.25 50 35.43	26 17 0.18 26 3 59.86
74 75	1	9.			51.0 3		70.00.07	8.94	2. 6 35.38	18 12.37	12.98	52 42.89	25 43 35.35 z.
76	1	1 1			226.538		53 2.19	8.93	VII.7 40.16	9 36.65	12.92	53 11.12	25 34 59.57 z.
77	- 1	36.5 49.	1 1				FF 10 F0	8.90	IV. 7 41.72 VII. 7 44.73	8 43.08	12.51 12.64	55 22.05 55 21.44	25 34 5.59 z. 25 32 21.45 z.
78					. 36.7 49 . 31.7 43		F0 7 01	8.91 8.92	" 5 38.61	6 58.81 25 3.58	12.64	56 16.23	25 50 26.10 z.
80		124.536.					00 0 00	8.89	VI. 1 37.55	52 0.57	11.78	22 2 9.85	26 17 22.35 z.
81	-	1 1		F	.7 12	3 !	2 35.48	8.87	VII.2 46.58	40 57.03	11.71	2 44.35	26 6 18.74 z.
82	7.8	1	1 1	1	.0 33.6 45	.8	8	8.84		29 51.96	11.41	5 18.02	25 55 13.37 z.
1	10	21.						8.81	1	18 32.96	11.22	6 54.06 7 10.02	25 43 54.18 z.
84	$\begin{bmatrix} 9.1 \\ 6 \end{bmatrix} \begin{bmatrix} 9.1 \end{bmatrix}$. 25.7 37	$.8 \ 23.0 35.5$			1	34 7.86 41 51.68	11.19 11.13	7 10.02 7 37.08	25 59 29.05 26 7 12.81
86	1				.0 40.2		1)	1	26 40.23	10.58	12 24.66	25 52 0.81 z.
87	10	.	.		. 7.019	.1		\$	4	27 38.65	10.53	1	25 52 59.18
88					.7 48.0 . $.0 24.0 36$			$\begin{vmatrix} 8.76 \\ 8.71 \end{vmatrix}$	2	41 44.36 5 41.12	10.46 10.28	13 32.33 15 8.60	26 7 4.82 z. 25 31 1.40 z.
90		$\begin{bmatrix} 0 & \cdot & \cdot & \cdot \\ 10 & \cdot & \cdot & 34 \end{bmatrix}$					1	1	1	41 13.49	10.06	17 6.86	
l l	1 10				.215.027		00 50 07	8.60	VII.1 40.45	50 20.24	8.69	30 59.51	26 15 38.93 z.
92	8.9	9 20.5 32	.8 45.0	57.0 9	.3 21.5 34	.0	. 32 57.20	8.57	VII.2 43.79	42 33.38	8.50	8	26 7 51.88 z.
93					.7		00 00 01 80	1		36 5.63	8.13	1	26 1 23.76 z.
94	4 9			21.8 34	.0 46.2 58	$\cdot^2 \cdot \cdot \cdot$. 22 38 21.73	8.49	VII.2 38.23	45 45.40	8.02	22 38 30.22	26 11 3.42 z.
-													

er.	tude.		SE	CON	IDS (OF :	ГRА	NSIT	rs.						Mean Right	Mean South
Number.	Magnitude.	1.	II.	111.	1V.	v.	vi.	vII.	10. 11.	Т.	a.	MICROMETER.	D.	d.	Ascension, 1850.0.	Declination, 1850.0.
			7	Zone	LX	VI.	S	eptem	ber 19.	M. D.=	25 25 10 ['] .0	n'.=-42.	84. n. = –	·3″.00.	(Continued.)	
95	9	4.0	16.6	28.8	41.0	53.0	5.0	17.0		h. m. s. 22 40 40.80	s. +8.47	VII. 6 36.85	_17 21".95	- 7 ^{''} .82	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	25° 42′ 39″.77° z.
96	9	56.3	8.8	21.0						44 33.17	8.44	IV. 3 42.08	34 47.59	7.53	44 41.61	26 0 5.12 z.
97	9							5.9		$44\ 29.22$	8.46	VII. 1 35.41	53 14.31	7.53	44 37.68	26 18 31.84
98	8.9	٠.	• •	• •	• •		• •		55.7	44 48.52	8.44	11. 4 37.93	31 13.55	7.51	$44\ 56.96$	25 56 31.06
99 100	8 9	• •	• •	7 9	19.5	91 6	44.0		55.0 7.3	1	8.40 8.41	11. 6 45.40	12 26.06	7.34	47 8.86	25 37 43.40
101		13.0	$\frac{\cdot}{25.3}$)		14.0			49 19.49 51 49.72	8.37	VII. 1 41.84 2. 4 35.73	49 32.19 32 29.76	$7.16 \\ 6.99$	49 27.90 51 58.09	26 14 49.35 z. 25 57 46.75 z.
102	10				54.3		1			52 54.36	8.35	(†) 5 36.49	26 17.12	6.92	53 2.71	25 51 34.04
103	9						52.0	1 1		53 27.53	8.35	VII. 5 43.74	22 6.38	6.89	53 35.88	25 47 23.27
104	10								4.8 17.0	53 9.99	8.35	11. 4 44.64	27 21.79	6.90	53 18.34	25 52 38.69 z.
105	9.10								52.5 5.0	54 57.82	8.34	" 4 42.44	28 37.81	6.79	55 6.16	25 53 54.60
106	10		34.0					34.7		23 3 58.11	8.26	I. 1 44.84	47 48.63	6.24	23 4 6.37	26 13 4.87
107	8.9							46.2		7 9.96	8.21	VII. 6 41.27	14 49.31	6.07	7 18.78	25 40 5.38 z.
108	9.10	••			37.3				• • • •	9 37.43	8.21	2. 1 39.20	51 3.02	5.93	9 45.64	26 16 18.95
109	$\begin{vmatrix} 9 \\ 8.9 \end{vmatrix}$	• •	• •		58.0			52.0		$\begin{array}{c} 10 \ 15.66 \\ 12 \ 57.94 \end{array}$	8.19	VII.5 40.50	23 58.33	5.90	10 23.85	25 49.14.23 z.
$\frac{110}{111}$	8.9				30.0		22.4	i i	$\begin{array}{c c} & 10.4 & 22.5 \\ \end{array}$	12 57.94	8.16 8.15	V. 3 34.50 11. 6 38.52	39 9.30 16 23.63	$\frac{5.79}{5.78}$	$\begin{array}{ccc} 13 & 6.10 \\ 13 & 23.85 \end{array}$	26 4 25.09 z 25 41 39.41 z.
112	10				13.0		1	1 1		16 13.05	8.13	IV. 3 37.29	37 33.02	5.67	16 21.18	26 2 48.69
113	8				1	l .	i .	58.0		$20\ 21.47$	8.11	I. 1 41.97	49 27.71	5.51	20 29.58	26 14 43.22 z.
114	10						16.5	28.3		20 51.82	8.11	VII.1 34.54	53 44.31	5.49	$20\ 59.93$	26 18 59.80 z.
115	8			46.0	58.0	10.2	22.5			25 58.15	8.03	1. 6 39.11	16 3.90	5.34	26 6.18	25 41 19.24 z.
116	8.9		16.0	28.0	40.0	32.3	4.5			28 40.19	8.01	VII.3 35.03	38 50.74	5.26	28 48.20	26 4 6.00 z.
117	8.9				51.5	3.5				29 51.47	8.00	V. 6 37.35	17 14.97	5.22	$29\ 59.47$	25 42 30.19
118	9	• •	• •	• •	• •			45.0	3.3 16.0	30 8.57	8.00	11. 3 37.43	37 27.27	5.22	30 16.57	26 2 42.49 z.
$\frac{119}{120}$	9.10					l .	1	42.3		33 5.61	7.97	I. 4 35.33 " 2 37 28	32 43.97	5.16	33 13.58	25 57 59.13 z.
120	8.9	47.0	59.1				1	37.1		35 23.53 $36 0.74$	7.96 7.94	" 2 37.28 VII. 7 38.61	46 18.21 10 30.17	$5.11 \\ 5.10$	35 31.49 36 8.68	26 11 33.32 z.
122	1	18.5	30.8				1			41 55.05	7.90	2. 2 40.24	44 35.63	$\frac{5.10}{5.02}$	42 2.95	25 35 45.27 z. 26 9 50.65 z.
123			23.0							44 47.41	7.87	" 5 40.50	23 57.94	5.02	44 55.28	25 49 12.96 z.
124	7.8		14.0	26.0	38.0	50.0	2.3	14.2		48 38.03	7.82	VII.7 41.14	9 2.81	5.01	48 45.85	25 34 17.82 z.
125	9.10	40.8	53.0	5.1	17.1	29.3				55 17.35	7.77	VI. 2 47.40	40 28.96	5.00	55 25.12	26 5 43.96 z.
126	9.10					٠.			37.8 50.0	$55\ 43.35$	7.76	11. 7 47.90	5 8.72	5.00	55 51.11	25 30 23.72
127	9.10		• •		$ \cdot\cdot $				51.8 4.0		7.75	" 1 38.34	51 32.49	5.00	58 4.66	26 16 47.49
128	8	• •	[0	9.5		59 33.93	1	VII. 2 37.90	45 56.77	5.00	59 40.76	The second secon
$\frac{129}{130}$	8			3.5				20.4		$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	7.63	VI. 4 37.07	31 44.09	5.24	0 12 23.44	25 56 59.33
131	8.9						د. ب	29.0		13 52.40	7.62 7.61	VII.1 36.33 " 4 41.40	52 42.53 29 14.36	$5.26 \\ 5.29$	$\begin{array}{ccc} 13 & 10.49 \\ 14 & 0.01 \end{array}$	26 17 57.79 25 54 29.65
132	8.9						1		27.0 40.0		7.61	11. 3 37.27	37 32.79	5.29 5.31	14 0.01	26 2 48.10 z.
133	10					6.0	18.1	30.2		16 53.87	7.59	VII. 7 41.43	8 52.81	5.38	17 1.46	25 34 8.19 z.
134	9.10		• •				16.8	29.0		17 52.42	7.58	" 5 42.44	22 51.32	5.40	18 0.00	25 48 6.72 z.
135	9.10		48.3	0.5						20 12.77	7.56	2. 2 45.53	41 32.91	5.46	20 20.33	26 6 48.37 z.
136	9.10					26.5	38.7	51.0		20 14.43	7.56	VII. 5 39.95	24 17.29	5.47	20 21.99	25 49 32.76
137	9.10								32.0 44.0		7.55	11. 6 32.16	20 3.32	5.52	21 44.74	25 45 18.84 z.
138	9.10		• •					28.4		23 51.74	7.53	VII.5 30.58	29 40.88	5.61	23 59.27	25 54 56.49
$\frac{139}{140}$	7.8 8.9	· · 13.0	$\frac{\cdot}{25.2}$				$\begin{vmatrix} 27.8 \\ \cdot \cdot \end{vmatrix}$	1	• • • •	25 3.33	7.52	" 2 38.00	45 53.33	5.66	25 10.85	26 11 8.99 z.
141	8.9	13.0			58.0					27 49.52 27 58.06	$7.50 \\ 7.50$	2. 6 38.86 III. 2 33.83	16 12.15 48 17.59	$5.77 \\ 5.78$	27 57.02 $28 5.56$	25 41 27.92
142	8.9				1 1		1		9.421.8	28 14.83	7.49	11. 6 37.41	17 2.01	5.79	28 22.32	26 13 33.37 z. 25 42 17.80
143	6.7						54.4	6.6		30 30.14	7.47	VII. 7 38.93	10 19.12	5.88	30 37.61	25 35 35.00
144	7.8	٠.	• •		14.2					31 14.05	7.47	" 4 3 9.00	30 37.22	5.92	31 21.52	25 55 53.14
145	9				17.5	29.3		54.0		32 17.39	7.46	" 5 37.19	25 52.63	5.98	32 24.85	25 51 8.61
146	7.8		37.5							0 34 1.88	7.45	IV. 3 40.23	35 51.49	6.06	0 34 9.33	26 1 7.55 z.
		[l		1									
										† Co	mputed as if	on IV.				
													7			

ber.	Magnitude.		SE	CON	DS (OF	TRAN	SITS.		т.	a.		MICROMETER.		D.	d.			Right	1	n So	
Number.	Magı	1.	11.	ш.	ıv.	v.	vi.	vII. 10	. 11.	***************************************			A CONTRACTOR OF THE CONTRACTOR					1850	,		0.0.	
				Zone	LX	VI.	Ser	otembe	r 19.	M. D.=	25 25	10′.0	n'. = -42 ["] .	84.	n".=-3	".00.	(C	ontinu	ıed.)			
147	9						4	6.0 4.	0 16.2	h. m. s. 0 35 9.50	+ s	.44	11. 7 39.87		9 46.03	— 6 ['] .	12		. s. 16.94	25 35	2.1	5
148	9			15.0	27.0		1 1		1	36 27.11		.43	IV. 6 38.57	1	16 22.84	6.	, i		34.54		39.0	
149	10						12.5 2	4.7	.	36 48.25	7	.42	VII.7 41.16		9 2.12	6.	21	36	55.67	25 34	18.3	3
150	9				31.5		1 1			38 31.56		.41	(†) 1 46.54	1	16 50.18	6.	8		38.97	1	6.4	
151	9		• •		• •		$ \cdot \cdot ^2$			39 50.22	1	.40	VII. 1 46.52	1	16 50.55		36		57.62	L	6.9	
$\begin{array}{c} 152 \\ 153 \end{array}$	$9.10 \\ 10$	1		• •	• •	• •		59.	5 12.0 7 59.5	41 4.76	1	.39	11. 1 45.17	1	17 36.58 17 57.27		44 48		12.15 59.50		$\begin{array}{c} 53.0 \\ 13.7 \end{array}$	
153	10			٠.	99 A	34 ($ \cdot \cdot \\ 46.05$	i i	1139.3	41 52.11 44 21.70	!	.39	" 1 44.57 VII.3 41.19	1	35 18.03		65		29.07		34.6	
155	6.7		: :				7.81			45 43.25		.36	" 7 38.81	1	10 23.27	6.			50.61		40.0	
156	9.10	1					55.3			47 30.90		.34	" 5 36.82	1	26 5.38		85		38.24		22.2	
157	7.8	16 (59 1	10.4	99. 5	24 4	46.5			49 22.50	7	.33	2. 2 39.00		15 18.42	Б	97	40	29.83	96 10	35.3	0 7
157	9.10)	1		1 1		5.01	7.5	! 1	49 22.50 53 40.55		.33	VII. 7 42.78	*	8 6.16		97 28		47.86	1	23.4	
159	9.10	1	10.5	1	29.5		1 1			58 29.55	1	.25	I. 1 37.41	5	52 5.24	7.	9		36.80		22.8	
160	9.10			·			541.05			59 16.46		.25	VII. 4 38.29	1	31 1.75		70		23.71	1	19.4	
161	8							5.0 43		59 48.53	1	.25	11. 6 42.34]	14 11.74	7.	73		55.78	1	29.4	
162	7				1		58.0 1	- 1	$\cdot \mid \cdot \cdot \mid$	$1\ 21\ 33.86$.11	VII.7 40.78	1	9 15.22		63		40.97	1	34.8	
163	7				1 1		223.83			29 59.36		.05	" 5 44.55		21 38.39	10.	1		6.41	1	58.9	
164	7			17 0		40.	5.0 1			31 40.53		.04	" 5 44.28	1	21 47.76	10.			47.57	1	8.5	
165 166	6 9	53.4	3.3	1	1		$\begin{array}{c} 54.0 \\ 40.05 \end{array}$		$\cdot \cdot \cdot $	38 29.89 45 15.51		.00	" 5 42.41 " 5 44.12	1	22 52.35 21 53.28	$\frac{11}{12}$.			36.89 22.47	1	15.7	
																	- 1					
167	8			٠٠	12.3	24.6				48 12.39	[.94	2. 2 46.55	i	10 57.69	12.			19.33		20.5	
$\frac{168}{169}$	$\begin{vmatrix} 6.7 \\ 8 \end{vmatrix}$			• •		٠.	1 1	$0.5^{+0.5}$	1 7.0	49 0.36		.95	11. 6 45.58 " 3 40.78	1	12 19.81 35 31.55	12. 13.		49	$7.31 \\ 20.85$	1	$\frac{42.8}{54.7}$	
170	9		: :					7.525		50 13.92 50 30.89	1	.92	" 1 42.36	1	19 13.64	13.	ı		37.81		36.8	
171	10	1	12.6	1	37.0		1 1			53 37.02		.91	IV. 3 37.78	i	37 16.08	13.			43.93	1	39.7	
172	9.10	1			1		26.03		.	55 1.76		.90	VII.2 40.01	1	14 43.93	13.			8.66	1	7.7	
173	9.10			• •	• •		• •	1.2 19	4 31.8	1 56 24.69	6	.90	11. 5 37.67	2	25 35.40	14.	02	1 56	31.59	25 50	59.4	2 z
					Zo	ne I	XVII.	. Se	ptembe	er 21. H.	D. =	4	13 , 2 1 00.0.	í.=·	—31 ['] .66.	n'.=	=—1ģ	.00.				
1	8						$2 _{12.5 _2}$			19 36 41.61	11	.38	VII.5 46.411	5	20 43.37	27.	27	19 36	52.99	43 42	10.6	4
2							118.4		$\cdot \mid \cdot \cdot \mid$	48 48.36		.20	8	1	5 29.07	24.	9		59.56	1	53.2	
3	1	1		1			027.04	1.0	$\cdot \cdot \cdot $	53 56.01		.18	" 3 38.450	1	37 14.14	22.	8		7.19	1	37.0	
4			243.0			44		• • •	$\cdot \cdot \cdot $	20 0 13.35	1	.11	II. 3 31.831 IV. 4 34.613	1	11 5.07	21.	8		$24.46 \\ 40.06$	1	$26.4 \\ 48.4$	
5 6	$\begin{vmatrix} 8 \\ 7.8 \end{vmatrix}$	• •		13.5	29.2		9.52		1	0 28.97 0 38.73	i	.09	VI. 2 40.910		$\begin{bmatrix} 33 & 27.15 \\ 44 & 39.39 \end{bmatrix}$	$\frac{21}{21}$.			49.84		0.6	
7	9	38.0	1	1			$0 \cdot 0 \cdot 0 \cdot 0 \cdot 0 \cdot 0 \cdot 0 \cdot 0 \cdot 0 \cdot 0 \cdot$			4 24.01	1	.06	IV. 2 38.076	ì	16 18.84	20.	5		35.07	1	39.2	
8	9						3 1.01			12 30.54		.95	" 2 36.122	1	17 27.23	18.	9		41.49		45.6	
9	9.10					23.0	$0 \cdot \cdot 5$	4.0 .	.	14 8.30	10	.87	VII.6 39.586]	15 53.08	18.	08	14	19.17	43 37	11.1	6
10	9		13.5	28.5	43.0	٠.	• •	• • •	. • •	20 22 43.54	10	.77	IV. 4 43.175	5	28 28.11	16.	21	20 22	54.31	43 49	44.3	2
					ı	COR	RECTIO	ons.							INSTRU	MENT	REA	DINGS		A CONTRACTOR OF THE CONTRACTOR		
			COR	TO	HOUR	LV				ZENITH						CI	RCLE.				THER	кмом
			CLC		COL		m.	n.	c.	POINT.	COINC.				Α.	в.	c.	D.	Mean.	BAR.	At.	Ex
					s.		8.	8.	8.	0 0 3.12	r.	Ze	one / XVII.—Sept. 211	h.			. الري	11 -		ı. 30.108		-0
Sept.	21, at 1	18h	-0	.419	-0.	020	0.415	+0.429	+0.022	0 0 3.12	40.100	LY		19.7 20.3	277 21 1'.7 3.5	5.7 5.5	13.0 16.0	3.2 6.2	5 ^{''} .40 7.80	30,108 30,122	72.5	69.
													5	21.3						30.130	71.0	6.5
						† Ta	iken for	IV.														
**********				11								11	Andrew A. P. all Street Co.			1	1	1				<u> </u>

Number.	Magnitude.	1.	SECOI	NDS OF	1 1	VII. 10	. 11.	т.	a.		MICROMETER.	D.	d.	1	Right ension,	Dec	n Sor clinati	
			Zone i	LXVII.	Sept	tember !	21.	Н. Д.=	43° 21	00		.66. n'. =	=-19.00.	(Cont	inued.)			
11 12 13 14 15 16 17 18 19 20 21 22 23 24	7.8 9 8.9 9 8.9 7.8 6 9 7 7.8 9	16.0 35.7 45.0 39.5 	34.2 49.5 31.0 45.4 51.4 6.5 1.2 16.6 . 9.6 38.5 54.6 46.3 2.6	5 1.0 16. 221.5 36. 3 59.2 14. 0 31.5 46. 0 24.5 40. 0 9.0 23. 0 16.2 31. 30.2 45.	0 48.5 0 48.2 0 31.0 4 3 51.8 2 29.2 4 0 1.51 0 1 8 39.8 0 47.2 5 0.51	3.5		h. m. s. 20 23 51.29 25 18.44 27 4.34 27 17.66 30 1.00 38 21.39 21 19 58.32 24 31.18 28 24.88 30 9.03 33 16.59 40 30.15 41 32.28 21 43 7.70	+10 10 10 10 10 10 10 10 10 10 10 10 10 1	.74	" 2 37.810 " 6 32.890	-35 50".58 34 15.70 12 14.03 39 38.79 14 4.5' 12 0.0' 48 18.3' 14 1.3' 45 3.2 27 14.90 49 19.10 46 28.09 19 47.6 11 37.79	15.77 15.33 15.39 15.39 14.77 13.33 1 6.88 7 6.2 4 5.77 4 5.44 5 14 5 14 7 4 12 7 4 4.24	0 20 20 20 20 4	4 2.05 5 29.18 7 15.01 7 28.38 0 11.63 8 31.89 0 8.82 4 40.93 8 34.61 0 18.71 3 26.25 0 39.67 1 41.74	43 55 43 33 44 0 43 35 43 33 44 9 43 35 44 6 43 48 44 10 44 7 43 40	6.5 31.4 5.29.3 5.4.0 6.19.3 6.19.3 6.25.1 6.7.6 6.8.9 6.24.2 7.6 7.6 8.9 8.9 9.5 9.5 9.5 9.5 9.5 9.5 9.5 9	0 7 8 2 2 6 1 6 2 1 7
				Zone	LXVI	II. S	Septem	ber 22. M	. D.	=:	24 55 20.0.	$=-38^{''}_{.}00$	n'.==-	$-4^{''}\!\!.01.$				
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	5.6 5 9 9 7 8.9 9.10 9.10 8.9 7.8 8.9 8.9 10 8.9 8.9	47.1 47.1 49.5	55.8 7.42.7 54.4 55.8 7.42.7 54.4 59.5 11.36.0 48.4 4.8 16.4 1.5 13.4 59.5 13.4	0 45.5 57. 36. 5.54.5 . 720.0 . 7 6.6 18. 29.0 41 423.7 . 0 1.113. 3 51.0 3 3 17.3 2.1 14.	.3	28. 6		19 25 52.60 26 45.34 27 24.78 27 44.63 30 54.52 32 19.92 33 6.76 34 29.01 34 34.40 35 54.09 36 19.72 37 10.10 41 23.74 42 0.61 43 28.92 43 35.47 47 25.97 47 50.98 49 4.19 48 13.52 54 5.96	1	.46 .42 .43 .45 .40 .38 .36 .38 .41 .39 .35 .36 .31 .31 .28 .27 .28	VII. 7 45.12 " 6 38.17 11. 4 43.30 I. 6 43.27 VII. 6 41.23 II. 6 38.68 V. 7 42.89 11. 5 37.67 VII. 1 44.61 11. 3 40.35 " 6 35.20 1. 2 39.85 V. 5 46.56 IV. 4 46.14 VII. 2 49.79 III. 2 38.30 V. 4 34.88 11. 4 38.12 " 3 35.76 V. 4 41.52	30 35.0 6 46.6 16 37.4 28 9.2 13 41.4 14 51.8 16 20.1 8 3.9 25 36.5 47 57.4 35 47.5 18 19.5 44 49.8 20 30.3 26 32.0 39 7.1 45 44.2 33 0.7 31 8.0 38 25.9 29 11.4	1 36.44 36.2 36.1 35.4 4 35.1 30 34.9 34.6 34.6 34.0 34.0 33.0 32.9 32.6 31.3 31.3 31.3 30.2	20 22 25 27 22 27 25 33 34 34 34 34 34 34 34 35 34 34 35 34 34 35 34 35 34 35 36 36 36 36 36 36 36 36 36 36 36 36 36	6 2.06 6 54.76 7 34.21 7 54.08 1 3.92 2 29.31 3 16.13 4 38.37 4 43.78 6 3.50 6 29.11 7 19.45 1 33.10 2 9.92 3 38.23 3 44.80 7 35.28 8 0.27 9 13.46 8 22.80 4 15.19 6 11.17	25 2 25 12 25 24 25 9 25 10 25 12 25 3 25 21 25 43 25 14 25 40 25 16 25 22 25 34 25 25 34 25 34 25 34	31.6 243.0 233.7 5.4 36.8 36.8 36.9 46.9 215.0 358.5 31.1 351.7 41.7 41.7 42.9 35.9 35.9 35.9 35.9 47.0 35.9 35.9 36.9 36.9 47.0 47	1 z. 3 z. 0 55
		-1 - 8	COR, TO	HOURLY				ZENITH					CIRC				THER	MOM.
Sept.	22, at	18h	s. —0.888	s0.014	s. -0.415	n. $+0.429$	s. +0.022	POINT.	r. 40.110	Z L		20.5 . 21.7 22.2	· · ·		Mean.	30.220 30.210 30.216	68.0 66.2 65.3	59.0 57.2 56.3
												0.4	.0 4.7	4.0 7.5	6.80	30.202	63.0	50.7

	tude		se	CON	DS	OF '	TRA	NSI	ΓS.					_	_	Mean Right	Mean Sout
	Magnitude.	I.	и.	ш.	IV.	v.	vi.	VII.	10.	11.	Т.	a.	MICROMETER.	D.	d.	Ascension, 1850.0.	Declination 1850.0
			ļ	Zone	LX	VIII		Sept	embei	- 22.	M. D.=	$=2\mathring{4} \ 55^{'} 20$	0.0. n'. == -3	8.00. n.=	—4. 01. ((Continued.)	
	10		90 A		5 C O						h. m. s.	s.	r.	$-16^{'}$ 3 $^{''}$ 65	2939	h. m. s. 19 58 5.30	25 [°] 11 [°] 53.04
	$\begin{bmatrix} 0 \\ 8.9 \end{bmatrix}$		32.0 	$\frac{.}{59.0}$	$\frac{56.2}{11.9}$	1	5				19 57 56.13 59 11.31	+9.17 9.15	IV. 6 39.16 VI. 7 47.99	$\begin{bmatrix} -16 & 3.65 \\ 5 & 7.74 \end{bmatrix}$	29.12	19 58 5.30 59 20.46	25 11 55.04
	9.10					1	15.	1		: : : :	59 51.00	9.15	11. 6 46.70	11 42.46	28.97	20 0 0.15	25 7 31.43
- 1	7.8						1	0 31.0	1		20 0 54.69	9.19	VII. 1 45.79	47 16.68	28.75	1 3.88	25 43 5.43
- 1	7.8					1	1	0 31.0			0 54.70	9.19	" 2 45.15	41 47.37	28.75	$1 \ \ 3.89$	25 37 36.12
3	7.8				38.0	49.8	2.	0			3 37.84	9.12	" 5 49.27	18 56.50	28.17	3 46.96	25 14 44.67
	8							1	53.5	6.2	459.22	9.12	11. 5 42.50	22 49.81	27.88	5 8.34	25 18 37.69
- 1	1	24.9			1		1	5 37.5			7 1.20	9.14	1. 2 42.13	43 31.62	27.46	$7\ 10.34$	25 39 19.08
		23.0	35.2		59.2		1	6			8 59.35	9.10	VII. 4 35.72	32 31.44	27.04	9 8.45	25 28 18.48
2	8.9	• •	• •	٠.	• •	٠.	7.	5 19.9	2		9 42.89	9.12	" 1 38.53	51 27.43	26.88	9 52.01	25 47 14.31
;	7.8							5			$10\ 37.29$	9.10	II. 2 38.87	45 24.45	26.69	10 46.39	25 41 11.14
- 1	8.9					29.0					11 16.89	9.10	VII.2 39.98	44 45.89	26.56	11 25.99	25 40 32.45
	7.8								732.0	44.0	11 37.39	9.05	11. 6 32.00	20 10.04	26.49	11 46.24	25 15 56.53
	8			• •	48.0			$2 \dots$	100		13 48.41	9.05	VII.5 33.20	28 11.40	26.04	13 57.46	25 23 57.44
	8		• •		• •	10 (004	1			13 55.30	9.05	11. 4 36.75 2. 5 40.60	31 55.38 23 55.64	$26.02 \\ 25.39$	14 4.35 17 9.01	25 27 41.40 25 19 41.03
3	$8.9 \\ 7.8$		• •		: :	12.0		$\begin{vmatrix} 3 & \cdot & \cdot \\ 0 & 44 & \cdot \end{vmatrix}$	5		$17 0.00 \\ 17 7.84$	$9.01 \\ 9.02$	I. 4 40.17	29 57.80	25.36	17 16.86	25 25 43.16
	8.9					: :		1			18 0.11	8.98	VII. 7 37.82	10 58.65	25.18	18 9.09	25 6 43.83
Ĺ	9							0 37.0	1		19 0.57	9.02	" 3 34.82	38 58.91	24.97	19 9.59	25 34 43.88
2	9			58.5	1	23.0	1	1			$22\ 10.86$	8.98	2. 3 40.51	35 42.27	24.34	$22\ 19.84$	25 31 26.61
3	9		56 5		20 5		45	0	 		22 20.62	8.98	" 3 40.27	35 50.54	24.31	22 29.60	25 31 34.35
Ĺ	7				1		1	0			23 13.86	8.96	VII. 4 46.15	26 31.31	24.13	23 22.82	25 22 15.44
5	7				١	1		223.	1.		23 47.06	8.96	11. 3 48.75	30 57.43	24.02	23 56.02	25 26 41.45
3	7		1	34.7			i	-			28 47.09	8.93	IV. 2 45.50	41 35.65	23.03	28 56.02	25 37 18.68
7	9.10				١			40.	5		29 3.97	8.94	VII.1 37.18	52 14.03	22.98	29 12.91	25 47 57.01
3	9.8				٠.		8.	620.	4		29 44.06	8.93	10. 1 45.70	47 19.62	22.84	29 52.99	25 43 2.46
9	7.8	٠.		34.0							31 46.11	8.90	V. 2 50.35	38 48.12	22.45	31 55.01	25 34 30.57
0	8.9			10.0			_	0 10.			32 33.80	8.84	11. 7 46.21	6 8.53 17 47.88	22.30	32 42.64	25 1 50.83 25 13 29.80
$\begin{bmatrix} 1 \\ 2 \end{bmatrix}$	$8.9 \\ 10$	• •	-	19.8		-			013.0	95 O	34 32.00 35 18.46	8.84 8.84	V. 6 36.14 VII.5 44.53	21 40.14	21.92 21.77	34 40.84 35 27.30	25 15 29.80
										20.0			i .			<u> </u>	
3	8.9						1	0	1		36 58.04	8.85	11. 2 43.60	42 40.39	21.45	37 6.89	25 38 21.84
4	$\frac{5}{9.10}$	10.0	04.5						10.5	1	37 16.08	8.87	" 1 36.43 II. 5 35.92	52 39.45 26 37.72	$21.40 \\ 20.72$	37 24.95 40 57.41	25 48 20.85 25 22 18.44
5 6		12.0							5		40 48.62 41 30.18	8.80	10. 3 39.65	36 11.92	20.60	41 38.98	25 31 52.52
7	9.10							- 1			47 9.15	8.76	III. 1 41.80	49 34.77	19.56	47 17.91	25 45 14.33
3	9		1	31.8		1	- 1		1		48 44.13	8.73	I. 4 36.98	31 47.94	19.26	48 52.86	25 27 27.20
9	7.8						7.	0 19.	0		48 42.79	8.69	VII.7 43.10	7 36.35	19.27	48 51.48	25 3 35.62
0	9							0 3.	8		49 27.14	8.69	11. 6 45.22	12 33.59	19.13	49 35.83	25 8 12.72
1.	8.9			21.5						1	53 33.93	8.68	I. 4 36.72	31 56.91	18.40	53 42.61	25 27 35.31
2	7.8	44.0	56.0	8.0	20.0	32.	2 .	56.	8		54 20.29	8.69	IV. 2 41.315	44 0.14	18.26	54 28.98	25 39 38.40
3	10							.			56 34.89	8.64	" 5 38.85	24 56.64	17.88	56 43.53	25 20 34.52
4	9	21.2						.			20 57 57.40	8.61	III. 6 33.62	19 14.87	17.62	58 6.01	25 14 52.49
5	4		i	1	1	ł		1	5		58 12.09	8.64	VII.3 32.31	40 25.62	17.58	58 20.73	25 36 3.20
6	8.9	38.9						.			21 0 15.29	8.61	IV. 5 34.40	27 30.32	17.22	21 0 23.90	25 23 7.54 25 25 32.44
7 8	$8.9 \\ 7.8$		1	1	1		- 1	44.			$ \begin{array}{cccc} 1 & 11.84 \\ 2 & 7.97 \end{array} $	8.60 8.59	" 4 40.25 10. 4 39.38	29 55.38 30 24.87	17.06 16.91	$\begin{array}{c c} 1 & 20.44 \\ 2 & 16.56 \end{array}$	25 26 1.78
$\begin{vmatrix} 5 \\ 9 \end{vmatrix}$	7.8		1	1	ř	1			5		4 25.29	8.57	2. 4 37.01	31 46.69	16.52	4 33.86	25 27 23.21
0	9	58.0	1	i	1				$\begin{bmatrix} 0 \\ 1 \end{bmatrix}$	1	4 34.78	8.57	VII. 4 33.80	33 37.74	16.50	4 43.35	25 29 14.24
1	9										9 41.31	8.53	" 2 42.34	43 24.41	15.64	9 49.84	25 39 0.05
2	8.9										12 38.77	8.48	I. 5 39.04	24 49.44	15.17	12 47.25	25 20 24.61
3	9				32.0	144	0				13 31.94	8.51	IV. 1 37.60	51 59.85	15.04	13 40.45	25 47 34.89
4	8.9					1			554.5			8.45	11. 6 38.98	16 9.03	14.96	14 8.53	25 11 43.99
- 1	2.0											1	1	1	14.72	21 15 39.83	25 3 35.55

er.	itude.		SEC	CON	DS	OF '	TRA	NSI	ΓS.				. ,				Mean Right	Mean South
Number.	Magnitude.	ı.	11.	ш.	IV.	ν.	VI.	vII.	10.	11.	Т.	•	a.	MICROMETER	D.	d.	Ascension, 1850.0.	Declination, 1850.0.
			${f Z}$ o	ne I	XV.	III.	S	epten	ıber 2	2.	М.	D. = -	24° 55′ 20		38.00. n. =	=4″.01.	(Continued.)	
76	8.9					45.0	57.5	5 9.5			h. m. 21 16		$+\frac{s.}{8.46}$	VII. 3 38.25	37 0 ["] .51	14.56	$h. \ m. \ s. \ 21 \ 16 \ 41.50$	25° 32′ 35″.07
77	8.9					i	1		47.7			53.20	8.44	" 5 32.96	28 19.68	14.51	17 1.64	25 23 54.19
78	7						26.8			[18	2.59	8.41	11. 7 35.98	12 1.71	14.33	18 11.00	25 7 36.04
79	8.9	٠.	• •				57.1		• •	• •		32.81	8.44	VII.1 42.68	49 4.08	14.09	19 41.25	25 44 38.17
80 81	9 8	• •	• •	• •			$\begin{bmatrix} 7.9 \\ 0.6 \end{bmatrix}$					43.52	8.41	VI. 4 37.50	31 30.24	13.91	20 51.93	25 27 4.15
82	9.10			٠.			3					$36.29 \\ 48.46$	8.37 8.36	VII. 7 40.86 VI. 7 39.25	9 13.69 10 9.54	13.78	21 44.66	25 4 47.47 2
83	6.7		- 1				1	22.2	1			45.79	8.36	VII. 6 33.35	19 23.92	13.61 13.47	22 56.82 23 54.15	25 5 43.15 25 14 57.39 z
84	8.9	i i	18.3									42.93	8.37	" 2 46.18	41 11.81	13.18	25 54.15 25 51.30	25 14 57.39 2 25 36 44.99 z
85	9.10						1	1		[30.63	8.32	2. 5 41.775	1	12.76	28 38.95	25 18 47.85
86	7.8				49.8	2.0	13.8	3			98	49.80	8.30	VII. 7 36.61	11 40.44	12.71	28 58.10	
87	7.8	1	49.2									13.44	8.29	VI. 7 36.64	11 39.64	12.71	28 58.10 30 21.73	25 7 13.15 z 25 7 12.15 z
88	8.9			14.3	26.5	39.0	50.5	5				26.54	8.30	VII.5 36.60	26 13.97	12.33	31 34.84	25 21 46.30
89	7		37.5	49.5	1.7	13.8	26.0	0		[33	1.75	8.31	IV. 1 38.96	51 12.88	12.11	33 10.06	25 46 44.99
90	7.8	٠.				1				22.5		15.69	8.28	11. 5 39.97	24 17.14	12.07	$33\ 23.97$	25 19 49.21 z
$\frac{91}{92}$	7		$\frac{24.5}{6}$		l	1	1		• •	• •		48.83	8.27	VI. 3 33.23	39 54.09	11.70	35 57.10	25 35 25.79
92 93	7.8 7.8		6.5				10.5	53.0	• •	[30.56	8.24	IV. 3 42.32	34 40.31	11.46	37 38.80	25 30 11.77
94	8.9							$\frac{33.0}{42.3}$				$16.38 \\ 6.01$	8.26 8.19	VII. 1 41.40 " 6 43.26	49 48.30 13 41.74	11.35 11.10	38 24.64	25 45 19.65
95	9		25.9		l	1	1					49.78	8.17	2. 1 44.97	47 44.79	10.22	40 14.20 46 57.95	25 9 12.84 2 25 43 15.01 2
96	8																	
97	9		22.0		40.0	30.0	1	$\frac{ \cdot }{29.2}$		• •		46.13 52.82	8.08 8.10	1. 6 39.33 2. 5 37.49	15 53.51	9.72	50 54.21	25 11 23.23
98	9						1	16.0				39.58	8.10	VII.3 40.31	25 43.08 35 49.37	$9.71 \\ 9.61$	51 0.92	25 21 12.79
99	7.8				ı		59.0	1				34.78	8.10	" 1 44.44	48 3.33	9.38	51 47.68 53 42.88	25 31 18.98 25 43 32.71
00	7.8						1		57.8			3.32	8.08	11. 2 49.26	39 24.97	9.32	54 11.40	25 34 54.29 2
01	8)]	55	13.86	8.07	VII.3 38.46	36 53.26	9.18	55 21.93	25 32 22.44 2
02	7		1					40.0		$\cdot \cdot $	59	3.33	8.00	2. 7 36.57	11 41.60	8.72	59 11.33	25 7 10.32
03	8	1	1					46.2	1	$\cdot \cdot $		9.93	8.00	I. 6 34.30	18 51.12	8.71	59 17.93	25 14 19.83
$\begin{vmatrix} 04 \\ 05 \end{vmatrix}$								$\begin{array}{c} 357.1 \\ 5.8 \end{array}$		$\cdot \cdot $		21.04	7.99	1. 4 37.81	31 18.77	8.35	22 2 29.03	25 26 47.12 2
		23.0										29.37	7.95	2. 5 36.36	26 22.09	8.01	5 37.32	25 21 50.10 z
06	8		1			1	2 12.5	1	• •	$\cdot \cdot $		48.17	7.96	VI. 1 43.96	48 20.12	7.86	$6\ 56.13$	25 43 47.98 2
07	9	• •	48.0		12.0			05.4		$\cdot \cdot $		12.11	7.87	2. 4 37.96	31 13.88	7.09	14 19.98	25 26 40.97
08 09	i											1.00	7.87	III. 3 40.80	35 32.79	7.00	15 8.87	25 30 59.79 2
10	9.10		48.0			1	1		$\frac{\cdot}{38.0}$			$12.25 \\ 43.77$	7.84 7.81	VI. 3 44.12 11. 6 38.34	33 38.04	6.78	17 20.09	25 29 4.82 2
11	8			- 1				252.3				15.91	7.76	VII. 4 44.26	16 31.14 27 36.57	6.63	$\begin{array}{c} 18\ 51.58 \\ 24\ 23.67 \end{array}$	$\begin{bmatrix} 25 & 11 & 57.77 \\ 25 & 23 & 2.70 \end{bmatrix}$
12	8						1	322.2				46.02	7.72	" 7 38.55	10 33.44	5.99	25 53.74	25 25 2.70 2
13	9.10							5				32.38	7.75	" 2 33.65	48 24.44	5.84	27 40.13	25 43 50.28
14	9				35.5	47.5	59.6	12.0				35.38	7.74	" 1 38.50	51 28.41	5.65	29 43.12	25 46 54.06 2
15	8.9			33.0	45.0	57.0	9.0	21.4		\cdots	32	45.05	7.65	" 7 47.10	5 38.24	5.40	32 52.70	25 1 3.64 z
16	8.9		43.25	55.0	7.2	19.5	31.5	43.5			35	7.29	7.64	2. 6 42.11	14 21.25	5.22	35 14.93	25 9 46.47 z
17	8		17.5 2	9.6	41.8	34.0	6.0	18.2		[41.80	7.61	II. 2 35.13	47 33.54	4.79	40 49.41	25 42 58.33
18		37.0	49.5	1.7	13.4	25.7	37.8	3]		13.62	7.56	2. 5 36.79	26 7.21	4.56	44 21.18	25 21 31.77 z
19								38.0		• •		1.48	7.57	II. 1 38.85	51 16.58	4.43	46 - 9.05	25 46 41.01 z
20	9							26.5		• •		49.92	7.53	VII. 1 36.54	52 36.09	4.18	49 57.45	25 48 0.27
21	$\frac{9}{8.9}$							16.0				51.98	7.49	IV. 5 38.32	25 14.96	4.07	51 59.47	25 20 39.03
22 23	6.9							16.0				39.70	7.48	VII. 4 35.91	32 24.89	4.02	52 47.18	25 27 48.91 z
23 24	9.10											$\frac{3.84}{18.80}$	$7.44 \\ 7.43$	2. 6 42.75 VII.7 37.05	12 59.13 11 25.25	3.84	56 11.28	25 8 22.97
25											23 2		7.43	" 7 42.40	8 20.55	$\begin{vmatrix} 3.77 \\ 3.53 \end{vmatrix}$	57 26.23 23 2 20.34	25 6 49.02 z 25 3 44.08 z
ı		- 1	1							ı								
$\begin{vmatrix} 26 \\ 27 \end{vmatrix}$	$\frac{7}{8.9}$	35.0										$\frac{11.12}{28.86}$	7.33	I. 7 40.23	9 35.46	3.31	7 18.45	25 4 58.77
28							93.1	1 1		1		51.38	$7.33 \\ 7.31$	VII. 4 41.50 VI. 4 38.35	29 11.88 31 9.88	$\frac{3.25}{3.20}$	8 36.19	25 24 35.13
				•			•	•	.	- COMMANDE	AU 0	C1.00		. r. a 90.99	31 3.00	3.20	23 9 58.69	25 26 24.08 z

		TS.						Mean Right	Mean South
Number. Magnitude	I. 11. III. IV. V. VI. VII.	. 10. 11.	Т.	a. ·	MICROMETER.	D.	d.	Ascension. 1850.0.	Declination, 1850.0.
	Zone LXVIII. Septe	ember 22. M	. D.=	24° 55′ 20′.0	o. n'=-38	″00. n″.=-	$-4.\overset{''}{0}1.$	(Continued.)	
129 9			. m. s. 10 55.03	$+\frac{s.}{7.30}$	11. 4 33.46	-33 49 .02	2"10	h. m. s.	25° 29′ 12″.18
$\frac{123}{130} \left \begin{array}{c} 3 \\ 9 \end{array} \right $		55.2 7.2	$10 \ 53.03$ $12 \ 0.77$	7.28	11. 4 33.46	-33 49.02 10 36.10	-3.16	23 11 2.33 12 8.05	25 29 12.18
131 8.9	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$		13 16.98	7.28	VII. 2 37.43	46 13.96	3.13	13 24.26	25 3 39.23 25 41 37.05 z.
132 8.9	26.5 39.0		14 14.68	7.28	VI. 7 41.52	8 51.18	3.05	14 21.96	25 4 14.23 z.
133 8	$ \cdot \cdot \cdot \cdot \cdot \cdot 21.0 33.3 45.6$		15 8.83	7.26	VII. 4 39.35	30 26.12	3.02	$15\ 16.09$	25 25 49.14
1 1	52.4 4.8 16.8 29.0 40.6 53.0		19 28.86	7.22	I. 5 43.40	22 19.20	2.87	19 36.08	25 17 42.07 z.
$ \begin{array}{c c} 135 & 9.10 \\ 136 & 7 \end{array} $			20 57.13	7.20	VII. 6 41.325	14 48.56	2.83	21 4.33	25 10 11.39
136 7	$egin{array}{ c c c c c c c c c c c c c c c c c c c$	1 1	22 38.00 $24 5.19$	7.18 7.18	" 7 46.57 11. 5 52.01	5 56.56 17 21.40	$egin{array}{c} 2.80 \ 2.77 \end{array}$	22 45.18	25 1 19.36 z.
1 1	22.534.547.059.311.323.435.		25 59.11	7.16	VII. 2 38.11	45 50.45	$\frac{2.71}{2.74}$	$ \begin{array}{cccc} 24 & 12.37 \\ 26 & 6.27 \end{array} $	25 12 44.17 25 41 13.19 z.
	16.028.040.252.5 4.717.029.		29 52.54	7.13	2. 2 36.27				
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{bmatrix} 16.0 & 28.0 & 40.2 & 52.5 & 4.7 & 17.0 & 29. \\ . & . & . & . & . & . & . & . & . & $		29 52.54 36 9.59	7.13	VII. 2 47.77	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$2.66 \\ 2.61$	29 59.67 $36 16.65$	25 42 16.44 25 35 39.50
141 7.8	44.3 . 8.8 20.8	5 I B	38 56.65	7.03	2. 6 45.00	12 41.45	$\frac{2.01}{2.58}$	39 3.68	25 35 39.50
142 8			39 30.69	7.03	VII.5 41.83	23 13.40	2.57	39 37.72	25 18 35.97 z
1 1	12.0 24.2 36.4 48.0 0.6 13.0 25.		44 48.52	7.00	II. 1 34.45	53 48.51	2.58	$44\ 55.52$	25 49 11.09 z.
144 6			45 28.22	6.96	11. 7 42.44	8 18.68	2.58	45 35.18	25 3 41.26
$egin{array}{c c} 145 & 9.10 \ 146 & 8.9 \ \hline \end{array}$		1 1 5	47 23.60	6.95	VI. 7 42.32	8 23.54	2.59	47 30.55	25 3 46.13
$egin{array}{c c c} 146 & 8.9 \ 147 & 6 \ \end{array}$	$\begin{vmatrix} . & . & . & . & . & . & . & . & . & . $	$\begin{vmatrix} 4 & \cdot & \cdot & \cdot \\ 33.746.0 \end{vmatrix}$	48 3.08 48 39.12	6.95	VII. 6 36.61 11. 3 34.99	17 31.33 38 52.57	2.59 2.60	48 10.03	25 12 53.92
148 7.8	53.0 5.0 17.	1 1 2	50 40.96	6.91	VII. 7 48.57	4 47.47	$\frac{2.60}{2.61}$	$\begin{array}{c} 48\ 46.07 \\ 50\ 47.87 \end{array}$	25 34 15.17 25 0 10.08 z.
149 7.8	$ \dots \dots \dots $	$_{9}$ $ $ $ $	51 54.48	6.92	" 3 44.71	33 17.40	2.62	52 1.40	
1 1	lllllll.		55 22.15	6.89	I. 4 40.17	29 57.80	$\frac{2.62}{2.66}$	55 29.04	25 28 40.02 25 25 20.46 z
151 9.10			55 44.59	6.88	VII.3 31.67	40 47.68	2.66	55 51.47	25 36 10.34
152 8	4.0 16.2 28.3 40.5		58 28.34	6.86	2. 5 39.40	24 37.12	2.71	58 35.20	25 19 59.83
153 8	53.0 5.2 17.7 30.		58 53.26	6.86	VII. 4 37.21	31 40.00	2.72	59 - 0.12	25 27 2.72 z
154 9	$ \begin{vmatrix} . & . & 6.0 & 18.0 & 30.0 & 42.0 & . & . \\ . & . & . & . & . & . \\ . & . &$	1 1 1	7 30.10	6.78	2. 5 41.13	23 37.37	2.94	0 7 36.88	25 19 0.31 z.
$ \begin{array}{c cccc} 155 & 9 \\ 156 & 8.9 \end{array} $	$\begin{bmatrix} \dots & \dots & \dots & 50.8 & 3.0 & 15.0 & 27. \\ \dots & 3.4 & 15.1 & 27.3 & 39.5 & \dots & \dots \end{bmatrix}$	1 1 1	750.81 1127.39	$6.78 \\ 6.75$	VII. 6 40.46 " 7 40.02	15 18.43	2.95	7 57.59	25 10 41.38 z.
157 9	$\begin{bmatrix} \dots & 3.4 & 15.1 & 27.3 & 39.5 & \dots & \dots \\ \dots & \dots & \dots & 39.4 & 51.2 & 3.5 & 15. \end{bmatrix}$		12 39.18	6.74	" 3 38.83	9 42.70 36 40.45	3.07 3.11	$\begin{array}{c} 11\ 34.14 \\ 12\ 45.92 \end{array}$	25 5 5.77 z. 25 32 3.56 z.
158 9.10		1 1	14 25.37	6.72	IV. 1 39.87	50 41.46	3.18	14 32.09	25 46 4.64
159 7.8	$ \dots \dots \dots \dots _{10.5 22}$	6	14 46.10	6.72	(†) 1 34.45	53 48.61	3.20	14 52.82	25 49 11.81 z.
			16 54.94	6.70	IV. 3 35.35	38 40.98	3.28	17 1.64	25 34 4.26 z.
161 7.8		7 0.9 12.4	18 6.28	6.69	•	11 38.22	3.32		25 7 1.54
	39.051.03.215,227.2.		$20\ 15.36$	6.67	2. 2 38.89	45 23.30	3.41	20 22.03	25 40 46.71 z
163 7			21 13.26	6.66	IV. 4 35.69	32 32.81	3.47	21 19.92	25 27 56.28 z.
$egin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{bmatrix} & . & . & . & . & . & . & . & . & $	$8 \begin{vmatrix} 32.7 \\ \end{vmatrix} 45.2$	21 38.24 24 44.91	6.66 6.64	11. 1 41.24 2. 3 45.05	49 53.33	3.49	21 44.90	25 45 16.82 z.
	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	1 1 1	25 20.16	6.63		33 5.47 30 20.95	$\frac{3.67}{3.70}$	$\begin{array}{c} 24 \ 51.55 \\ 0 \ 25 \ 26.79 \end{array}$	25 28 29.14 z. 25 25 44.65 z.
	Zone LXIX.	. September	23. H.	D. —9	4 25 10.0.	n'. = 45.46.	,,,	- 5 ['] .00.	
				1		10.70.		0.00.	
1 9	14.	2 19	29 37.90	8.80	IV. 4 36.861	31 53.37	43.01	19 29 46.70	24 57 46.38
2 9	47.5 11.5		$31\ 47.35$	8.81	" 2 36.550	46 45.59	42.47	31 56.16	25 12 38.06
3 9	32.2 44.4 56.		32 20.16	8.80	" 2 39.570	45 1.31	42.34	32 28.96	25 10 53.65 z.
4 7.8	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$		33 7.13	8.80	" 2 37.140	46 25.24	42.14	33 15.93	25 12 17.38 z
$\begin{array}{c c} 5 & 7.8 \\ 6 & 9 \end{array}$	48.0 0. 29.5 41.6 54.0 6.		33 24.01 34 29.62	8.75 8.77	" 6 36.345 " 3 36.233	17 41.92	42.07	33 32.76	24 43 33.99
$\begin{bmatrix} 0 & 3 \\ 7 & 9 \end{bmatrix}$	29.5 41.6 54.0 6.		34 35.18	8.77	" 3 41.096	38 11.46 35 23.54	$41.80 \\ 41.78$	34 38.39 $34 43.95$	25 4 3.26 z
1 1	34.0 46.4 58.1 10.5 22.2 34.6 46.		37 10.42	8.77	" 1 43.840	48 25.31	41.78	34 43.95 37 19.19	25 1 15.32 25 14 16.45
9 9	$ \dots \dots 55.5 7.5 19.6 42.0 \dots $		38 7.65	8.71	" 5 46.765	20 24.35	40.90	38 16.36	24 46 15.25
10 8	24.5 36.5 48.5 1.0	19	42 0.88	8.73	" 1 39.990	50 38.25	39.94	19 42 9.61	25 16 28.19
<u>i</u>		1 1		† Taken as I	V.				

ber	Magnitude.	s	ECOL	DS C	OF TI	RAN	SIT	s.		т.	a.	MICROMETER.	D.	d.	Mean Right Ascension,	Mean South
Number	Magr	1. 1	1. 111	. Iv.	ν.	vi.	vII.	10. 1	1.						1850.0.	1850.0.
		<u> </u>	Zone	LXX	<u>.</u> ,	Sept	embe	r 24.	М	. D.=-9	24° 27′ 47′.1	1. n'. = -25	5.16. n. =-	$-4^{''}\!.00.$	(Continued.)	
31	8.9				5.5	17 5	29.5			h. m. s. 21 50 53.27	$+{}^{s.}_{7.43}$	v VII. 1 35.37	_53 16 .54	1395	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	25° 21′ 17″.60
32	8				1 1	- 1	40.0			59 3.90	7.32	" 3 34.40	39 13.52	12.93	59 11.22	25 7 15.56
33	8							17	8	59 10.77	7.33	11. 2 36.77	46 36.14	12.92	59 18.10	25 14 36.17
34	7	52	2.0 3.	6 16.3	28.04	40.0	52.1	.	• 100	22 6 15.98	7.23	I. 6 37.96	16 44.88	12.11	22 6 23.21	24 44 44.10 z.
35	9.10			- 1	1 1			2.515	5.2	7 8.37	7.25	11. 1 38.18	51 38.90	12.01	7 15.62	25 19 38.02
36	7.8	35	6.0 46.	5 59.0	1 1	• •		1		10 58.91	7.16	V. 7 48.12	5 3.42	11.58	11 6.07	24 33 2.11
37	9							17.1 29	ı	11 22.85 19 22.90	7.19 7.09	11. 5 43.00 " 7 39.01	22 32.51 10 17.11	11.54 10.72	11 30.04 19 29.99	24 50 31.16 z. 24 38 14.94
38	$9.10 \\ 7.8$					i	59.0	$egin{array}{c c} 26.238 \end{array}$		20 31.81	7.09	" 5 37.43	25 44.84	10.72	20 38.91	24 53 42.55 z.
39 40	7						- 1	22.43		21 28.35	7.07	11. 7 40.97	9 9.44	10.51	21 35.42	24 37 7.06 z.
												" 4 43.43	28 4.73	10.42	22 31.70	24 56 2.26 z.
41	7.8 8	0.00	2.5		59.0	 11 A	1	19.0 3	1.1	22 24.62 25 46.84	$7.08 \\ 7.04$	VII. 3 36.42	38 3.77	10.42 10.09	22 31.70 25 53.88	24 56 2.26 z. 25 6 0.97 z
42 43	5			i	26.03	1		1		27 13.92	7.03	" 6 35.97	17 53.60	9.95	27 20.95	24 45 50.66 z
44	9				1 1		22.5			27 46.15	7.02	10. 6 34.71	18 36.74	9.90	27 53.17	24 46 33.75 z
45			. 45.							$32\ 58.06$	6.97	2 4 34.56	33 11.22	9.41	33 5.03	25 1 7.74
46	8			0 8.1	20.1	32.1	44.2			35 8.01	6.96	I. 2 44.89	41 56.39	9.22	3514.97	25 9 52.72 z
47	8.9			1	18.1			1	• 50	36 6.27	6.92	VII.7 48.19	5 0.80	9.13	36 13.19	24 32 57.04 z
48	6.7	l !			3				- [43 1.71	6.85	" 7 47.24	5 33.59	8.53	43 8.56	24 33 29.23 z
49	7	1 1	1.0 56.	1	1		• •	1	7.0	$\begin{array}{ccc} 45 & 8.10 \\ 45 & 20.55 \end{array}$	6.84	V. 6 40.27 11 4 40.37	15 25.34 29 50.37	$8.35 \\ 8.33$	45 14.94 45 27.40	24 43 20.80 z 24 57 45.81 z
50	8	$ \cdot\cdot $.		.	• •	• •	• •	15.0^{2}	7.0	45 20.55	0.00	11 4 40.57				
51	8		. .	.	1		31.8			$46\ 55.37$	6.82	VII. 6 35.66	18 4.29	8.20	47 2.19	24 45 59.60 z
52	8	.		1	1 1		36.0			47 59.88	6.82	" 4 41.89	28 58.49	8.11	48 6.70 49 11.73	24 56 53.71 z 24 38 17.36 z
53	8	1			35.0		41.1		•	49 4.94 51 22.94	6.79	" 7 38.88 " 5 36.98	$\begin{array}{c cccc} 10 & 22.23 \\ 26 & 0.98 \end{array}$	$8.02 \\ 7.83$	51 29.72	24 53 55.92 z
54 55	9.10	20.83	3.045.	1	33.0	•		l i		55 57.15	6.72	III. 7 43.63	7 38.41	7.47	56 3.87	24 35 32.99 z
56	8	20.00	- 1	50.0	1 1					55 50.03	6.72	VI. 7 37.79	10 59.96	7.48	55 56.75	24 38 54.55
57	6	1 1					40.9	59.01	1.0	$56 ext{ } 4.53$	6.74	11. 2 45.51	41 34.35	7.46	56 11.27	25 9 28.92
58	4.5	$ \cdot\cdot $.		54.0	6.0			58 29.93	6.69	" 7 47.98	5 7.42	7.27	58 36.62	24 33 1.80 z
59	9.10	• • •	. 47.	3 0.0						23 1 59.71	6.68	10. 6 36.30	17 41.88	7.03	23 2 6.39	24 45 36.02
60	8.9	• • •		• • •	• •	• •	50.1	8.32	0.5	2 13.88	6.68	11. 3 40.25	35 50.91	7.02	2 20.56	25 3 45.04 z
61	8	.	. 9.	5 21.5	33.5					$4\ 21.57$	6.66		10 5.23	6.89	4 28.33	24 37 59.23 z
62	8									4 55.45		VII.5 34.81	27 15.90	6.85	5 2.10	
63	9							• • •	H	6 39.38	6.63	VI. 7 37.91	10 55.82	6.75	6 46.01 9 6.33	24 38 49.68 z 24 47 41.59 z
64 65	8.9		49							8 59.72 11 1.80	$6.61 \\ 6.59$	VII.6 32.66 " 3 36.30	19 47.87 38 7.91	$6.61 \\ 6.50$	11 8.39	24 47 41.59 z 25 6 1.52 z
65 66	8.9	$\frac{39.55}{5}$								14 15.66	6.56	1. 3 39.35	36 21.97	6.35	14 22.22	25 4 15.43 z
67			5.717.							19 29.80	6.51	2. 1 41.23	49 53.85	6.09	19 36.31	25 17 47.05 z
68	7		. 52					1 1		21 4.40	6.49	VI. 5 41.55	23 23.28	6.03	21 10.89	24 51 16.42
69	6	1	4.5 26	38.5	50.8	3.0	14.8			$22\ 38.62$	6.48	VII.3 44.34	33 30.31	5.97	22 45.10	25 1 23.39 z
70	9	• • '	7.0 18.	8 31.0	43.0				[$25 \ 31.08$	6.45	V. 1 37.49	52 3.53	5.87	25 37.53	25 19 56.51 z
71	5.6	34.14	6.358	1 10.3	3 22.4	34.4	46.5			34 10.33	6.37	VII. 4 37.40	31 33.54	5.61	34 16.70	24 59 26.26
72	9									35 35.72	6.36	I. 1 33.46	54 22.50	5.58	35 42.08	25 22 15.19
73	9	1	5.0 27	$.0^{[}_{1}$						38 39.26	6.33	2. 6 42.85	13 55.70	5.50	38 45.59	24 41 48.31
74	8		.	i	1 1		1	1 1		38 57.31	6.32	VII. 3 33.55	39 42.83	5.49	39 3.63	25 7 35.43 z
75	1							$ 26.0 ^{3}$		39 31.62	6.32	(†) 2 29.33 VII 4 26 54	50 53.96	5.48 5.45	39 37.94 42 11.14	25 18 46.55 z 24 59 55.76 z
76	8		· · · · · 44						• •	42 4.84 43 56.19	6.30 6.28	VII. 4 36.54 VI. 5 35.50	32 3.20 26 52.22	5.43	42 11.14	24 59 55.76 z 24 54 44.76
77 78	9 5	1 1	4.916		1 1	1	1	! !		45 28.93	6.27	VII. 3 40.25	35 51.53	5.42	45 35.20	25 3 44.06 z
79	8.9		4.436							47 48.31	6.25	2. 3 40.40	35 46.01	5.39	47 54.56	25 3 38.51
80	8									23 48 3.59	6.25	B .	45 1.00	5.39	23 48 9.84	25 12 53.50
				J						†1	laken as IV					

Number.	Magnitude.	I.	SE	1	IDS	OF '	ΓRAI		'S.	-	т		a	•	MICROMETER.		D.	d.			Right ension,	De	ın So clinati 60.0	
		1		Zon	e LX	х.	Sej	ptem	ber 24.	M	•	D. =	=-24° 2	27 47	7.'11. n' = -2	2516	n.'=-	-4.00	. (C	ontinu	ıed.)			
81 82 83 84 85 86 87 88 89 90 91 92 93 94		43.2 4.0 43.5	55.7 19.1 16.1 43.0 55.3	7.6 30.9 30.0 18.8 7.5 28.0 55.0 7.4	19.8 43.3 42.0 30.8 19.7 40.0 7.0	31.4 45.5 31.5 52.0	52.3 31.0 10.4	56.0 18.0 9.7 27.9 4.4 16.3		25	55 59 0 0 5 7 7 11 11 14 17 21	\$1.64 19.70 43.13 41.90 33.56 30.90 51.48 19.62 28.05 40.13 7.08 19.56 46.36 10.94	+ 6 + 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	s. .22 .18 .14 .13 .09 .07 .07 .04 .03 .00 .99 .95	r. VII. 4 36.05 2. 4 38.49 IV. 7 36.81 VII. 4 43.95 7 46.28 IV. 1 39.01 11. 2 43.32 2. 1 43.39 VII. 3 37.79 7 35.23 I. 3 34.43 IV. 6 40.31 VII. 7 41.20 III. 2 47.61		32 20".15 30 55.57 11 33.94 27 47.37 6 6.74 51 11.08 42 50.00 48 39.28 37 16.45 12 28.27 39 12.49 15 24.00 9 2.14 40 22.68	5. 5. 5. 5. 5. 5.	H	23 50 55 59 0 0 5 7 7 11 14 17 21 22	3. s. 47.86 47.86 25.88 49.27 48.03 39.65 36.97 57.55 25.66 34.08 46.13 13.07 25.51 52.30 16.86	24 58 24 39 24 55 24 33 25 19 25 10 25 16 25 5 24 40 25 7 24 43 24 36	126 3 48.0 26.3 3 39.8 3 59.2 36 3 42.5 3 31.8 6 9.0 20.8 7 5.1 8 16.8 8 55.0 8 15.6	33 z. 39 z. 33 z. 25 z. 31 z. 33 z. 35 z. 32 z. 38 z. 32 z.
				<u> </u>			LXX		Octo			м.		—26°	25 ['] 10 ^{''} .0. n'.	=-	-25.00.	n".=-	4″.13	3.				,
1 2 3 4 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 *19 20 21 22 23	8.7 8.9 8 8 9.10 8 8.9 8.9 9.10 7	47.1	7.6 5.0 57.7 5.1	40.2 17.4 (9.6 117.3 511.8 5.55	29.4 45.2 54.3 0.1 21.8 29.5 7.5 24.0 21.2	4.3. 57.4 6.6 12.3 41.6 19.5 35.7 29.0	16.5 16.7 . 10.1 19.0 24.5 	29.29.3 36.8 37.5 6.5 	112.0 24.	. 77 33 2	59 59 1 1 2 3 5 8 8 9 10 12 16 19 26 27 32 33 34 34	29.88 32.44 33.22 2.33 15.44 52.00 52.41 29.50 45.20 54.32 21.88 29.54 7.40 23.93 17.51 21.11 6.77 38.40 17.33	51 55 55 55 55 55 55 55 55 55 55 55 55 5	6.39 6.33 6.34 6.29 6.30 6.22 6.23 6.23 6.23 6.21 6.19 6.10 6.93 6.92 6.93 6.93 6.93 6.93 6.93 6.93 6.93 6.93	VII. 1 34.10 III. 3 32.28 11. 2 36.22 " 5 47.10 " 2 48.62 VII. 1 35.20 " 7 46.36 2. 6 45.40 VI. 2 46.70 " 1 43.25 VII. 4 35.83 " 1 42.32 11. 3 39.17 2. 5 33.57 " 2 38.41 I. 5 30.61 VII. 5 39.31 " 7 46.77 V. 7 44.10 VI. 6 40.75 VII. 6 38.92 11. 2 36.88 " 2 39.36		54 0.81 40 27.20 46 55.52 20 10.94 39 47.28 53 22.88 6 3.81 12 27.58 40 54.26 48 44.95 32 27.89 49 16.97 36 28.40 27 58.46 45 40.16 29 41.03 24 40.60 5 49.62 7 22.05 15 8.57 16 11.68 46 32.70 45 7.07	22. 21. 21. 21. 21. 20. 20. 20. 19. 19. 19. 18. 18. 17. 16. 16. 16. 16. 15.	50 50 50 50 50 50 50 50	599 591 591 591 591 591 591 591 591 591	5 35.25 9 37.77 9 38.55 7.68 2 20.75 5 57.30 6 57.63 9 49 9 59.55 5.17 2 22.41 5 27.02 9 34.66 1 12.43 1 28.93 9 22.44 1 26.03 1 11.69 1 43.31 1 20.64 1 22.28	27 5 27 12 26 45 27 18 26 31 26 37 14 26 57 14 26 55 26 50 26 31 26 40 26 41 27 11	33.06 58.7 27.06 42.227.06 42.227.06 42.227.06 42.227.06 42.227.06 42.227.06 42.227.06 42.227.06 42.227.06 42.	70 z. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2.
			ı			CORI	RECTI	ons.		1			1	-			INSTRU	MENT	REAL	DINGS			1	
			cor	. то	HOUR		m.	n	. c		ZEN		COINC.				Α.	B.	C.	p.	Mean.	BAR.	THEF	Ex.
Oct. 7	, at 21/	h	_4	,757	s. +0.	013	s. -0.261	s.	s. 273 +0.	022	ზ 6	4".93	r. 40.110	Zo LX	XI.—Oct. 7 5 5 2	6. 20.9 21.3 22.0 22.5 23.6	294° 12' 15'.5 13.5 	20″.4 18.4 17.5	27.0 25.0 21.2	20".3 18.3 16.1	20″.80 18.80 16.52	30.268 30.302 30.318	67.1 66.8	64.8 64.3 26.6 62.3 61.0



ber.	Magnitude.		SECOI	NDS	OF T	'RAN	SITS.		Т.	a.	MICROMETER.	D.	đ.	Mean Right Ascension,	Mean South
Number.	Magr	1. 11	ı. III.	ıv.	v. 1	vi. v	п. 10.	11.	1.	a.	MICROMETER.	D.	α.	1850.0.	1850.0.
			Zon	ne LX	XI.	Oct	ober 7.	Ν	$I. \qquad D. = -2$	6 25 10.0.	n'. == -25".	00. n'. == -	4.13. (Continued.)	
24	8							7.0	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$+\frac{s.}{4.93}$	11. 2 39.64	_44 57 ["] .37	-15.80	$21 \ 37 \ 4.05$	27° 10′ 23″.17 z.
25	9			54.0	6.3				38 54.08	4.86	V. 7 38.73	10 27.48	15.53	38 58.94	26 35 53.01 z.
26	7				5	3.2 5	6.0		39 28.50	4.85	VII.7 41.89	8 38.15	15.45	39 33.35	26 34 3.60 z.
*27	9.10		1	1			1	16.3	40 9.28	4.86	11. 5 46.92	20 17.15	15.36	40 14.14	26 45 42.51
28	9.10	1	1	1	- 1	1	.1 22.0		47 27.50	4.85	10. 4 43.60	27 59.19	15.20	41 32.35	26 53 24.39 z.
29 30	9	31	.0 42.8			16			43 55.36	4.81	V. 6 36.11	17 48.94	14.89	44 0.17	26 43 13.83
31	7			193 4	36.0		$\begin{bmatrix} 0.8 \\ 0.3 \end{bmatrix}$	• •	44 39.80 48 23.57	4.84	VII.1 39.62 2. 2 38.34	50 50.19 45 42.58	14.79 14.32	44 44.64 48 28.37	27 16 14.98 z.
32	7.8				27.740			1	52 15.50	4.75	" 1 42.91	48 56.23	13.86	48 28.37 52 20.25	27 11 6.90 z. 27 14 20.09 z.
33	6	17.7 30							55 54.27	4.67	" 7 37.78	10 59.74	13.44	55 58.94	26 36 23.18
34	5.6		. 12.8	1											
35	8	1 1	12.6	1			3.8	1 8	22 4 25.30 4 31.97	4.60	1. 3 35.62 I. 2 33.25	38 30.98 48 38.72	12.50 12.49	22 4 29.90 4 36.58	27 3 53.48 z.
36	9.8	! !	.7 27.9	1 1					$6\ 40.22$	4.55	VI. 6 37.16	48 38.72 17 12.57	12.49	$\begin{array}{c} 4 \ 36.58 \\ 6 \ 44.77 \end{array}$	27 14 1.21 z. 26 42 34.83
37	5		. 54.7						8 6.93	4.53	VII. 7 34.60	12 49.89	12.11	8 11.46	26 38 12.00
38	8.9		30.5						14 42.67	4.45	VI. 7 39.16	10 12.54	11.45	14 47.12	26 35 33.99 z.
39	8.9			38.0	50.3	2.4 14	6		$15\ 37.85$	4.47	VII.2 44.17	42 21.55	11.37	15 42.32	27 7 42.92 z.
40	1	36.0 48							19 12.68	4.44	I. 2 38.75	45 28.73	11.02	19 17.12	27 10 49.75 z.
41	9	1 1	8						21 19.31	4.42	VII.1 34.24	53 55.99	10.83	21, 23.73	27 19 16.82 z.
*42	5						5.5		22 28.65	4.38	" 5 39.80	24 23.65	10.74	22 33.03	26 49 44.39
43	9.10	• • •	. 32.3	344.2	56.8	21	. 6	• •	31 44.54	4.28	2. 4 37.20	31 40.25	9.99	31 48.82	26 57 0.24
44	10	39.0							34 15.93	4.25	VII.3 38.75	36 43.51	9.81	34 20.18	27 2 3.32
45	8		2.5 24.3			1.5 13	.7		38 36.85	4.20	" 3 33.15	39 56.93	9.50	38 41.05	27 5 16.43 z.
46	9		. 23.2						40 35.69	4.20	V. 1 33.21	54 31.82	9.36	40 39.89	27 19 51.18
47	9	5.818 50.8 3	.1 30.3			- 1		1 1	42 42.64	4.17	VII.2 32.94	48 49.41	9.24	42 46.81	27 14 8.65 z.
48 *49	8		$\begin{array}{c c} .1 & . \\ .8 & 5.5 \end{array}$			1	• • •	1 1	48 27.79	4.09	2. 3 36.85	37 48.79	8.88	48 31.88	27 3 7.67 z.
50	8		1			7 3 10	0.028.0		48 18.17 49 33.12	4.09	V. 4 31.70 11. 5 32.74	34 50.72 28 26.85	8.90	48 22.26	27 0 9.62
51	7				18.0			10.1	52 5.80	4.04	V. 4 37.28	31 38.04	$8.82 \\ 8.69$	$\begin{array}{ccc} 49 & 37.19 \\ 52 & 9.84 \end{array}$	26 53 45.67 z. 26 56 56.73 z.
52	9				- 1	- 1	1	20.5	52 13.25	4.04	11. 4 38.73	30 47.11	8.68	52 17.29	26 56 5.79 z.
53	8	19	.5 31.9	44.0					55 44.02	3.98	IV. 7 42.34	8 22.88	8.52	55 48.00	26 33 41.40
54	9			27.0	39.0 .				56 26.89	3.99	V. 3 43.21	34 9.71			00 50 00 10 -
55	6	8.420	.9 33.1						23 0 45.13	3.92	VI. 6 44.45	13 0.83	$8.48 \\ 8.28$	56 30.88 23 0 49.05	26 59 28.19 z. 26 38 19.11 z.
56		43	.555.6	8.1	20.032	2.5 45			5 8.00	3.91		47 31.98	8.12	f	27 12 50.10 z.
57	9.10	39.752	.2 4.0	17.0		53	.6		8 16.76	3.87	VII.2 38.50	45 37.41	8.00	8 20.63	27 10 55.41
58		10.3 23							10 47.26	3.83	" 5 45.82	20 55.74	7.92	10 51.09	26 46 13.66
59	!								$11\ 27.22$	3.84	11. 1 39.33	50 59.61	7.91	11 31.06	27 16 17.52 z.
*60		i I	.3 18.3						14 30.90	3.80	IV. 1 36.80	52 27.84	7.83	14 34.70	27 17 45.67
61 62	9	30					.3		15 19.33	3.79	VII. 2 35.21	47 31.01	7.81	15 23.12	27 12 48.82 z.
63		20.9 33							19 55.14 23 57.75	$3.73 \\ 3.67$	" 1 38.74 2. 7 41.34	51 20.59 8 56.82	7.69	19 58.87	27 16 38.28 z.
				1 1			1						7.64	24 1.42	26 34 14.46 z.
64 65	8.9						51.5		24 57.20	3.66	11. 6 42.64	14 2.58	7.63	25 0.86	26 39 20.21
66		36.949						3.0	25 55.62 20 13 77	3.65	" 7 38.17	10 46.02	7.62	25 59.27	26 36 3.64
67		53.5 6							$\begin{array}{c} 29 \ 13.77 \\ 31 \ 30.58 \end{array}$	$\frac{3.62}{3.59}$	2. 6 38.66 1. 3 39.44	16 20.30 36 19.09	7.57	29 17.39	26 41 37.87 z.
68	5.6	12	.3 24.6	37.0	49.3				36 37.00	3.54	I. 3 34.13	39 23.09	$7.56 \\ 7.55$	$31 \ 34.17$ $36 \ 40.54$	27 1 36.65 27 4 40.64 z.
69	9								23 36 40.60	3.55	1	53 5.93	7.55	23 36 44.15	27 18 23.48 z.
				7	Zone L	LXXI	I. (l l	er 8. M.	D = -2	7 55 10.0.	n'.=-18.60.	n".=3	00.	
1	0	25 0 45	c	10	1 5 0 0	, ,		1	04.40		_			The second secon	
$\begin{vmatrix} 1 \\ 2 \end{vmatrix}$	9	$35.0 47. \ 28.7 41.$	459 E	12.4	24.5 36	7 49	.2	• •	21 12 12.17	5.61		26 23.72	16.67	21 12 17.78	28 21 50.39
1	9	20.741.	. + 00.0	$\frac{0.51}{30.84}$	12.855	5.6		1 8	14 6.33 21 15 30.59	5.61 5. 5 9		48 47.18	16.38	14 11.94	28 44 13.56
							1		~1 10 00.00	5.53	111.2 41.02	43 41.75	16.17	21 15 36.18	28 39 7.92

Number	Magnitude.	ı.	SECON	NDS OF		SITS.	11.	Т.	a.		MICROMETER.		D.	d.	A	n Right scension,	Dec	n Sou clination	
		1	Zon	le LXXII	Г. О	ctober 8	. I	Л. D.=—	27 55 1	10.0	0. n'=-18 ["] .	60.	n".==30	0. (Contin	ued.)			
4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 *** *** *** *** *** *** *** *** ***	8.9 7.8 9.10 6.7 8 6 7 8.9 9.8 9 6.7 9 9 8.9 9 6.7 9 9 8.9 9 9.10 4.5 6 9 8.9 9 9 9 9 9 9 9 9 9 9 9 9 9	37.0 3.6 37.0 17.0 15.7 	36.5 48.6 23.6 19.7 16.0 28.6 51.2 3.5 28.0 30.0 42.6 43.7 56.6 48.0 5.0 17.3 5.0 17.3 5.0 17.3 39.2 51.1 18.4 30.0 18.7 30 39.5 51.2 39.5 39.2 51.1	38.3 50	5 3.51 19.03 	1.5	58.4 55.5 14.0 10.3 14.2 	h. m. s. 21 16 24.81 18 38.32 19 54.04 24 1.33 24 36.18 25 16.31 28 32.11 29 40.91 33 16.36 33 23.69 36 40.42 38 54.87 39 0.66 41 8.73 42 0.62 47 50.18 42 47.20 46 43.21 50 52.84 51 20.12 52 48.63 53 5.13 54 2.11 55 5.31 57 29.96 58 30.28 59 2.45 22 1 32.27 5 4.00 5 43.02 8 43.41 9 51.37 11 15.99 14 2.13 14 22.33 15 59.08 17 39.93 17 39.54 18 20.09 22 21 24.50	5 5 5 5 5 5 5 5 5 5.	55 53 52 49 47 47 41 42 36 33 35 30 27	2. 2 39.23 IV. 3 37.36 VII. 3 36.11 2. 5 43.32 I. 3 35.54 2. 5 35.98 VII. 7 43.17 2. 1 35.60 4 4 38.19 VII. 7 40.65 IV. 7 38.45 V. 2 44.30 11. 7 45.66 6 6 48.83 VII. 7 42.47 2. 5 38.14 VII. 7 32.15 6 2 46.38 11. 1 42.68 6 7 39.68 6 1 39.73 IV. 1 41.41 VII. 1 38.80 VII. 1 37.79 7 4 42.30 2. 6 38.35 IV. 1 41.41 IV. 1 38.80 VII. 1 37.79 7 4 42.30 2. 6 38.35 IV. 3 41.43 2. 6 45.05 V. 7 44.41 IV. 6 44.42 VII. 6 40.74 VII. 5 42.90 11. 2 42.52 IV. 1 39.19 11. 7 38.15 6 11. 7 38.15 6 11. 7 38.15 6 11. 7 38.15 6 11. 7 38.15 6 11. 7 38.15 6 11. 7 38.15 6 11. 7 38.15 6 11. 7 38.15 6 11. 7 38.15 6 11. 7 38.15 6 11. 7 38.15		26 57.62 27 47.69 45 10.91 37 30.76 38 13.68 22 20.53 38 33.40 26 34.07 7 52.54 53 7.87 31 4.95 9 19.55 10 35.83 42 16.33 6 25.94 10 27.43 8 16.74 25 19.47 13 38.64 41 4.27 49 3.01 9 52.43 50 17.78 51 17.78 51 17.78 51 17.78 51 17.78 51 52.57 28 43.32 16 29.73 35 10.17 12 38.28 7 9.93 13 0.65 15 7.59 22 35.37 43 16.94 51 4.47 10 45.32 52 23.05 40 59.86	-16'.0 15.7 15.5 14.9 14.8 14.7 14.3 14.1 13.6 13.2 12.9 12.8 12.6 12.4 12.5 11.0 10.3 10.3 10.3 9.4 9.1 9.0 8.8 8.6 8.6 8.7 8.7	4 21 11 14 46 66 60 00 88 00 88 00 88 66 11 55 66 63 11 77 66 63 11 77 66 68 88 88 88 88 88 88 88 88 88 88 88	m. s. 16 30.36 18 43.85 19 59.56 24 6.82 24 41.65 25 21.76 28 37.52 29 46.33 32 1.72 33 29.02 36 45.77 39 0.17 39 5.93 41 13.98 42 5.96 41 55.41 42 52.42 46 48.36 50 57.95 51 0.26 55 10.44 55.41 42 52.42 46 48.36 50 57.95 51 25.26 13 7.26 55 10.44 57 35.06 8 48.33 9 56.2 11 20.86 14 27.16 16 3.90 17 44.76 17 44.36 18 24.95 21 29.22	28 22 28 23 28 40 28 32 28 28 31 28 31 28 31 28 31 28 31 28 31 28 31 28 31 28 31 28 31 28 31 28 31 28 31 28 31 28 31 28 31 31 28 31 31 31 31 31 31 31 31 31 31 31 31 31	23.33 13.22 35.83 55.66 38.44 44.85 57.57 16.14 31.00 42.44 43.86 43.86 40.77 8 59.8 38.81 1 12.8 4 49.2 2 9.6	3 0 0 5 5 2 4 4 3 3 z. 5 5 3 3 z. 8 8 7 7 z. 5 3 3 3 3 11 4 4 z. 14 1 z. 14 1 z. 14 1 z. 14 1 z. 15 18 8 z. 14 4 z. 15 18 2 z. 16 1 z. 16 18 2
			cor. To	HOURLY	RRECTI	ons.		ZENITH					INSTRU		CLE.	GS.		THEF	RMOM.
			CLOCK	cor.	m.	n.	c.	POINT.	COINC.		_		Α.	в.	C. 1	o. Mean	Ann	At.	Ex.
	8, at 2	21h	s. 4.427	*. +0.010	s. -0.261	+0.273	s. +0.022	2 0 0 5,13	r. 40.104	1	Zone JXXII.—Oct. 8	h21.2 21.7 22.5 23.0 23.7 0.1	292° 42′ 30″.2 29.2 29.0	1 1	39,2 3	34.55 3.2 33.55 	30.366 	69°.1 68.0 67.2 67.0 66.8	62.7 61.6 61.7

er.	itude.		SE	CON	DS	OF :	ΓRA	NSIT	rs.		т.	a.	MICROMETER.	D.	d.	Mean Right	Mean South
Number.	Magnitude.	Ι.	п.	ш.	ıv.	v.	VI.	vII.	10.	11.	1.	a.	MICKOMETER.	D,	u.	1850.0.	1850.0.
				Zon	ie L Σ	XII	•	Octol	oer 8.		M. D.=-	27 55 10 ["] .0	o. n'.=-18'	60. n'.=3'.	00. (C	ontinued.)	
44	9.10	29.2	42.0	54.0	6.9	19.1	31.2				h. m. s. 22 24 6.67	$+ \stackrel{s.}{4.74}$	r. 2. 4 37.85	-31 16 67	— 7.60	h. m. s. 22 24 11.41	28° 26′ 34″.27 z.
45	9			29.2							$25\ 41.77$	4.72	V. 4 39.96	30 4.35	7.46	25 46.49	28 25 21.81 z.
46	9							32.0			25 54.56	4.72	VII. 5 40.90	23 44.46	7.44	25 59.28	28 19 1.90 28 9 48.29
47	8.9 9		٠.	•, •					57.6	10.7 17.0	27 2.03 $27 8.10$	4.70 4.71	11. 6 41.78 " 3 40.17	14 30.95 35 52.82	$7.34 \\ 7.33$	$\begin{array}{ccc} 27 & 6.73 \\ 27 & 12.81 \end{array}$	28 31 10.15
48 49	7.8		16.5	$\frac{1}{29.0}$::	: :		•••		29 41.41	4.66	IV. 6 35.69	18 2.17	7.10	29 46.07	28 13 19.27 z.
50	9				1	1	39.0	t .			30 13.99	4.65	VII.7 43.23	7 50.47	7.05	30 18.64	28 3 7.52 z.
51	9								29.5	42.0	30 33.46	4.66	11. 4 48.90	24 54.69	7.02	30 38.12	28 20 11.71
52	9							1	41.8	54.8	31 46.27	4.63	" 7 40.93	9 9.27	6.92	31 50.90	28 4 26.19
53	7				٠.			40.6		• •	33 3.41	4.61	VII. 7 44.64	7 1.73	6.81	33 8.02	28 2 18.54 z.
54	7							33.0			33 55.61	4.61	" 6 41.61	14 37.42	6.74	34 0.22	28 9 54.16 z.
55 50	7.8			20.5	40.5			1	24.5		34 28.33 26 49 87	4.63	11. 2 39.89 V. 7 40.53	44 47.81 9 23.89	$6.69 \\ 6.50$	34 32.96 36 47.44	28 40 4.50 z. 28 4 40.39 z.
56 57	$\frac{9}{7}$			$\frac{30.5}{51.0}$	$\frac{42.7}{3.5}$		3				36 42.87 39 3.50	4.57 4.55	v. 7 40.53 2. 6 40.86	15 3.00	6.30	39 8.05	28 10 19.30 z.
58	9.10			31.0							39 16.84	4.55	V. 6 42.66	14 1.36	6.28	39 21.39	28 9 17.64 z.
59	6							45.5			40 8.16	4.55	VII.5 37.46	25 43.32	6.21	40 12.71	28 20 59.53 z.
60	9			1		1	1	47.0			44 9.81	4.49	" 6 39.90	15 36.51	5.93	44 14.30	28 10 52.44 z.
61	9		1	324.6	1	1	i	1	• •	٠.	46 37.23	4.48	(†) 2 42.02 V 1 24.00	43 35.10 54 3.72	5.77	46 41.71 47 49.08	28 38 50.87 28 49 19.41 z.
62 63	8	19 5		32.0			551 ($\begin{vmatrix} \cdot \cdot \cdot \\ 3.5 \end{vmatrix}$			47 44.61 49 26.05	4.47	V. 1 34.00 I. 2 29.48	50 48.09	5.69 5.57	49 30.50	28 46 3.66 z.
		40	1							•		1			1		
64	9			5 44.5 56.0	1	1	1	$ \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot$	• •	• •	51 57.41 53 8.40	4.41 4.41	2. 2 33.79 VII. 1 34.96	48 18.79 53 30.34	5.42 5.35	52 1.82 53 12.81	28 43 34.21 28 48 45.69 z.
65 66	7.8 8			52.5	1	1	1	242.1			23 2 4.61	4.41	" 7 38.17	10 45.24	4.85	23 2 8.88	28 6 0.09
67	9.10		: :			1		312.4	1		5 35.44	4.23	" 7 35.71	12 10.19	4.69	5 39.67	28 7 24.88
68	8.9		١.,			48.0	0	12.6			7 35.57	4.20	" 7 49.19	4 24.60	4.60	7 39.77	27 59 39.20 z.
69	9	•			1	1		7 26.0			12 48.77	4.15	2. 3 42.36	34 37.46	4.39	12 52.92	28 29 51.85 z.
70	7		1	3 45.5	1	1	1	i	• •	• •	$\begin{array}{c} 15 \ 57.97 \\ 16 \ 39.55 \end{array}$	4.10	" 7 37.35 VI. 6 40.62	11 13.23 15 11.72	4.28 4.25	$\begin{array}{c} 16 & 2.07 \\ 16 & 43.64 \end{array}$	28 6 27.51 z. 28 10 25.97 z.
$\frac{71}{72}$	6.7	31.9		727.0				5 46.0			18 8.57	4.03	VII. 6 48.00	10 56.71	4.20	18 12.64	28 6 10.91
73	7							7.2			19 30.11	4.06	" 6 48.00	10 56.71	4.16	19 34.17	28 6 10.87
74	9		 		15.	527.4	$4 _{40.3}$	$\frac{1}{3}53.0$			21 15.34	4.05	" 4 39.94	30 4.83	4.11	21 19.39	28 25 18.94 z.
75	8.9							25.0			22 47.96	4.02	" 7 35.90	12 3.64	4.08	22 51.98	28 7 17.72 z.
76	8.9			1	1		1			٠.	26 52.49	3.98	2. 3 37.65	37 20.18	3.98	26 56.47	28 32 34.16
77	6	1	ŀ			1	1	18.0	1	• •	27 40.70	3.97	VII. 5 41.23	23 33.08	3.96	27 44.67 34 25.01	28 18 47.04 z. 28 28 8.39 z.
78 70	7.8	• •		1	1	1	$0 \begin{vmatrix} 46.5 \\ \end{vmatrix}$	2 58.5		• •	34 21.12 36 12.91	3.89 3.86	" 3 45.35 " 7 45.58	32 54.51 6 29.32	$\frac{3.88}{3.87}$	36 16.77	28 28 8.39 2.
79 80	9	::	20		1	1	1	1			37 45.19	3.85	" 4 47.21	25 53.70	3.86	37 49.04	28 21 7.56
81	8.9	1		515.0		1	1				40 27.62	3.83	IV. 1 43.76	48 26.56	3.84	40 31.45	28 43 40.44 z.
82	6			0 16.3	3 29 .0	41.0	0 53.6	6.6			41 28.78	3.82	VII.2 37.93	45 56.14	3.84	41 32.60	28 41 9.98 z.
83	9			· ·	14.	7 27.	4		• •	• •	50 14.82	3.72	V. 1 32.59	54 52.40	3.87	50 18.54	28 50 6.27 z.
84	7.8					15.	3 28.	3 40.7			51 3.13	3.70	VII.3 30.77	41 18.14	3.88	51 6.83	28 36 32.02 z.
85								5 35.2			52 58.28	3.69	" 2 32.30	49 10.65	3.91	53 1.97	28 44 24.56 z.
86	1	1						7 11 (57 29.55	3.61	V. 7 37.55	11 6.82	3.98	57 33.16 59 37.21	28 6 20.80 28 13 59.49
87 88	$\begin{vmatrix} 8.9 \\ 4 \end{vmatrix}$	• •	1		1	1	1	$7 11.0 \\ 0 15.8$			59 33.61 0 1 38.18	$\frac{3.60}{3.58}$	VII. 6 34.43 " 1 33.80	18 45.49 54 10.41	$\frac{4.00}{4.05}$	0 1 41.76	28 49 24.46 z.
89	1	16.0	1	641.6		1	1	1	i		3 53.46	3.55	i	42 52.63	4.12	3 57.01	28 38 6.75
90	9				1	1	1 56.				4 31.59	3.54	VI. 2 44.85	41 57.19	4.13	4 35.13	28 37 11.32
91	8.9							6.8	3		5 29.17	3.53	N	43 32.10	4.16	5 32.70	28 38 46.26
92	7			• •	40.	753.	0 6.	0			0 6 40.79	3.52	VI. 4 46.52	26 17.59	4.19	0 6 44.31	28 21 31.78
April 1	A STATE OF THE PARTY OF THE PAR							1.			4 Down	roduced -:	if observed at TV				
											† Declination	requeed as i	if observed at IV.				



Number.	Magnitude.		SECO	NDS OF	TRAN	ISITS.		Т.		a.		MICROMETER.	D.	d.	Ŋ	Asce	Right	Dec	ın Se	
N	Ma	1.	п. п.	IV. V.	VI.	vII. 10.	11.					12.,			A COLUMN TO A COLU	1850	.0.	185	60.0.	
				${f Z}$ one	e LXXI	III.	October	· 9. I	Л.	D = -	39°	48 50.0. n.'=	=—17 ["] .74.	n'.=	—1″. 0	00.				
1	9.10	i		47.8 1.				h. m. 20 25 4		+7			22 ['] 33 ^{''} .53	—16″.	64	h. n 20 25	s. s. 55.07	40° 11		
$\frac{2}{3}$	9.10	i.	1 1	$\begin{bmatrix} . & . & . \\ 7.55.0 & 9. \end{bmatrix}$		$\begin{bmatrix} 52.8 \\ . \\ . \end{bmatrix}$	1 1		$9.50 \\ 55.09$.51 .40	" 3 37.90 2. 6 38.71	$37 21.70 \\ 16 20.41$	16. 15.	9		$17.01 \\ 2.49$	40 26		
4	9				. 2.5	7.5	1 8		33.82		.44	VII.2 37.30	46 30.76	15.	H		41.26	40 35	35.9	92
5	8.9			3 22.0 .			1 1		21.95	1	.38	2. 2 42.50	43 29.51	14.	1		29.33	40 32		
6 7	8.9			$egin{pmatrix} 054.2 & 9 \ 546.7 & 0 \ . \end{bmatrix}$		$\frac{38.0}{1.0}$	1 1		$\frac{54.50}{16.65}$	i	$.28 \ .27$	I. 7 43.15 2. 4 35.00	$\begin{bmatrix} 7 & 54.33 \\ 33 & 3.37 \end{bmatrix}$	13. 13.	Ħ		$\begin{array}{c} 1.78 \\ 53.92 \end{array}$	39 56 40 22		
8	8			244.458			1 2		14.26		.27	VII. 3 37.43	37 38.14	13.	1		51.53	40 26		
9	9		31.1 45.	5 14.	.2 29.0 4	13.6		21 0 3	59.97	7	.04	" 2 38.52	45 48.18	10.	А		7.01			
10	5.6	• •	51.0 4.9	9 19 . 4 33 .	.8 48.1	2.5		3 :	19.40	6	.96	10. 6 44.61	12 55.58	9.	89	3	26.36	40 1	55.4	47 в.
				Zone	LXXI	v. (October	11.	м.	D.=	3	9 48 20.0. n.:	=-7 [.] 00.	n'.=	— 1ő.8	3 6. .				
1	5	16.8	31.345.	6 0.0 14.	3			22 28	0.06	4	.64	2. 1 42.30	49 27.51	6.	24	22 28	4.70	40 37	7 53.	75
2	5.6		42.2 56.	7 11.2 24	.7 39.7 5	53.8	1 1		10.86		.55	VII.7 44.04	7 22.92		04	30	15.41	3		
3	9	1	22.3 37.	1	7				51.76	1	.49	" 2 43.77	42 46.01		57		56.25	40 31		
4 5	$\begin{vmatrix} 8.9 \\ 7 \end{vmatrix}$	52.0	6.520.	$5 \begin{vmatrix} 35.0 \\ \end{vmatrix} 28.$			1 8		$\frac{34.81}{13.97}$	ì	$.42 \\ .42$	" 4 47.02 " 1 39.29	26 6.49 51 15.44		34 19		39.23 18.39	40 14		
6	4			1					24.64		.33	IV. 7 42.24	8 26.03		04		28.97	39 56		
7	9			3.	7 18.0			43	49.16	4	.32	VI. 6 37.49	17 3.58	4.	93		53.48	40 5		
8	7			1	0 22.8 3	1			53.75		.30	VII. 5 39.86	24 26.06		85		58.05	40 12		
9 10	$\begin{vmatrix} 9.10 \\ 8 \end{vmatrix}$	1	59.7 14.	$\begin{vmatrix} 2 & . & . \\ 5 & 28.7 & 43 \end{vmatrix}$		11.8	1 8		27.78 28.70	1	$.16 \\ .07$	11. 2 39.84 VII. 5 38.80	$\begin{vmatrix} 45 & 1.66 \\ 25 & 2.87 \end{vmatrix}$		$ \begin{array}{c c} 28 \\ 05 \end{array} $		31.94 32.77	40 33		
11	9				. 13.02	-		23 7 4			.87	" 6 38.12	16 41.31		ì		46.31	40 5		
12	9				1 1	51.8	1 1		8.34		.88	" 1 36.71	52 44.68		47		12.22	40 41		
13	6			4 1	.7 36.6 5	1			8.12	1	.81	" 7 39.27	10 8.57	3.	8		11.93	39 58		
$\frac{14}{15}$	9	1	46.1	$\begin{vmatrix} 14.7 & 28. \\ 5 & 12.1 & 26. \end{vmatrix}$		1	1 6		14.60 12.00		.64 $.48$	" 5 37.60 " 3 36.05	25 44.49 38 26.00		06 85		18.24 15.48	40 14		
16	8.9	20.0	45.757				1		21.61	1	.39	" 6 41.70	14 36.90	2.	Ħ		25.00	40 20		
17	9		1 1 .	8 53.	1 1		1		39.03		.27	'VI. 7 44.15	7 19.45	2.			42.30	39 55		
18	9								17.94	1		VII. 7 49.51	4 13.15		73 70		21.07	39 52		
19 20	9 9		$\begin{bmatrix} 23.6 \\ 49.5 \end{bmatrix}$	$4 \begin{vmatrix} 17.7 \\ 17.7 \end{vmatrix}$.	.5				51.93 17.70	1	.05 .96	" 5 44.44 " 7 39.71	21 47.15 9 53.17		76 82		54.98 20.66	1		
21			1 1	0 18.3 32.				0 1			.91	" 2 38.42	45 52.08	2.	i		21.12	40 34		
22	$\begin{bmatrix} 7 \\ 6.7 \end{bmatrix}$	40.2		23.237					23.25		.70	I. 6 39.63	15 48.77		30		25.95	40 4		
23	6.7		48.3 2.	6 16.8 30	.9 45.8		1 1	15	16.84	2	.67	" 6 37.31	17 9.48	3.	39		19.51			
24	6	1		0 54.0 .					54.21		.62	IV. 6 37.91	16 51.86		52		56.83	1		
$\frac{25}{26}$	$\begin{vmatrix} 6 \\ 2.3 \end{vmatrix}$::		47.0 1.			1 1		$47.08 \\ 59.61$	1	.61 $.58$	V. 3 33.17 " 1 30.65	40 6.58 56 16.01		56 66		49.69 2.19	40 28		
27	1		1 1		0 34.0				4.72	1	.54	VII. 4 38.50	31 2.53		78		7.26			
	1		1	COI	RRECTI	ons.							INSTRUM	ENT I	READI	NGS.				
			COR. TO	HOURLY				g p	,,,,					CIRC	LE.				тне	RMOM
			CLOCK.	cor.	m.	n.	c.	ZENIT		COINC.			Α.	в.	c.	D.	Mean.	BAR.	At.	Ex
Oct.	9, at 21 <i>i</i>	h	s. -4.288	s. - 0.004	s. _0.261	$_{+0.273}^{s.}$	s. +0.022	o° ó	4".51	r. 40.105	Z_0	one h. XIII.—Oct. 920.4	280° 51′ 18″.2	19.5	27.2	22.0	21.72	1. 30,202	71.4	67.4
	11, at 2		-4.896	- 0.008			+0.022	0 0	- 1	40.105		20.7	16.0	17.3	- 1	20.0		30.196		
~~~~			1-70-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1	l	1	<u> </u>	<u> </u>	1			LX	XIV.—Oct. 11, 22.5	280 51 45.8	46.2	1	48.5	,	30.436	60.4 57.0	
												23.0 23.5					: :		56.8	1

er.	itude.		SI	ECOI	NDS -	OF '	TRAI	risi	rs.		т.			MICROMETER.	D.	d.	Mean	Right	1	n Sor linati	
Number.	Magnitude.	I.	11.	III.	ıv.	v.	vi.	vii.	10.	11.	1.	a.		MICROMETER.	р.	u.	1850.	,	1850		<u>-</u>
				Zone	e LX	XIV	·. (	Octol	oer 1	1.	M. $D. =$	39° 48	ź 21	0.0. $n. = -7.0$	0. n."=-	10.86.	(Contin	ued.)			
28 29	9 9			8.0		45.0	59.3				h. m. s. 0 25 22.44 27 30.75	2	.50 .46	VII. 6 39.50	$-20^{'}$ $41^{''}$ .62 15 53.25	$-3^{''}_{4.02}$	27	$24.94 \\ 33.21$		$17.2^{\circ}$	7
30	7			• •		27.4	42.0	56.4	• •	• • •	0 28 12.91	2	.45	6 " 2 39.17	45 25.96	4.06	0 28	15.36	40 33	50.0	2
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1 2	$\begin{vmatrix} 2.3 \\ 4 \end{vmatrix}$	0.8	15.		1	1	$32.8 \\ 514.1$		1		21 11 3.48 14 44.83		.88	8	$\begin{array}{c c} 6 & 38.20 \\ 19 & 4.29 \end{array}$	18.56 17.92	21 11 14	8.36 49.66	41 26 41 38		
3	3.4						7 59.5			• •	22 29.99		.71	1	30 25.45	16.60		34.70	41 50		
4	6	14.6					7 29.0			• •	30 59.18		.66	B 3	31 52.95	15.23		3.84	41 51		
5	6	• •	1				327.5				42 58.09		.35		47 7.34	13.40		2.44 $25.68$	42 6 41 57		
$\begin{vmatrix} 6\\7 \end{vmatrix}$	7 4	30 (	54		$\begin{bmatrix} 21.5 \\ 5 \end{bmatrix}$		1 51.0			• •	22 0 21.66 5 23.26		.02	H 1:	$     \begin{array}{c c}       37 & 42.46 \\       45 & 48.62     \end{array} $	$\frac{11.06}{10.45}$		27.19	41 57		
8	2	39.0		1	1	1	59.1	 13.8			6 29.49		.91	1	45 57.57	10.43 $10.32$		33.40	42 5		
9	4				36.5	1	1 1				14 36.54		.75	4	52 16.39	9.39		40.29	42 11		
10	6.7				1				56.6	12.0	16 51.06	3	.71	" 1 43.31	49 3.66	9.15	16	54.77	42 8	42.8	1
11	2		14	198 8	343 5		13.0	97 5			34 43.52	, 3	.36	" 1 38.00	52 8.45	7.44	34	46.88	42 11	45 8	9
12	6		14.	20.0	10.0	1	34.8				36 5.80		.30	9	13 38.23	7.32		9.10	41 33		
13	7					1	40.6				44 11.45		.15	8	28 25.52	6.68		14.60	41 48		
14	7					37.5	52.0	6.7			46 22.93	3	.10	6 40.95	23 52.63	6.53	46	26.03	41 43	29.1	6
15	5		.,					0.7	23.0	38.0	47 17.20	3	.09	" 3 43.34	34 18.45	6.46	47	20.29	41 53	54.9	1
16	5	1	1		1	1	1 20.9		l		$51 \ 51.57$	3	.01	IV. 3 37.64	37 37.16	6.15	51	54.58	41 57	13.3	1
17	5	27.7	1	1		i	5 41.0		1	• •	55 11.86	1	.92		17 54.37	5.94	ł	14.78	41 37		
18	4		1	1		1	4.6		1		23 6 35.42		.71	il i	35 29.99	5.33	23 6		41 55		
19	5	• •				1	4 59.3				8 29.80		.67	R I	41 20.22	5.23		32.47	42 0		
20	3	• •	• •		3.7	18.	732.8	• •	· ·	• •	10 3.82	2	.64	V. 5 49.85	18 43.43	5.17	10	6.46	41 38	18.6	ОВ.
21	6.7		.,		24.0	38.6	53.3	8.0			12 23.87	2	.59	VII.3 42.73	34 39.48	5.08	12	26.46	41 54	14.5	6
22	6								18.1	32.7	36 12.26	5 2	.11	8	11 35.65	4.55	•	14.37	41 31		
23	5	6.7	721.			1	219.8			• •	43 50.58		.97	<b>R</b> !	19 59.64	4.50	i .	52.55	41 39		
24	7			34.0	0 46.5	1.3	5 16.0	30.5			23 52 46.70		.79	VII.7 36.19	11 58.60	4.54	23 52	48.49	41 31	33.1	.4
					Zoi	ne L	XXV	Ί.	Oc	tober 1	7. M.	D. = -	45	<b>å</b> 46 47.78. n'.	== -2 ["] .12.	". = -	-19.00.				
1	7	Π	Ι	T.,	40.3	3	10.5		l		21 4 40.25	3 4	.96	3 VI. 4 39.25	30 45.05	19.22	21 4	45.19	43 17	52.0	)5
2	4	32.3	347.	1		1	47.0	1			17 17.30		.73	2	24 30.96	16.91		22.03	43 11		
3	6	50.1	5.	0 20.3	5 35.5	5	6.3	21.1	٠.		24 35.67	4	.62	2 " 1 45.21	48 3.80	15.63	24	40.29	43 35	7.2	21
4	6	20.8	36.	551.0	5.9	20.5	5 36.3	51.0	• •		21 30 6.04	4	.48	8 " 6 32.24	20 11.33	14.67	21 30	10.52	43 7	13.7	′8 
			1			COR	RECT	ions				1			INSTRU	MENT RE	ADINGS.				
			1	г. то оск.	Houi	- 1	m.	,	ı.	c.	ZENITH POINT.	COINC.				CIRCLE			BAR.	THER	RMOM.
															Α.	в. с	р.	Mean.		At.	Ex.
Oct.	16, at 9	22h		s. 5.709	s.		s. 0.530	+0.	.507	$^{s.}_{+0.022}$	0° 0′ 4′.57	r. 40.111		Zone h. LXXV.—Oct. 16, 21.2 21.7	'	11'.0 21'.	0 10'.0	12 ^{''} .80	30.132 30.140	63.1 63.5	61°.1 63.0
† Oct	. 17					•.		.						22.4 23.0	)	:: :	:   : :	: :	30.154	$64.3 \\ 64.5$	63.5
			1		!			1					1	23.6 LXXVI. Oct. 17, 21.0	277 54 35.0	40.0 49.		$\frac{1}{40.73}$	$30.144 \\ 29.916$	$\frac{64.5}{66.0}$	61.2 65.5
										this da			1	21.6 22.2	i	• •   •		: :	29.912 29.904	66.2 66.3	65.0 65.0
		‡7	the c	ircle re	eading	incre	ased 3/	from	tnat	recorde	α.			22.7 23.2	'	39.0 48.		39.95	29.912 29.918	66.5 66.8	65.2 64.8
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er.	itude.		SEC	ONI	os c	OF '	TRA	risn	'S.		m				D	,	0		Right	1	ın So	
I amber.	Magnitude.	1.	11.   11	1.	IV.	ν.	VI.	VII.	10.	11.	Т.	a	•	MICROMETER.	D.	d.	a e partidonesa	Asc 1850	ension, ).0.		clinati 50.0.	ion
			Zon	ie L	XX	VI.	0	ctobe	r 17.	. IN	1. D.=-	$-42^{\circ} 46^{\circ}$	47′.7	8. n'. = -20".	12. n'' = -	-19.00	. (	(Conti	nued.)			
5	7.8					• •	4.3	19.0			h. m. s. 21 40 33.8		s. .29	VII.3 40.69	35 54.47	13	.00		n. s. 0 38.09	43 22	55.2	 25
6	7.8						7.1				42 36.7		.28	" 1 35.55	53 40.88	12.	H	45	2 41.06		41.3	
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$\stackrel{\circ}{1}$	6		46.0 1	- 1	- 1		1 1				21 16.0		.46	" 6 38.46	16 34.39		.70		19.51	1	29.8	
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3			31.4 46							[	38 1.4		.13	" 4 36.41	32 23.96		.07		3 4.62	1	17.8	
4	8	٠.	19.5	. 4	9.5	• •	19.5	35.0	• •	• •	43 49.5	$0 \mid 3$	.02	" 2 34.85	48 9.51	5.	.59	43	3 52.52	43 35	2.8	38
5		1	46.3 1	- 1			1	- 1			47 16.1	į.	.94	IV. 4 33.16	34 17.89		.32		19.09	1	10.9	
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$\begin{bmatrix} 7 \\ 8 \end{bmatrix}$	6 6		11.5		- 1		20.7	36.0			150.4 $2642.0$	1	.64	VII. 2 36.35 IV. 2 42.10	47 17.35 43 56.96		.36 .34		53.06 44.16		9.4 48.0	
9		1 1	$\frac{11.5}{26.5}$ .	- 1	- 1		26.7				23 26 56.6	Į.	2.11	8 1	39 50.33		.34		58.74	1	41.4	
										Corne				ALIANAL V								
					Zor	ne I	JXXV	II.	0	ctobei	· 19. M.	D.=	=4	3 47 40.0. n.	=-27.00.	n'.=	=-21	.87.		· · · · · ·		
1	3	1	26.341				1				20 23 56.5	1	.41	i i	9 0.47	26	H		1.97		6.6	
$2 \mid$	6								• •	• •	26 23.7	1	.47	VII.7 43.68	7 34.53		.90		5 29.23		41.4	
3	6.7		56							• •	27 22.5 35 11.6	-	$\frac{1.36}{1.25}$	" 6 44.93 " 4 41.82	$\begin{array}{c} 12 \ 46.66 \\ 29 \ 17.43 \end{array}$	25. 24.	- 1		7 27.95		52.2	
$\begin{bmatrix} 4 \\ 5 \end{bmatrix}$	$\frac{6.7}{2.3}$		$\frac{1}{41.4}$ 56				42.2				38 12.3	1	.22	III. 2 42.38	43 53.34		.50		3 17.53		56.8	
6	7										38 29.7		.21	VII.2 42.30	43 55.61	23.	н		34.92	44 31	59.0	)5
7	7						26.1		•,•		$41\ 55.4$		.16	" 1 37.71	52 33.20	22.	9		0.60	44 40		
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$\begin{bmatrix} 9 \\ 0 \end{bmatrix}$	4		13	$\begin{vmatrix} \cdot \\ 0 \end{vmatrix}_2$	- 1		38.5	- 1	16.8	2.8	47 37.8 50 28.3		.95	" 1 39.30 " 7 43.34	51 37.75 7 46.78	21 . 21 .	9		42.89 33.34	1	48.0	-
1	5	44.6	0.115								55 30.4	2 4	.87	IV. 6 34.62	18 48.12	20.	.42	55	35.29	44 6	48.5	i4
2			40.955	- 1	- 1		1 1	- 1			21 0 10.9		.78	" 7 37.27	11 19.84	19	H		15.77	1	19.4	
	4.5		0.5 15								8 30.9		.68	" 1 39.99	51 13.91	18.	a		35.60	44 39		
4	7		40								11 55.3			VII.6 42.70	14 4.64	17.	12		59.91	1		
5	7	1 1	$30.245 \\ 33.848$	+	- 1		1	- 1		• • •	$   \begin{array}{cccc}     16 & 0.78 \\     20 & 4.1   \end{array} $	1	.52 $.42$	IV. 3 38.53 " 5 44.15	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	17. 16.	ä		5 5.30 8.53	44 25 44 10		
6 7	$\frac{4.5}{6.7}$		99.040								28 30.2	ì	.28	VII. 6 35.35	18 22.40	15.	H		34.55	44 6		
8	3		51.0 6								33 21.8	1	.16	IV. 5 43.15	22 39.41	14.	9	33	26.03	1	34.0	
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0	7		54.8 10				1 1	- 1		[	50 25.2		.81	VII. 4 54.45 " 6 50.86	21 55.24	12.	N		29.03		47.7	
$\begin{vmatrix} 1 \\ 2 \end{vmatrix}$	7 4	1	$\frac{14.4}{10.225}$	1	- 1		1 (	- 1			53 44.7° 21 56 41.1°	1	.73	IV. 1 35.71	9 18.99 53 43.92	$\frac{12}{11}$ .	11		3 48.50 5 44.88	43 57	$\begin{array}{c} 11.1 \\ 35.8 \end{array}$	
							RECTI						1		INSTRUM	TENT	READ	INGS.				
				T				.0110.			ZENITH			710000			RCLE.				тнек	RMO
			CLOCK.	- 1	cor.	- 1	m.	n.		c.	POINT.	COINC.	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		Α.	В.	c.	D.	Mean.	BAR.	At.	ŀ
t. 19	), at 22	h	s. -6.30	3	s. 0.0	18 -	s. -0.530	s. +0.5	507 -	s. ⊢0,022	359 57 8.09	r. 40,123	Zo LX	XVII.—Oct. 19, 20.	1 276° 51′ 59″.6	4'.8	16.7	5.7	6.70	ı. 30,226	51,3	
				1								<u> </u>		21. 21.	6 58.0		::	: :		30.228	50.9 50.2 49.7	4
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er.	tude.		SE	CON	DS (	OF	TRA	NSI	rs.		TI.				D.	d.	3	Right		un Sc	
Number.	Magnitude.	I.	II.	ш.	1v.	v.	VI.	vu.	10.	11.	Т.		a.	MICROMETER.	р.	a.	185	,		50.0.	
			Z	one I	LXX	VII	. (	Octol	er 19	).	M. D.=	=-43 4	7 40	0.0. n'. = -27	/00. n."=-	_21 ["] .87.	(Cont	inued.)			
23	4	22.2	38.1	53.1	9.0	24.5	39.6	53.2			h. m. s. 22 2 8.	86 +	s. 3.60	IV. 1 37.01	<b>-52</b> 58.49	<b>—</b> 11 ["] .40		n. s. 2 12.46	44° 40	49".8	39
24	6		1						29.0	45.0	7 20.		3.48	A .	41 6.66	10.92	â .	7 23.63	1	3 57.5	8
25	6		43.1		1 1		1	59.8			11 13.		3.00	b	01 50 01	10.00	a a	1 16	44	10.0	•0
26	6.7	1	1		i 1		5				13 58.		$\frac{3.32}{2.21}$	R .	21 52.31 21 52.21	10.32 $10.29$	Я	$ \begin{array}{ccc} 4 & 1.68 \\ 4 & 20.33 \end{array} $	1	42.6 42.5	
27 28	$\frac{7.8}{2}$	1	43.2		1 5				26.0 • •	41 0	14 17. 20 13.		$\frac{3.31}{3.20}$	8	27 51.35	9.77	H	0 16.69	1	41.1	
29	2	~			1 1		13.5		1		20 42.		3.20	li de la companya de la companya de la companya de la companya de la companya de la companya de la companya de	43 13.87	9.73	8	0 45.95		3.6	
30	6	f	1				28.6				22 57.	ł	3.14	¥	31 12.57	9.57	2	3 0.94	44 19	2.1	4
31	5.6								20.0		23 11.	73	3.12	10. 6 42.41	14 14.84	9.55	2	314.85	44 2		
32	5	56.5	12.1	27.1	42.5	57.5	12.4	28.0		٠.	27 42.	34	3.03	IV. 4 45.65	27 4.69	9.23	2	7 45.37	44 14	53.9	2
33	7.8				15.5	31.0	)				29 15.	60	3.01	10. 2 43.28	43 20.55	9.11	2	9 18.61	44 31	9.6	6
34	7					41.8	57.3	13.0			29 26.	i	3.01	R .	43 36.52	9.10	Я	9 29.63	44 31		
35	6				43.7		13.5	28.5			39 42.	99	2.77	ii .	26 24.29	8.49	H	9 45.76		12.7	
36	8				1		42.0		1	[	46 11.	61	2.61	8	8 53.02	8.16		614.22	1	41.1	
37	7						25.0			• •	54 54.	į.	2.42	B	4 59.31	7.81	ä	4 57.18		47.1	
38	6		1 1	i			41.5			 1C 1	57 11.	- 1	$\frac{2.37}{0.27}$	3	$5\ 26.60$ $31\ 59.42$	$7.73 \\ 7.70$	3	$713.68 \\ 824.01$	i i	$14.3 \\ 47.1$	
39	$\frac{1.2}{7.8}$		$ \cdot\cdot $	40.9			52.0 $34.5$				58 21. 23 7 3.		$\frac{2.37}{2.18}$		37 22.72	7.48	H	7 5.97	44 25		
$\begin{vmatrix} 40 \\ 41 \end{vmatrix}$	7.8		1 1	1			35.0		í		12 4.	- 1	2.16	§ .	10 22.57	7.39	g	2 6.78		9.9	
42	5			- 1	- 1		26.5				13 55.		$\frac{2.00}{2.02}$	i	13 0.89	7.38	N	3 57.98	44 (		
İ				-								1			9 12.20	7.36	1.	5 30.63	43 50	59.5	6 B
43	$\frac{3}{7.8}$		• •	- 1	28.5		59.0 $30.0$			• •	15 28. 16 59.	1	$1.99 \\ 1.98$	i .	53 13.01	7.35	Ħ	7 1.13		0.3	
$\begin{vmatrix} 44 \\ 45 \end{vmatrix}$	7.8			• •			23.7				23 52.	1	1.80	1	37 23.75	7.34	ă	3 54.61		11.0	
46	8		1	48.0							49 3.	1	1.26	8	22 24.38	7.76	4:	9 4.71	44 10	12.1	4
47	6	48.1	1		34.0						0 4 34.	01	0.93	IV. 6 46.40	11 56.00	8.46	0 -	4 34.94	43 59	44.4	6
48	6					49.5	4.8	19.8			5 34.	33	0.91	VII.7 46.10	6 10.02	8.52	il.	5 35.24	1	58.5	
49	6		22.5	38.0	53.5						8 53.	i	0.84	b	49 5.31	8.70	B	3 54.31	i	54.0	
50	7		• •	• •	• •		1 1			• •	9 40.		0.82	N .	53 27.15	8.74	Ē.	9 40.93	1	15.8	
51	4			• •	• •	• •	1		20.7		11 11. 19 47.	- 1	$0.79 \\ 0.61$	8	$16 \ 31.47$ $43 \ 0.40$	$8.84 \\ 9.44$	3	1 12.62 9 48.31	44 30	1 20.3 1 49.8	
52	1.2		• •	• •	• •	• •	• •		56.8	12.3											
53	5						30.6				24 0.		0.52	8	35 20.61	9.77	H	4 0.56	1	10.3	
54   55	$\begin{array}{c} 7 \\ 4.5 \end{array}$						11.5 $31.3$			• •	31 40. 43 0.	1	$0.36 \\ 0.13$	8	$\begin{array}{c} 19 \ 30.05 \\ 24 \ 57.62 \end{array}$	$10.40 \\ 11.49$	Ħ	1 41.33 3 0.80	44 12		
56					1		21.5			• •	0 44 50.			IV. 2 42.55	43 46.97	11.68	il .	4 50.90	1		
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-	C	10.5	0.5	15.0	20. 0	44.0	FO. 6				01 07 00	00	2.69	VII. 5 43.40	22 22.34	10.89	91.0	5 32.67	40 11	92 0	13
$\begin{vmatrix} 1 \\ 2 \end{vmatrix}$	6	40.5					58.0				21 25 29. 27 10.	1	$2.69 \\ 2.67$	š .	41 9.59	10.70	ii .	7 13.64	40 30		
3	1	56.8	11.5								21 29 39.		2.61	i I	23 7.92	10.43		9 42.53	i .	8.3	
-				1	(	CORI	RECTI	ons.						123	INSTRUI	MENT REA	dings.		I		
				Ī		T		1					-			CIRCLE	2.			тнев	MOM.
			COR.		COR	- 1	m.	n	٠.	c.	ZENITH POINT.	COINC			Α.	В. С.	D.	Mean.	BAR.	At.	Ex.
				-		-	8		-	8		- r.	-   3	Zone I					ı.	0	0
Oct. 2	1, at 22	2h	<u>-7</u> .	708	-0.0	24 -	_0.530	+0.	507	-0.022	0° 0′ 6.2	r.40.123	Ĺ	XXVIII.—Oct. 21,21		32.0 41".	i	33.95	30.246	51.8	41.8
				'-							·		-		2.1 24.5			31.45	30.240	50.2	39.0
															2.4 24.5	30.0 40.		31,75		49.5	39.5
															<u> </u>	<u> </u>					

er.	Magnitude.		SECO	NDS	OF '	TRAN	SITS.		Т.		MICROMETER.	D.	d.	Mean Rig Ascensio	'	ın Sou clinatio	
ın amber.	Magn	Ι.	п. ш	. IV.	v.	yı. v	п. 10.	11.	1.	а.	MICROMETER.	D.	u.	1850.0.	1	60.0.	J11,
			Zon	e LXΣ	(VII	Ι. (	October	21.	M. D.=	—39° 48′	5ő.0. n'=-1	1.52. ".=-	10 ["] 00.	(Continue	d.)		
4	6					34.04	8.2	100000000000000000000000000000000000000	h. m. s. 21 37 5.33	s.	r. 6 VII. 7 42.49	_ ś 15 ["] .88	- 9 ["] 67	h. m. s. 21 37 7	79 39 5	15."55	 5
5	5				::		4.8	: 0	38 31.63	2.4	g.	23 11.92	9.53	38 34	1	2 11.43	
6	7			-	1	30.2		521.2	45 1.50	2.3	N N	49 53.94	8.91	45 3		3 52.8	
7	6		i l			1	7.7		48 4.73	2.2	5	11 4.76	8.63	48 6.	1	3.39	
8	6			1		514.02		1 1	49 45.48	2.2	5 VII. 5 38.47	25 13.60	8.47	49 47.	.73   40 1	12.0	7
9	5	55.5	10.024	.238.7	53.	[5,]	2.0 .	]	53 38.79	2.1	8 IV. 3 44.15	33 44.35	8.16	53 40.	1	242.5	
10	6.7		37			0.21.03		.   • • •	55 52.33	2.1	9	36 46.45	7.97	55 54	1	5 44.49	
11	2								57 - 0.43	2.1	H	27 0.22	7.88	57 2.	1	5 58.10	
12	6		13.0 27	1	1	1 1			59 41.59	2.0	9	22 47.18	7.66	59 43	1	1 44 8	
13	5	30.1	44.3 59	.0 13.2	27.3	541.8	• •   •	$\cdot   \cdot \cdot  $	22 1 13.16	2.0	3 " 4 44.20	27 43.60	7.56	22 1 15	.19 40 10	3 41.16	6
14	6	34.5	49.0 3	.3 17.7	32.0	46.5	.		5 17.72	1.9	7 " 2 47.96	40 19.67	7.28	5 19	.69   40 29	16.9	5
5	6			. 44.0			.		9 43.65	1.8	g	29 8.05	6.97	9 45		3 5.09	
6	5		1 1			3		4	8 53.86	1.9	g	51 35.67	7.02	8 55	1	32.69	
L7	5	• •	48.4 2		1	1	1		13 17.08	1.7	ä	45 3.39	6.75	13 18		1 0.1	
18	6	• •				5 58.7 1			16 29.85	1.7	1	9 58.76	6.56	16 31	1	8 55.39	
.9	2	• •	33	.8 48.3	2.	5 16.5	$\cdot \cdot   \cdot  $	•   • •	22 19 48.09	1.6	5 VI. 7 49.14	4 25.25	6.36	22 19 49	.74   39 5	3 21.6	1
5 6 7 8 9 10 11 12 13	6.7	25.0 27.3	8.5 23 		5 22. 1 7 36. 1 18 7 30. 3 27. 2 6.	46.8 		0 38.7	3 15.62 2 16.29 3 53.31 7 7.67 9 38.52 10 21.27 32 10.47 40 12.29 41 3.11 43 31.52 44 15.42 48 12.19 52 51.31 59 13.02	4.0	11. 5 45.28 14. VII. 5 45.65 11. VII. 5 42.87 10. 5 41.93 11. VII. 4 42.82 11. VII. 6 37.35 12. VII. 6 37.35 13. VII. 6 37.35 14. VII. 6 37.35 15. VII. 4 41.16 17. VII. 5 40.30 19. VII. 5 42.24 18. VII. 1 41.94	36 1.96 21 23.42 21 11.47 22 49.31 23 20.96 28 41.77 50 41.97 17 12.83 32 34.31 29 40.53 24 18.79 23 11.50 50 0.89 35 7.41	4.06 3.95 4.13 4.46 4.73 4.80 7.50 8.63 8.75 9.12 9.23 9.81 10.55 11.60	3 12 2 12 3 49 7 4 9 35 10 17 32 6 40 8 40 59 43 27 44 11 48 8 52 47 59 8	.98   43   15 .97   43   15 .26   43   15 .06   43   15 .79   43   15 .56   43   45 .26   43   25 .42   43   25 .30   43   15 .00   43   15 .00   43   43   43 .00   43   43   44	3 46.02 7 .31 5 5.66 3 33.77 4 5.69 9 26.5 1 29.4 8 1.4 8 1.4 9 29.6 5 8.00 4 1.3 0 51.4 5 59.0	7 0 7 9 7 6 6 5 2 1
15 16 17	1		515.530						2 10 45.93	4.6	1	52 32.73	13.62	$2\ 10\ 41$	1	3 26.3	
15 16 17 18	8		1	1	1	0.58.11	i	1 24	22 28.17	4.7	a	14 50.06	15.82	22 23		5 45.8	
15 16 17 18	8 7.8		1		ļ	RECTI	ons.	8				INSTRU	MENT RI	Adings.			
15 16 17 18 19	8 7.8		• •   •		COI	CICLIO I I							CIRCL	е.		THER	ŁM (
14 15 16 17 18 19 20	8 7.8												CIRCL				
15 16 17 18	8 7.8		COR. T			m.	n.	c.	ZENITH POINT.	COINC.		Α.	в. с	. р. Ме	an.	At.	]
15 16 17 18 19 20	8 7.8		COR. T	co	RLY R.		8.	s. +0.351	POINT.	-	Zone LXXIX.—Oct. 28	h0.6 277°51′ 6″.2	В. С		i i	48°.5	4
15 16 17 18 19 20	8 7.8 7.8		COR. T	co	RLY R.	m. s.	8.	s.	POINT.	-	Zone LXXIX.—Oct. 28	h0.66 277°51′ 6′.2 1.3	B. C	5 10".5 12"	an. 1	48.5 48.0	4 4
15 16 17 18 19 20	8 7.8 7.8		COR. T	co	RLY R.	m. s.	8.	s.	POINT.	-	Zone LXXIX.—Oct. 28	h0.6 277°51′ 6′.2 1.3 1.5 1.9 5.5 1.9 2.3	в. с	5 10'.5 19'	an	48.5 48.0 47.1 46.9	4 4 3 3
15 16 17 18 19 20	8 7.8 7.8		COR. T	co	RLY R.	m. s.	8.	s.	POINT.	-	Zone LXXIX.—Oct. 28	h0.6 277°51′ 6′.2 1.3 1.5 1.9 5.5 1.9 2.3	B. C	5 10".5 12 : : : i1 : : : i2	an	48.5 48.0 47.1 46.9	4 4 3 3
15 16 17 18 19 20	8 7.8 7.8		COR. T	co	RLY R.	m. s.	8.	s.	POINT.	-	Zone LXXIX.—Oct. 28	h0.6 277°51′ 6′.2 1.3 1.5 1.9 5.5 1.9 2.3	B. c	5 10.5 12 	an.  1. 48 30.074 2. 30.074 30.088 30.088 30.086	48.5 48.0 47.1	4 4

er.	Magnitude.		SE	CON	DS (	OF :	ΓRΑΓ	rsit	'S		Т.				D.	d.	3		Right	Mea	n So	
Number.	Magn	Ι.	11.	ш.	IV.	ν.	vi.	vII.	10.	11.		a.		MICROMETER.	ъ.	u.		1850		185		
			Z	one .	LXX	IX.	О	ctobe	er 28	3. N	Л. D.=-	-42° 50′	40.	0. n'. == -0″.7	6. n'.=-	$21^{'}\!.00$ .	(C	Contin	ued.)			
21	3	24.0	39.4	54.4	9.4	24.4	39.7				$h. \ m. \ s. \ 2 \ 34 \ 9.52$	$\begin{vmatrix} & s \\ + & 4 \end{vmatrix}$	.94	IV. 2 46.67	-41 9 ['] .90	18".	15	h. m 2 34	. s. 4.58	43 32	8'.0	5 в.
22	7.8						1.5				$36 \ 31.55$		93	VII.5 48.75	$19\ 23.17$	18.	64	36	26.62	43 10	21.8	31
23	4	1 1		i i	1		29.8				$39\ 59.47$	5.	01	IV. 3 38.62	37 9.72	19.	36	39	54.46	43 28		
24	7.8							58.7	21.6	36.7	41 13.19	5.	05	11. 2 36.58	47 11.12	19.			8.14	43 38		
25	8		23.7							]	45 53.80	1	10	IV. 3 40.34	36 9.95	20.	H		48.70	43 27		
26	7						20.03				48 50.29		11	VII. 5 48.07	19 47.10	21.	H		45.18 $2.75$	43 10 43 13		
27	8		54.6				38.0				3 9 8.12 13 24.46	1	.37 .41	" 5 42.80 II. 5 47.16	22 51.17 20 19.25	24.25.	Ŋ		19.05	43 11		
28 29	$\frac{8}{2}$	1			0.7			• •			13 24.40	1	48	IV. 1 45.84	47 44.73	26.	ii ii		55.39	43 38		
30	7.8							- 1		38.2	14 15.62	1	41	11. 6 39.45	15 59.38	26.	a a		10.21	43 7		
31	7.8						42.0			1	21 11.88	5	.52	VII. 4 39.38	30 42.29	28.	ı	21	6.36	43 21	51.1	2
32							1.3.0				24 16.86	1	50	IV. 7 43.26	7 52.14	29	9		11.36	42 59		
33	3				- 1		17.0				24 46.78	1	53	VII. 6 36.30	17 49.98	29.	8		41.25	43 8		
34	8				1						32 21.06	1	59	" 7 45.39	6 37.20	31.	ă.	32	15.47	42 57	48.8	33
35	7						43.5			[	34 3.39	5.	64	" 5 41.65	23 31.30	32.	.07	33	57.75	43 14	43.3	37
36	5.6		1							42.6	36 18.99	5.	71	10. 1 37.97	52 18.71	32.	.66	36	13.28	43 43	31.5	37
37	7.8				13.8	29.3					39 14.00	5.	75	B .	51 27.54	33.	42	39	8.25	43 42	40.9	6
38	6.7	4.5					19.3	- 1		]	49.39			IV. 6 32.87	19 50.20		9			43		
39	7	i					23.5				48 53.03	1		i i	45 21.99	35.	1		47.21	43 36		
40	7	36.0	51.1	6.3	21.7	36.5	51.5	6.6	٠.		51 21.43	5.	.84	" 2 45.82	41 49.13	36.	.63	51	15.59	43 33	5.7	6
41	5		4.7								4  2  34.79	1	.90	IV. 4 44.38	27 48.07	39.	i i		28.89	43 19		
42	7.8						51.0			• •	3 20.77		.89	VII.5 40.96	23 55.56	39.	1		14.88	43 15		
43	7.8						57.2			1 8	5 27.46		.87	" 7 40.31	9 34.71		.50		21.59	43 0		
44	7.8						50.0	- 1		• •	11 20.12	!	.90	" 7 41.79	8 42.74	42.	H		14.22	43 0		
45	6	1					30.2			• •	17 0.29		.96	" 6 36.92	17 28.13	43.	H		54.33 59.67	43 8 43 21		
$\frac{46}{47}$	7.8 8						$\begin{array}{c} 36.0 \\ 10.0 \end{array}$				19 5.68 20 39.71		.01 .06	" 4 41.14 " 2 37.30	29 40.66 46 47.22	44.44.	g		33.65	43 38		
48	7.8						48.0				23 18.02	1	.99	" 6 43.42	13 41.21		.56		12.03	43 5		
49	6						10.0				25 46.25		.06	IV. 2 47.21	41 1.28		.27		40.19	43 32		
50	6		1 1				21.0			1 11	25 50.31	4	.10	11. 1 37.50	52 35.17	46.	- 4		44.21	43 44	.1.4	15
51	8	51.5	7.0		36.5	51.8	7.0	22.0			46 36.83	6	.12	VII.5 35.47	27 7.71	52.	.39	46	30.71	43 18	40.1	0
52	i						29.6				47 59.38		.13	N .	27 17.02	52.	11		53.25	43 18		
53	7.8						34.0				52  3.64		. 19	ä	48 40.00	54.	8	51	57.45	43 40	14.0	)2
54	7.8		1				35.0				53 4.78	6	.14	VII.5 40.40	24 15.34	54.	.32	52	58.64	43 15	49.0	)2
55	7.8						59.0	14.0	٠.		4 54 28.58	6.	.19	" 2 39.54	45 28.54	54.	.74	4 54	22.39	43 37	3.2	28
			entrantant en en en	March Strategies .	Z	one	LXX	Х.	N	oveml	er 21. M.	D.	<u> </u>	12° 50′ 50″.0. n	<u>.</u> = -4.00.	n'.==-	19.5	3.				
1	7		29 5	44 8	0.0	15 (	30.0	45.0		-	23 33 59.89	1	.96	VII.6 46.06	12 8.28	3	.16	23 33	57.93	43 3	1.4	14
2	8						29.0			1 8	37 58.85	1	.04	VI. 6 33.34	19 32.77	1	.04		56.81	43 10		
3	9	1	41.8			1		1	٠.		23 42 12.00	2	.15	II. 6 39.60	15 53.91	2.	.75	23 42	9.85	43 6	46.6	36
						COR	RECT	ions						· ·	INSTR	UMEN'	r real	DING.				
			cor.	то	Honi	RLV					ZENITH					CII	RCLE.				THE	RMOM.
			CLO		COL		m.	2		c.	POINT.	COINC.			Α.	в.	c.	D.	Mean.	BAR.	At.	Ex.
Nov	21, at	7 <i>h</i> .	s 11.	589	s.	039	s. _0 168	s. ±0	103	s + 0.351	o° 0′ 25″.17	r, 40,120	Z	Tone / XXXNov. 2123	h. 277° 51′ 6″.0	13.0	23.2	13.0	· 18.40	ı. 30,196	49°.7	42°.6
**O.K.	~1, dl		11.	500		304	-0.100	Τυ.	100	- C.OOI	0 0 20.11	20,1,50			0.0					29.955		
														0	7.2	13.2	25.0	13.7	19.70			
																		W. P. LANGE				
													:									

Number.	Magnitude.	SECONDS OF TRANSITS.  1.   11.   111.   11.   v.   v1.   v11.   10.   11.	т.	a.	MICROMETER.	D.	d.	Mean Right Ascension, 1850.0.	Mean South Declination, 1850.0.
		Zone LXXX. November 21.	M. D.=	42° 50′ 50″.0	. n' == -4'.6	00. n''=-	-19.53.	(Continued.)	
4	8	34.749.8	$h. \ m. \ s. \ 23 \ 42 \ 4.64$	s. — 2.14	VII. 6 37.42	_17 10 ^{''} .05	-2".76	h. m. s. 23 42 2.50	43 8 2.81
5	7		44 57.82	2.19	11. 2 49.24	39 47.12	2.64	44 55.63	43 30 39.76
6	8	11.527.041.756.511.326.0	$48\ 56.55$	2.32	VII.7 38.17	10 49.06	2.47	48 54.23	43 1 41.53
7	7	57.0 11.7 27.0	51 26.89	2.37	IV. 6 43.77	$13\ 28.64$	2.40	$51\ 24.53$	43  4  21.04
8	8.9		52 52.06	2.40	11. 6 38.96	$16\ 15.51$	2.37	52 49.66	43 7 7.88
9	7	$\begin{bmatrix} 5.721.036.151.0 & 6.4 & . & 36.5 & . & . & . \end{bmatrix}$	57 51.27	2.49	IV. 1 37.48	$52\ 35.58$	2.26	57 48.78	43 43 27.84
10	7	$ 40.555.8 10.425.7 40.4 55.5 10.4  \dots   \dots  $	0  4  25.56	2.66	" 7 40.53	$9\ 26.99$	2.16	$0 + 4 \cdot 22.99$	43 0 19.15 в.
11	8.9	$1.617.031.346.4 1.516.3 \dots$	$7\ 46.56$	2.74	VII.7 41.24	9 1.95	2.12	$7\ 43.82$	42 59 54.07
12	8.9		8 34.04	2.76	11. 3 34.45	$39 \ 32.70$	2.11	8 31.28	43 30 24.81
13	2	9.224.539.354.49.024.039.0.	$18\ 54.24$	3.01	IV. 6 38.76	$16\ 23.55$	2.14	18 51.23	43 7 15.69 в.
14	7	20.035.050.1 $5.520.135.450.3$	0 27 5.23	3.20	" 5 39.54	24 44.31	2.30	0 27 2.03	43 15 36.61 в.

Zone.	No.		Zone.	No	
I.	8	One minute of right ascension less makes this star identique with Zone III, 20, and with 1924, Mad-	XXV.	73	One revolution of the micrometer? Argelander, 15885, 15886, 15887.
		rass.		81	A double star.
	11	This star may be the same with Zone III, 23, and	XXVII.	27	One revolution of the micrometer? Argelander, 16011.
		1954, Madrass. A revolution of the micrometer		53	One revolution of the micrometer? Argelander, 16795.
		being misread.		70	One revolution of the micrometer? Argelander, 17201.
II.	7	One revolution of the micrometer? 2833, Madrass.	XXVIII.	109	One revolution of the micrometer? Argelander, 20929,
V.	4	One minute in right ascension? Zone XII, 4. 1502,			20930, 20931.
		Madrass.	XXXII.	50	Two revolutions of the micrometer? Argelander, 19737,
	20	2453, Madrass?			19738.
VIII.	6	One revolution of micrometer? Argelander, 11808,	XXXVII.	26	Two revolutions of the micrometer? Argelander, 18774.
		11809.	XXXVIII.	30	A double star. The following star observed.
	10	Argelander, 12131?	XL.	4	This star may be B. A. C., 5521; an error of 10 sec-
IX.	5	One revolution of the micrometer? Argelander, 14950.			onds in the right ascension.
	13	One minute in right ascension? Argelander, 15686,	XLIII.	10	A revolution of the micrometer? Argelander, 20886.
		15687, 15688.	XLVI.	52	A double star.
XI.	43	One minute in right ascension? 2191, Madrass.	L.	22	A revolution of the micrometer? Argelander, 21780,
XV.	3	One revolution of the micrometer? Argelander, 12056.			21781.
	4	One revolution of the micrometer? Argelander, 12070,	LII.	27	A revolution of the micrometer? Argelander, 19737,
		12071.			19738.
	11	Misreading of wire of the micrometer? Argelander,	LV.	39	The recorded transit readings disagree?
	4 900	12197, 12198.	LVI.	26	6812, B. A. C.
	47	One revolution of the micrometer? Argelander, 12949.		$\left \begin{array}{c}49\\50\end{array}\right\}$	The declination given for 50 is probably that of 49.
	61	One revolution of the micrometer? Argelander, 13155.	T 7777	50)	The star being 7314, B. A. C.
	66	One revolution of the micrometer? Argelander, 13246.	LVII.	52	8027, B. A. C.
	79	Misreading of wire of micrometer? Argelander, 14302.	LVIII.	32	A revolution of the micrometer? Argelander, 21615.
	81	Misreading of wire of micrometer? Argelander, 14440.		52	A revolution of the micrometer? Argelander, 22295.
	121	One revolution of the micrometer? Argelander, 15373.		54	A revolution of the micrometer? Argelander, 22316,
	$\begin{array}{c} 147 \\ 150 \end{array}$	One minute in right ascension? Argelander, 15975.  Many small stars here.	LX.	1	22317. A revolution of the micrometer? Argelander, 20784,
XVII.	150	A double star.	LA.	1	20785.
26 7 11.	27	One revolution of the micrometer? Argelander, 14302.		2	Ten seconds in right ascension? Argelander, 20792.
XIX.	29	One revolution of the micrometer? 2988, Madrass.		35	One revolution of the micrometer? Argelander, 21322.
20120.	33	A cluster of stars, of which the brightest has been		47	One revolution of the micrometer: Argelander, 21470.
	00	taken.		60	One revolution of the micrometer? Argelander, 21669.
XXI.	4	A minute in right ascension. 2785, Madrass.		154	One revolution of the micrometer? Argelander, 161.
22.2.1.	30	This star may be 5681, B. A. C. A misreading of	LXII.	10	Ten seconds in right ascension? Argelander, 21075.
	00	+ 20s. in right ascension.		51)	The right ascensions of these stars are probably trans-
XXII.		This zone has but one reading of the circle.		52	posed. Argelander, 22181, 22182.
	7	One revolution of the micrometer? Argelander, 15040.		87	One revolution of the micrometer? Argelander, 23022,
	47	Misrcading of micrometer? Argelander, 16891, 16892.			23023.
XXIII.	24	One revolution of the micrometer? Argelander, 13374.		121	One revolution of the micrometer? Argelander, 683,
XXIV.	1	A double star.			684.
	3	One revolution of the micrometer? Argelander, 15885,		127	One revolution of the micrometer? Argelander, 831.
		15886, 15887.	LXIII.	24	One revolution of the micrometer? Argelander, 19809.
	4	15895, 15896, 15897, Argelander?		37	20078, Argelander?
	13	One revolution of the micrometer? Argelander, 16630,	LXIV.	45	One revolution of the micrometer? 8376, B. A. C.
		16631.	LXVI.	22	One revolution of the micrometer? Argelander, 20406.
	41	A double star.	LXXI.	19	One revolution of the micrometer? Argelander, 21573.
XXV.	28	One revolution of the micrometer? Argelander, 13871.		27	One revolution of the micrometer? Argelander, 21656.
	40	One revolution of the micrometer? Argelander, 14548.		42	One revolution of the micrometer? Argelander, 22192.
	59	One revolution of the micrometer? Argelander, 15217.		60	One revolution of the micrometer? Argelander, 22791.
	70	One revolution of the micrometer? Argelander, 15792.	LXXII.	38	One revolution of the micrometer? Argelander, 22104.



## ERRATA.

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Zone XI. No. 43, for H, read M.
    XV.
              3, for 3, read *3.
    XV.
              4, for 4, read *4.
    XV.
              27, for *27, read 27.
    XV.
              62, for *62, read 62.
    XV.
             113, for *113, read 113.
  XVII.
              24, for *24, read 24.
 XVIII.
               7, for *7, read 7.
              23, for *23, read 23.
 XXIII.
 XXIII.
              24, for 24, read *24.
 XXIX. In the column "Mean South Declination," throughout the zone, for 410, read 400.
```